

Probing Impulsive Strain and Lattice Dynamics by Time-Resolved Ultrafast X-ray Diffraction

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To My Family and Friends

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CHAPTER I

Introduction

The interest in semiconductor dynamics is driven by the rise of solid state technology in consumer products and the pursuit of a fundamental understanding of physical properties. High purity, perfect crystal semiconductors are readily available and used in applications in the telecommunication, computer, and laser industries. With femtosecond laser pulses, extremely fast dynamics can be probed, helping to understand the fundamental interaction between light and matter on the time scale of a few oscillations of an electromagnetic field. Optical reflectivity and transmission of perturbed systems were the first experiments to indirectly measure the crystal lattice response to ultrafast excitation. X-ray diffraction, however, is able to directly assess the atomic positions inside the lattice. Synchrotron radiation, producing high brilliance x-ray pulses, together with time resolved experimental methods allows for picosecond resolution of transient dynamics in semiconductors.

Measuring acoustic phonons and strain in bulk materials has been an ongoing area of interest in the time-resolved research community. Although there are several proposals to explain the dynamics observed in crystals none describe nonlinear dependencies on deposited energy in crystals far below the damage threshold. This thesis presents time-resolved studies of strain and acoustic impulses in bulk semicon-

ductors and provides an explanation for observed ultrafast dynamics. This work is based on pump-probe experiments of indium antimonide (InSb) and gallium arsenide (GaAs). X-ray diffraction simulations of strained crystals have been developed to provide direct analysis of the data.

The remainder of this chapter serves to introduce the subject of ultrafast semiconductor science. Chapter II reviews relevant theories of ultrafast dynamics and strain in semiconductors. Chapter III introduces the theory of x-ray diffraction in perfect crystals. It continues to explain calculations for simulations of x-ray diffraction in strained crystals developed for these experiments. The experimental setup is discussed in Chapter IV. In Chapter V, results of the optical pump, x-ray probe experiment are presented for InSb and GaAs. Finally, Chapter VI concludes the study and proposes new opportunities for development of this research.

1.1 Ultrafast Dynamics

Semiconductor crystals absorb photons of energies $h\nu$, greater than the band gap E_g . In direct gap semiconductors, this process promotes valence band electrons to the conduction band without a change in momentum. At high incident radiation densities, the electron-hole pairs create an electrostatic potential large enough to alter the periodic structure of the crystal. This deformation potential deflects atomic planes, straining the crystal. Photo-induced strain occurs only within the penetration depth of the light, typically 100 – 1000 nm. The perturbed atomic planes recoil as they return to equilibrium positions, launching a coherent acoustic impulse.

The first proposed model to describe crystalline strain was a thermoelastic traveling wave model where all incident radiation energy is deposited into the lattice as heat. The resulting transient strain wave propagates at the speed of sound in the

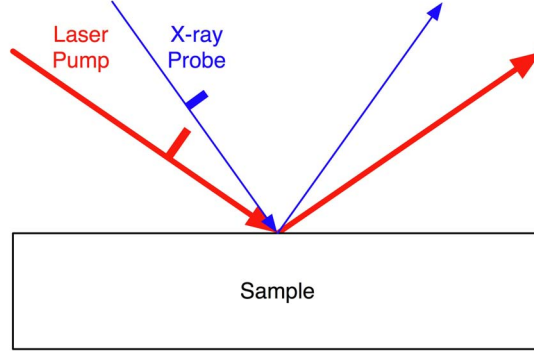


Figure 1.1: Typical setup for a time resolved pump probe experiment. The x-ray pulse probes the crystalline lattice at a time after a laser pulse perturbs the system.

material into the crystal depth, while a permanent exponential strain profile remains at the surface. A constant strain is a good first approximation since thermal diffusion is extremely slow compared to electron diffusion (six orders of magnitude slower) or other transient processes in photo-excited semiconductors. In this model, the strain response is linear with the amount of absorbed energy.

Many previous experiments have analyzed acoustic impulses and strained semiconductors data with this model [1–5]. There exists omissions from this model, including contributions from electrons and nonlinear responses to absorbed laser fluence. Other experiments have accounted for the electrons by including electron-hole plasma diffusion and Auger recombination for germanium [6]. Free carrier absorption for GaAs has also been proposed, but has not provided satisfactory supporting evidence to this phenomenon [7]. The experiments presented in this thesis investigate strain in InSb and GaAs and presents a strain model to describe the nonlinear fluence dependence in GaAs.

To measure transient strain, time-resolved Bragg x-ray diffraction is employed. This technique has been established as a powerful tool to view transient structural

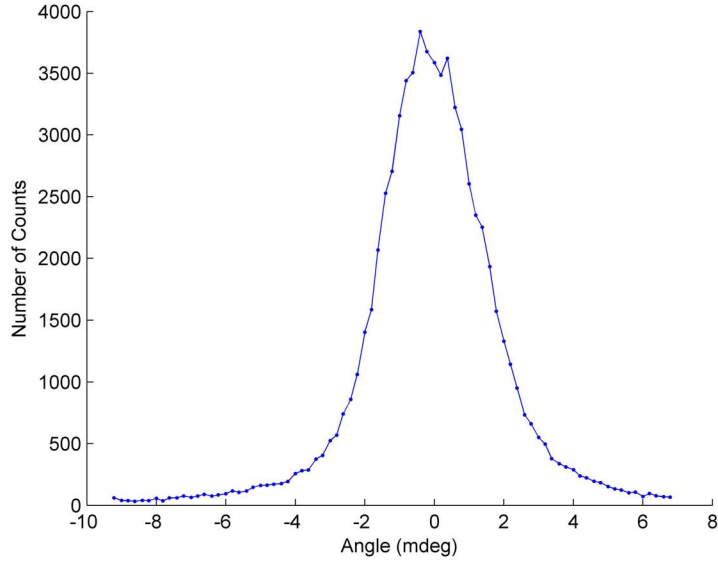


Figure 1.2: Example of Bragg diffraction peak for InSb.

dynamics in crystalline solids [8]. Using a pump-probe experimental setup (Figure 1.1), wafer samples of polished semiconductors are illuminated by femtosecond pulses of amplified laser light, deforming the crystal lattice. At a variable delay, the x-ray probe diffracts from the perturbed structure, resolving transient dynamics in the material. The delay is systematically lengthened from time-zero, T_0 , or the time when x-ray and laser pulse arrive concurrently. As the crystalline lattice is distorted, the distance between atomic planes changes and the satisfactory angle for Bragg diffraction shifts. Bragg peaks (see Figure 1.2) are recorded at each time point and the center is extracted. An example of the time-resolved data for the centroid Bragg peak shift is shown in Figure 1.3.

1.2 Thesis Motivation

The dynamics of photo-excited semiconductor systems have been the focus of many experimental pursuits [1,4,9]. However, a detailed understanding of the lattice

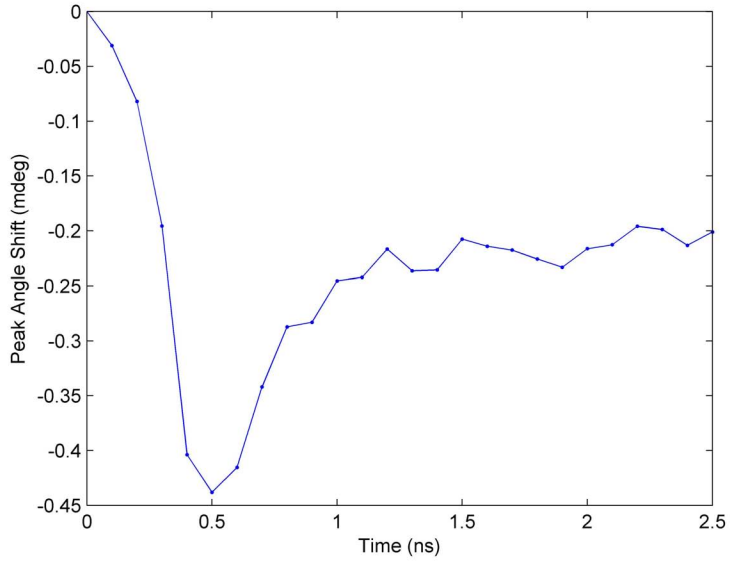


Figure 1.3: Example of Bragg diffraction peak-shift data for InSb at low fluences.

dynamics and thermalization are still illusive. These studies have used a computer model to predict the outcome of x-ray diffraction that did not include the detail necessary to investigate intensity-dependent dynamics in lattice structure across different systems. The available programs had not been adequately benchmarked, were not flexible in the selection of materials or x-ray energies, and were not scaleable to the study of increasingly complicated models of real semiconductor behavior.

Furthermore, there exists unanswered questions on the linear and nonlinear effects of InSb and GaAs. The fluence dependence of these materials are in stark contrast with each other and offer insights to carrier generation and thermalization as well as structural dynamics. This thesis demonstrates the correct method of constructing strain profiles for the purpose of analyzing time-resolved diffraction experiments.

CHAPTER II

Dynamics of Strain in Semiconductor Crystals

Strain in semiconductors generally results from lattice mismatch in atomic planes. The lattice mismatch may be constant in time, such as a crystal epitaxially grown on a substrate, or can be transient such as an acoustic phonon. This discussion will focus on transient strain in crystals where strain is produced from rapid heating, acoustic impulses, and interactions between free carriers and the lattice. The following reviews the physics of semiconductors and crystal strain imposed upon ultrafast laser excitation.

2.1 Semiconductors Under Ultrafast Laser Excitation

When light is incident on opaque material, several processes and interactions occur on various time scales from femtoseconds (10^{-15} s) to nanoseconds (10^{-9} s) which eventually transfers energy from absorbed photons to thermal vibrations in the lattice [10]. It is important to note that the subsequent processes are not sequential, but rather happens across overlapping intervals. The first energy transition is carrier generation. Photons of energy exceeding the band gap are absorbed to create a single electron-hole pair. The excess photon energy moves immediately into the lattice

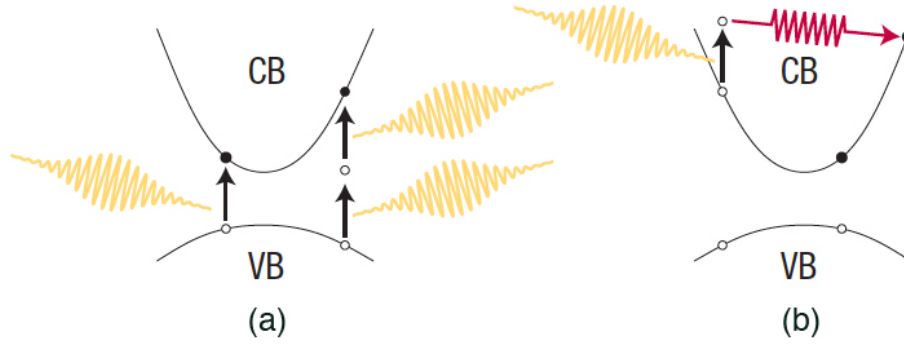


Figure 2.1: Carriers are generated through single or two photon absorption (a). Photons can also be captured through free carrier absorption (b). Figure adapted from [10].

as thermal vibrations. Two photon absorption, a nearly instantaneous process, will occur at high field intensities but since this process is intensity dependent and these experiments do not have the necessary photon densities, it does not play a role in dynamics discussed here. As well, an electron in the conduction band can absorb a second photon, called free carrier absorption (FCA). FCA does not increase the carrier density but creates highly energetic carriers within the lattice, potentially liberating additional electrons at a later time through impact ionization. Carrier generation occurs on a time scale of up to a few femtoseconds. A cartoon of these processes is given in Figure 2.1

The crystal enters the thermalization regime after the ultrashort pulse has exited the crystal and deposited energy into the electrons. Thermalization occurs primarily through carrier-carrier and carrier-phonon scattering, depositing energy into the lattice on the time scale of a few hundred femtoseconds to tens of picoseconds. Carrier-carrier scattering is an electrostatic collision that does not change the total energy of the carriers. It may take hundreds of femtoseconds for carriers to equilibrate through

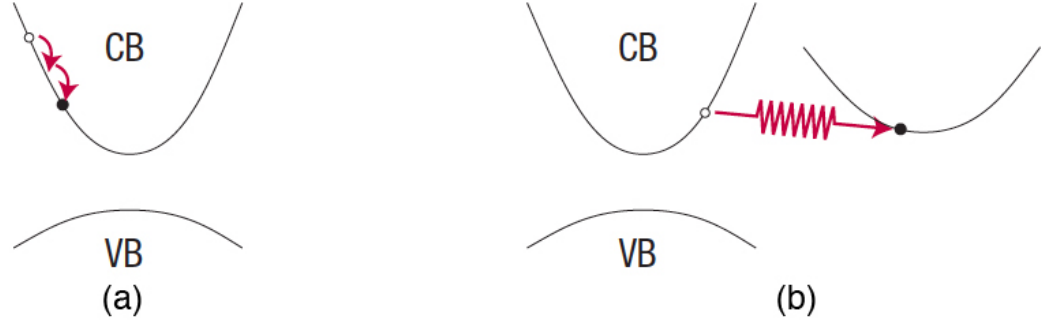


Figure 2.2: Carriers thermalize through carrier-carrier scattering (a) or carrier-phonon scattering (b) where carriers emit a phonon as heat into the lattice. Figure adapted from [10].

carrier-carrier scattering. Carrier-phonon scattering is an inelastic process in which electrons absorb (or emit) phonons, gaining (or losing) energy and momentum to the lattice. Figure 2.2 gives a schematic of the thermalization processes. Each of these process do not change the carrier density, but decreases the total carrier energy through the emission of phonons. All carriers generally reach thermal equilibrium after a few picoseconds. Throughout carrier generation and thermalization, electrons are diffusing into the crystal depth. Initially, electrons are deposited throughout the penetration depth of the laser ($\sim 100 \text{ nm} - 1\mu\text{m}$). Immediately, these carriers begin to propagate at supersonic speeds, dependent on the diffusion constant in the material.

At longer time regimes, picoseconds to nanoseconds, the lattice carriers are removed through recombination. Carrier removal takes place through radiative or non-radiative recombination. In radiative recombination, electrons transition from the conduction band to valence band and release energy as a photon. Since energy is radiated away from the crystal, the lattice remains unaffected. Non-radiative recombination transfers energy to the lattice and is dominated by Auger recombination.

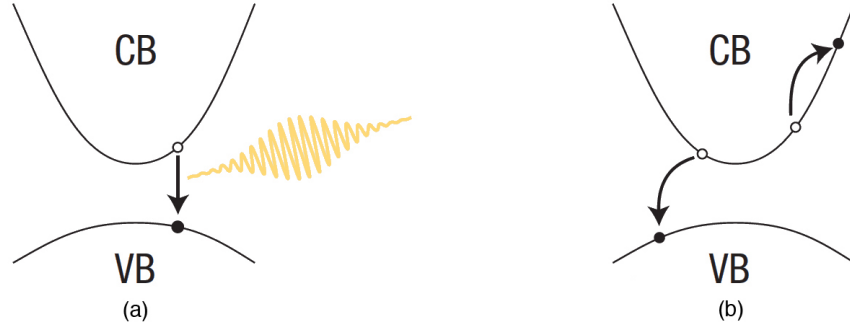


Figure 2.3: Radiative recombination (a) releases a photon where in Auger recombination (b), an electron and hole recombine, donating the excess energy to a third carrier. Figure adapted from [10].

Other non-radiative processes like recombination-generation centers and defect-and-surface recombination rely on dopants or impurities to facilitate the transition of energy into the lattice. The samples used in this study are of extremely high purity and other non-radiative recombination processes do not play a major roll in carrier removal. Auger recombination goes as the cube of the carrier density, n ,

$$\frac{\partial n}{\partial t} = -An^3 \quad (2.1)$$

where A is the Auger coefficient. This contribution quickly overpowers other recombination contributions due to the cubic dependency. The Auger process occurs when an electron and hole collide and recombine, giving the excess energy to third carrier (see Figure 2.3). This three-particle process is responsible for the cubic density dependence. The higher energy electrons thermalize through carrier-carrier and carrier-phonon scattering, giving energy to the lattice as heat. After all carriers have recombined, the lattice is hot and identical to that of a crystal heated in by conventional means where the lattice vibrations are indistinguishable between the two

cases.

In an opaque semiconductor heated without the use of ultrafast pulses, melting would occur if the root mean square of the atomic displacement (vibrational amplitude), $\langle u^2 \rangle^{1/2}$, exceeds the Lindemann criterion, or 10% of RMS displacement. When femtosecond pulses are used, the lattice disorder is initially due completely to the non-thermal electronic excitation component. At large pulse energy densities ablation can occur where free electron absorption dominates early dynamics and drives lattice vibrations into a non-thermal melting regime where material is ejected from the surface.

2.2 Strain in Semiconductors

The specific dynamics of the lattice through excitation, thermalization, and carrier removal is of importance to many in the scientific community and the semiconductor industry (e.g. optical communication, photovoltaics, solid state lasers). When carriers are produced, the lattice can¹ respond to the deformation potential by expanding. The coupling between carriers and lattice creates a highly perturbed system within the penetration depth while leaving the bulk unaffected. After the pump pulse leaves, the deformation propagates as an acoustic pulse throughout the crystal. This stress pulse, or coherent longitudinal acoustic phonon, moves through the lattice at the speed of sound. An analytic model to this strain was proposed by Thomsen *et al.* to describe an exponential strain profile matching the penetration depth profile [11]. This model assumes only thermal contributions with strain dependent on the depth, z , such that the strain tensor, $[\boldsymbol{\eta}]$, has a single nonzero component η_{33} . The solution

¹Deformation potentials can be positive or negative, corresponding to a expansion or contraction of the lattice. In this discussion, all materials happen to have positive deformation potentials.

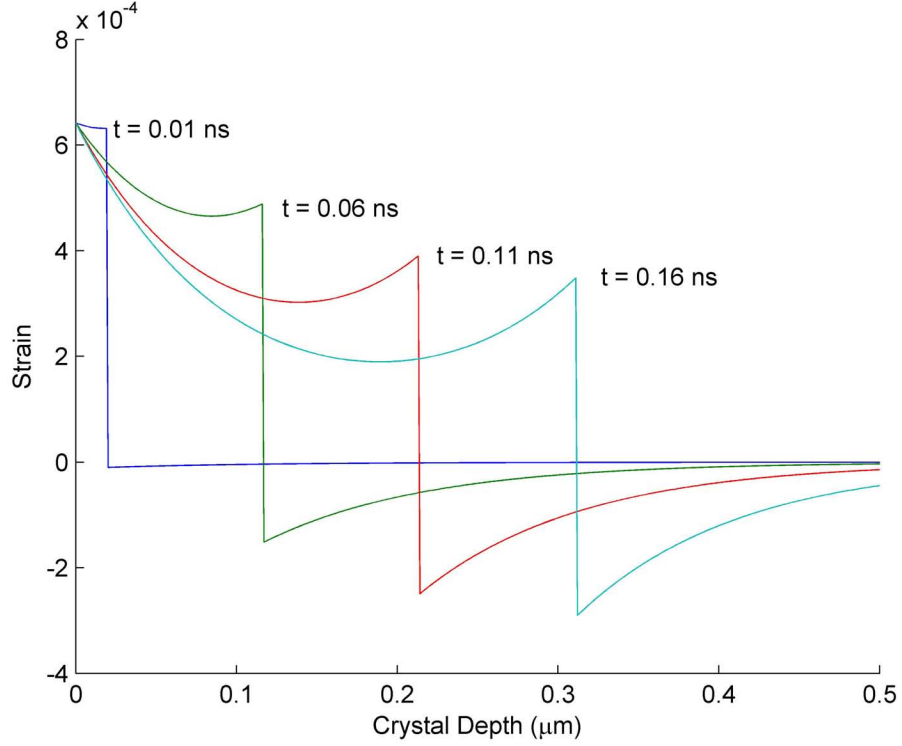


Figure 2.4: Thomsen strain model at several time points. Calculated using Equation 2.2 for InSb.

to the wave equation with the initial condition of zero strain everywhere at $t = 0$ is

$$\eta(z, t) = (1 - R) \frac{Q\beta}{A\zeta C} \frac{1 + \nu}{1 - \nu} \left[e^{-z/\zeta} \left(1 - \frac{1}{2} e^{-vt/\zeta} \right) - \frac{1}{2} e^{-|z-vt|/\zeta} \operatorname{sgn}(z - vt) \right] \quad (2.2)$$

where R is the reflectivity, Q is the energy incident on the surface of the crystal, β is the linear expansion coefficient, A is the illuminated spot size, ζ is the absorption length, C is the specific heat per unit volume, and ν is Poisson's ratio. The longitudinal speed of sound, v , in the material is given by

$$v^2 = 3 \frac{1 - \nu}{1 + \nu} \frac{B}{\rho}$$

where B is the bulk modulus and ρ is the density. A list of these parameters are given in Appendix A for InSb and GaAs.

The thermoelastic Thomsen model is mathematically sound and accurately represents an undamped wave in a homogeneous medium. Since the initial condition is zero strain everywhere, the propagating strain pulse is bipolar and has equal contributions of negative and positive amplitudes. The Thomsen strain is a product of thermal expansion alone where the temperature rise in the crystal $\Delta T(z)$, is a function of only the energy deposited per unit volume within the crystal,

$$\Delta T(z) = (1 - R) \frac{Q}{A\zeta C} e^{-z/\zeta}.$$

That is, all of the energy in the laser pulse is converted directly into heat. This is an approximation as previous experiments have shown that the electron-phonon coupling time is ~ 10 ps in many semiconductors [1,12,13]. The finite generation time smooths out the discontinuity in the Thomsen wave model. As well, strain generation in the Thomsen model is not physical. For ultrafast pulses, energy is deposited into the lattice within ~ 50 fs. In Figure 2.4, it can be seen that the strain takes an extremely long amount of time to strain the penetration depth of the laser.

A plasma driven strain model, proposed by DeCamp *et al.* (a version of this strain model is shown in Figure 2.5), accounts for the coupling between the photo-excited plasma and lattice [6]. The temperature profile (Figure 2.6) is dependent on the contributions from Auger recombination and temperature diffusion,

$$\frac{\partial T}{\partial t} = D_t \frac{\partial^2 T}{\partial z^2} + An^3 \frac{E_g}{C} \quad (2.3)$$

where D_t is the thermal diffusion coefficient and E_g is the electronic band gap. The

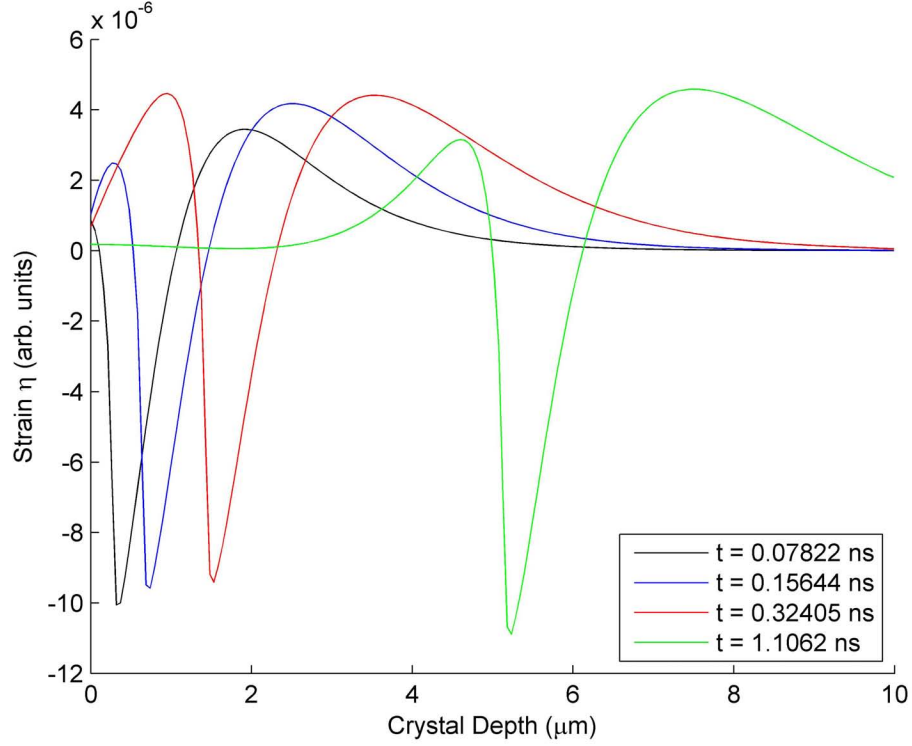


Figure 2.5: Strain profile for the case including diffusion and recombination at several time points. Calculated from Equation 2.5 for GaAs at a fluence of 0.25 mJ/cm² and laser wavelength at 800 nm.

number density of carriers is reduced by Auger recombination and diffusion moves electrons into the lattice. The diffusion length L_{diff} , is proportional to the diffusion constant and a function of time where

$$L_{\text{diff}} \sim 2\sqrt{D_{t,e} t}$$

and

$$\frac{\partial n}{\partial t} = D_e \frac{\partial^2 n}{\partial z^2} - An^3. \quad (2.4)$$

The electron diffusion (Figure 2.7) is often supersonic, creating stress deep in the

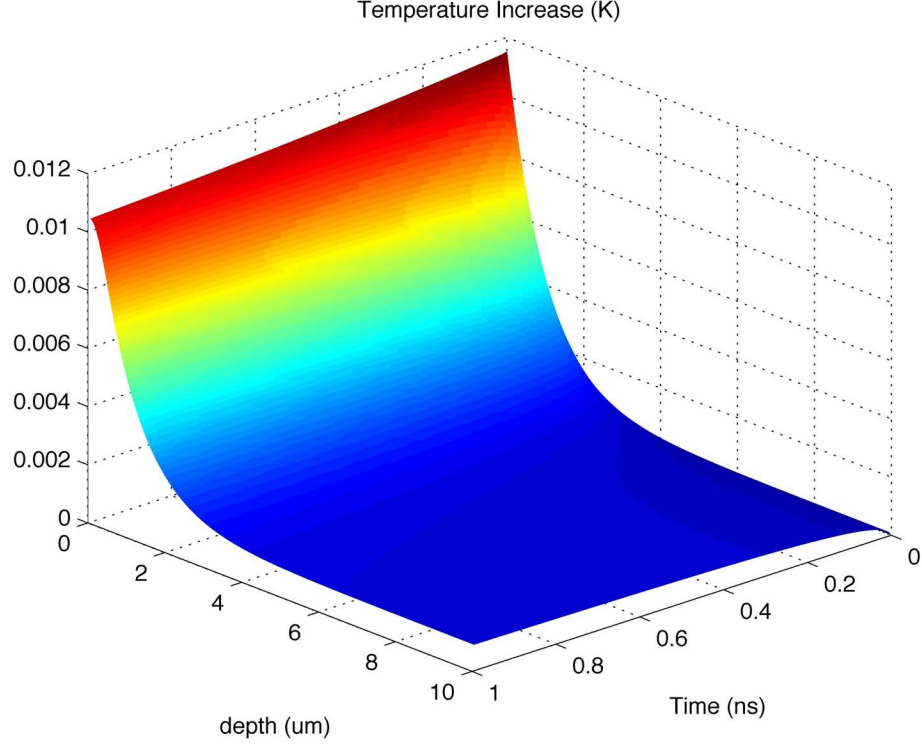


Figure 2.6: Temperature profile for GaAs, at a fluence of 0.25 mJ/cm^2 , including contributions from Auger recombination and thermal diffusion. The crystal remains hot at the surface due to slow thermal diffusion and additional heat supplied by the Auger effect.

crystal before the acoustic pulse arrives which spatially broadens the acoustic pulse by a factor of up to five [14]. The strain profile now contains temperature and plasma density dependences:

$$\eta(z, t) = \alpha_t T(z, t) + \alpha_e n(z, t) \quad (2.5)$$

where α_t is the thermal expansion coefficient and α_e is the electronic coupling coefficient, also referred to as the deformation potential [6]. A list of values for these parameters is presented in Appendix A for InSb and GaAs. The strain, η , drives a displacement in the lattice (strain wave) along a direction normal to the surface,

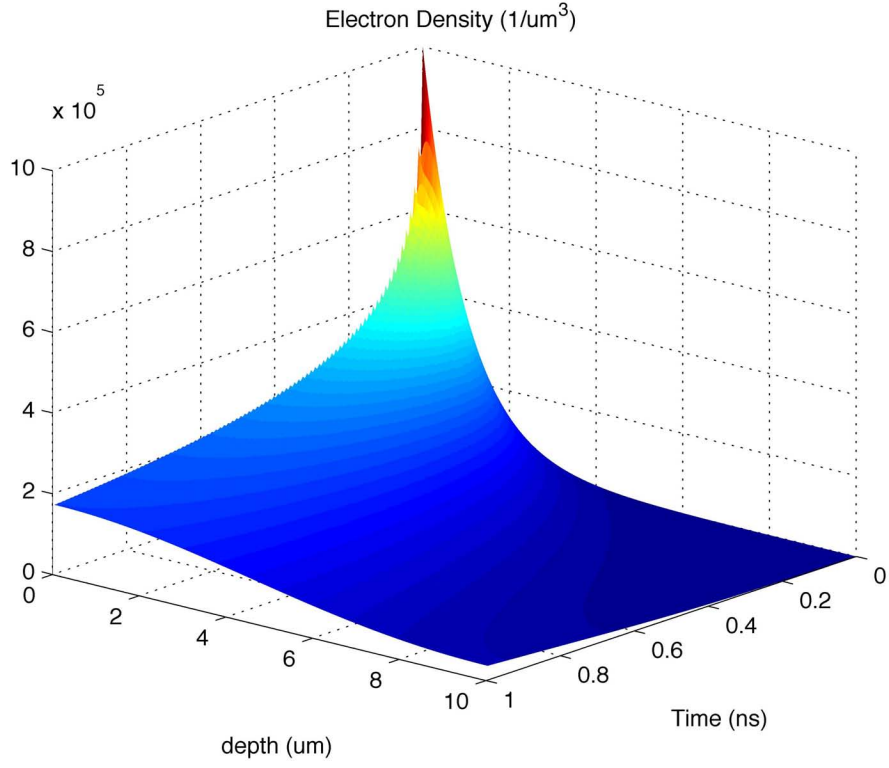


Figure 2.7: Electron density for GaAs, at a fluence of 0.25 mJ/cm^2 , including contributions from Auger recombination and electron diffusion. Electron diffusion quickly reduces the carrier density at the surface, moving deep into the crystal at early times.

governed by the wave equation,

$$\frac{\partial^2 u}{\partial t^2} = v^2 \frac{\partial^2 u}{\partial z^2} \quad (2.6)$$

where

$$\eta = \frac{\partial u}{\partial z} \quad (2.7)$$

and u is the atomic displacement from equilibrium. Due to the contributions from the electronic component, the shape and speed of the impulsive wave differs signif-

icantly from the Thomsen model. The traveling wave in space and time, solved by Equation 2.6 is shown in Figure 2.8.

It is interesting to note that the temperature profile is heavily dependent on the Auger recombination and band gap. For every absorbed photon, the excess energy over the band gap ($h\nu - E_g$) is transferred to kinetic energy of the electron. After which, the temperature diffuses into the bulk and continues to rise for several nanoseconds from the large contribution of Auger heat. The temperature profile (Equation 2.3) in space and time is shown in Figure 2.6.

The carrier density, on the other hand, is an ever-decreasing monotonic process. Assuming an instantaneous generation, carriers diffuse into the crystal and are recombined with holes, quickly eliminating excess charge. The carrier profile (Equation 2.4) is shown in Figure 2.7. The strain profile is simply the sum of the thermal and electron density profiles, scaled by the respective coupling coefficients.

Decamp *et al.* found that in order to explain the dynamics observed in germanium, diffusion and Auger recombination must be present in the strain model. Previous x-ray diffraction experiments had analyzed data using the Thomsen model with only slight modifications to approximate non-thermal terms [1, 4, 6, 12]. To correctly analyze semiconductor dynamics, the differential relations (Equation 2.3, 2.4 and 2.6) must be solved numerically.

Summarizing the progression of dynamics and strain in photo-excited semiconductors: photons are first absorbed by electrons in the material. A portion of the photon energy, equal to the band gap, goes directly into promoting electrons to the conduction band. Excess energy, $h\nu - E_g$, is transferred to the lattice as heat. As carriers cool, they recombine, further heating the lattice. The total strain in the crystal is a scaled sum of the electron deformation and thermal distortion of the lattice,

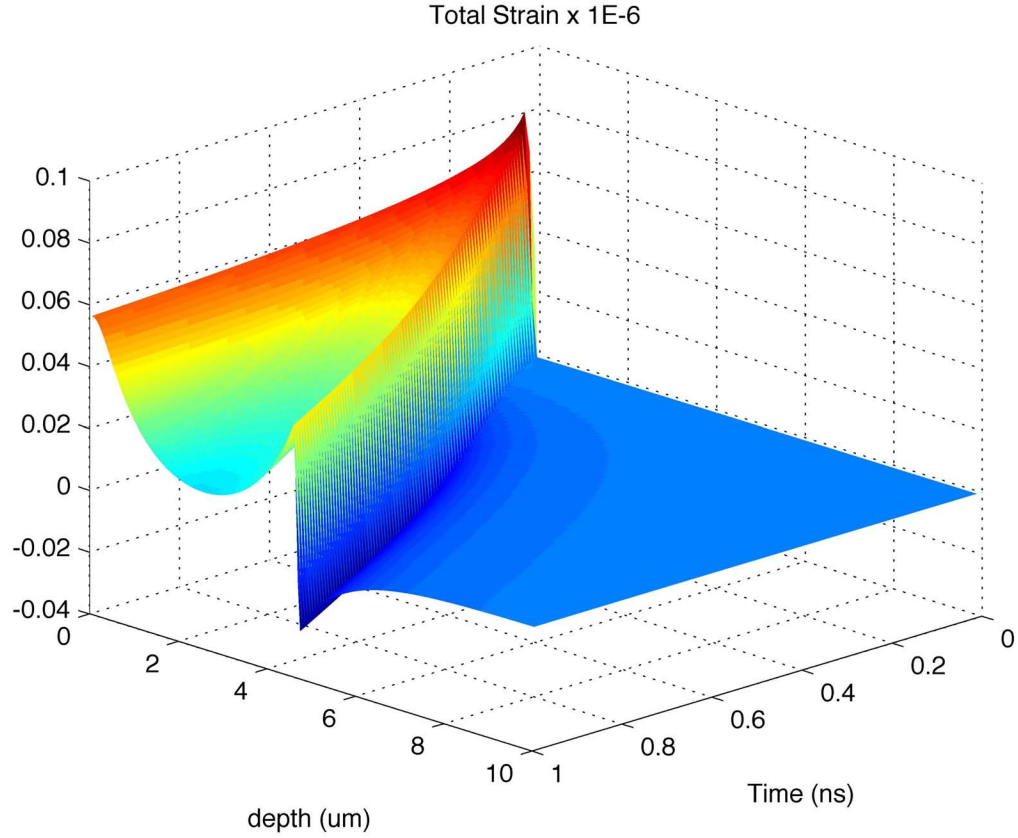


Figure 2.8: The absorption of energy at the surface of the crystal launches an acoustic bipolar impulse through the depth of the material. The Auger recombination and electron diffusion drive the wave, decreasing the deformation potential. This serves to balance the symmetry of the traveling wave. At 1 ns, the wave looks very similar to the Thomsen model since a large number of the electrons have been recombined. The thermal diffusion can be seen at the surface layer with an long-lived exponential decay.

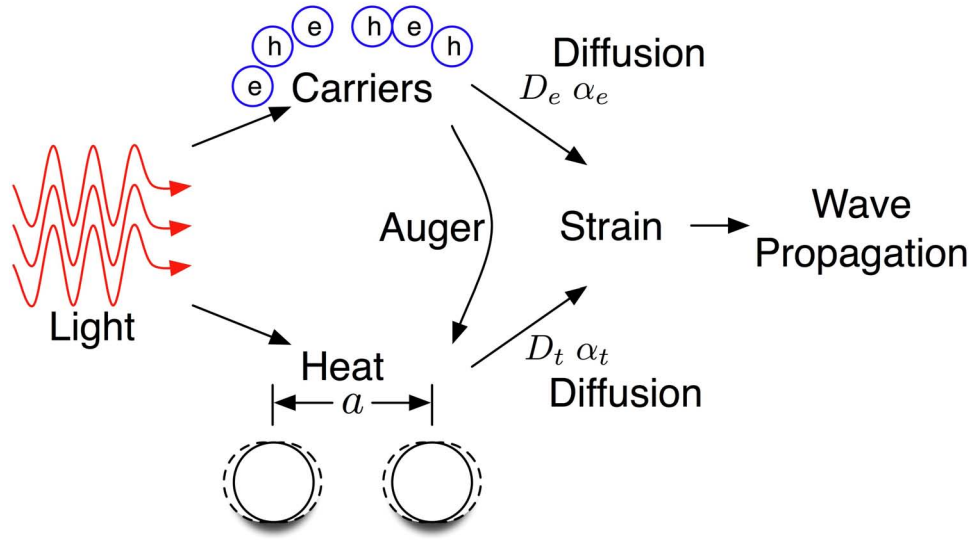


Figure 2.9: The evolution of ultrafast excitation involves several processes: carrier production, recombination, and thermal vibrations. These deform the lattice structure, producing strain which then propagates into the crystal.

where carriers and temperature continuously diffuse into the bulk material. These processes are illustrated schematically in Figure 2.9.

CHAPTER III

X-ray Diffraction in Ideal Crystals

In 1895 Wilhelm Rontgen demonstrated that x-rays had properties unlike visible light after producing the first x-ray radiograph showing the hand of his wife. In the years prior to this discovery the group theory of crystals had been published and, in 1912, M. von Laue proposed using crystals as a natural diffraction grating. He showed experimentally that crystals generated an interference pattern analogous to a periodic three-dimensional diffraction grating. In 1914, he received the Nobel Prize in Physics for his work in crystals. Immediately following, the father and son team of W.H. Bragg and W.L. Bragg proposed a different geometry with superior experimental techniques to probe the structure of crystals, work that won them the Nobel Prize in 1915. These inaugural experiments laid the foundation for the study of structure at atomic length scales.

This chapter will explore the theory of x-ray diffraction. The discussion is limited to perfect crystals, giving an overview of diffraction by x-rays in the Bragg geometry. A more thorough discussion of space groups, imperfect crystals, and other geometries is presented in Warren and Zachariasen [15, 16].

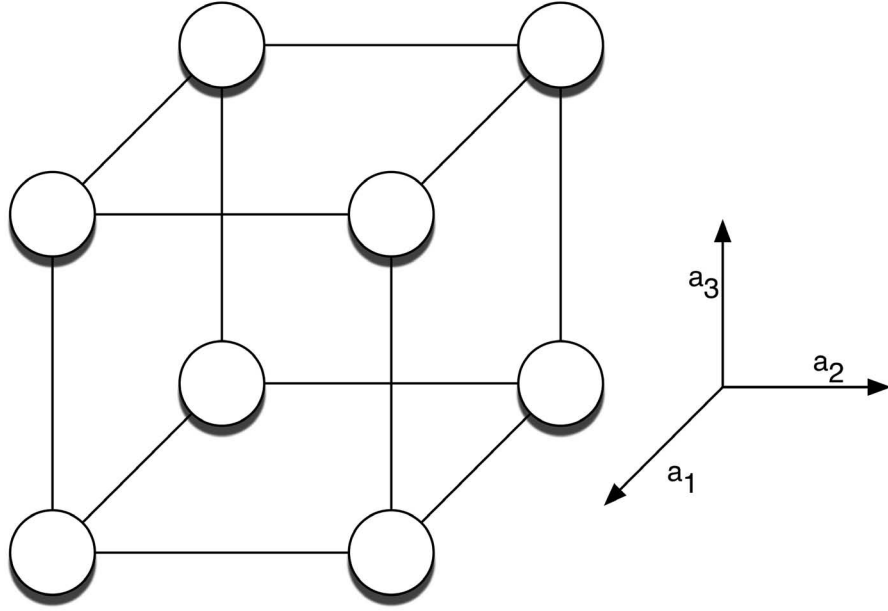


Figure 3.1: Three Dimensional representation of the unit cell defined by the crystal axis $\mathbf{a}_1\mathbf{a}_2\mathbf{a}_3$.

3.1 X-ray Diffraction

Diffraction is the process by which light produces an interference pattern after passing through a narrow aperture or sharp edge. As Laue showed, the periodic structure of crystals produces interference patterns similar to that of a grating. The basis for the first order solution to crystalline diffraction is based on Laue's assumption of the diffraction grating model. This method is commonly referred to as the wave kinematical diffraction theory. The diffraction grating condition requires the product of the distance between slits and the change in wave vector, $\Delta\mathbf{k}$, between the diffracted and incident beam, \mathbf{k}_H and \mathbf{k}_0) respectively, be of integer value. The wave vectors are of equal magnitude $|\mathbf{k}_H| = |\mathbf{k}_0|$ and are defined along the unit vector of the incident and diffracted directions, $\mathbf{u}_{0,H}$ where $\mathbf{k}_{0,H} \equiv \frac{1}{\lambda}\mathbf{u}_{0,H}$ and λ is the wavelength of the

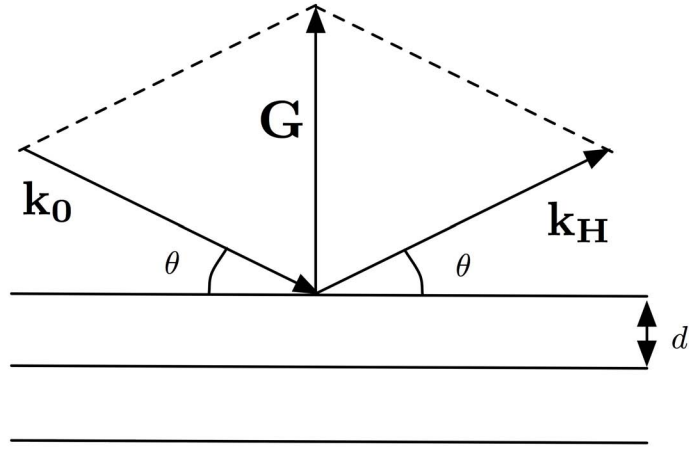


Figure 3.2: Relations involved in the vector representation of diffraction.

incident beam. The diffraction condition is

$$\mathbf{a}_i \cdot (\mathbf{k}_{H_i} - \mathbf{k}_0) = H_i \quad (3.1)$$

where H_i is an integer, \mathbf{a}_i is the unit cell axis vector describing the periodicity of the crystal and measuring the separation of neighboring equivalent points. Each of these terms are indexed over three spatial coordinates where $i = 1, 2, 3$. It is then possible to describe any vector in the lattice by

$$\mathbf{r}_i = x_i \mathbf{a}_i + y_i \mathbf{a}_i + z_i \mathbf{a}_i. \quad (3.2)$$

where $0 \leq x_i, y_i, z_i \leq 1$. In three-space Equation 3.1 is known as the Laue vector equations and express the conditions to produce diffraction maxima.

It is convenient to express the unit cell geometry in reciprocal space. Defining the unit reciprocal lattice vector, \mathbf{G} , (see Figure 3.2) corresponding to an allowed reflection,

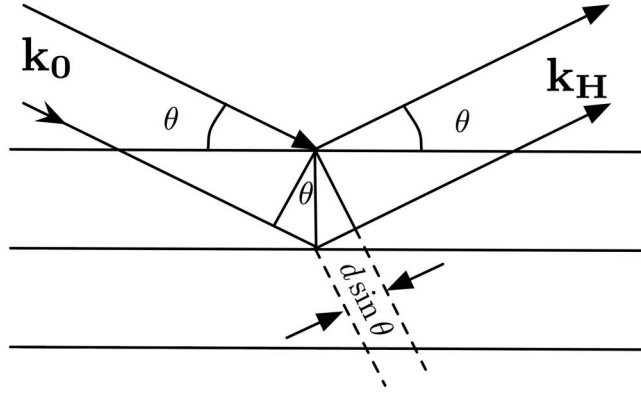


Figure 3.3: Vector representation of the Bragg Law.

$$\mathbf{G} = H_1 \mathbf{b}_1 + H_2 \mathbf{b}_2 + H_3 \mathbf{b}_3 \quad (3.3)$$

with \mathbf{b}_i being the reciprocal vector set of \mathbf{a}_i :

$$\mathbf{b}_1 = \frac{\mathbf{a}_2 \times \mathbf{a}_3}{\mathbf{a}_1 \cdot \mathbf{a}_2 \times \mathbf{a}_3} \quad (3.4)$$

$$\mathbf{b}_2 = \frac{\mathbf{a}_3 \times \mathbf{a}_1}{\mathbf{a}_1 \cdot \mathbf{a}_2 \times \mathbf{a}_3} \quad (3.5)$$

$$\mathbf{b}_3 = \frac{\mathbf{a}_1 \times \mathbf{a}_2}{\mathbf{a}_1 \cdot \mathbf{a}_2 \times \mathbf{a}_3} \quad (3.6)$$

where \mathbf{a}, \mathbf{b} have the property $\mathbf{b}_i \cdot \mathbf{a}_j = \delta_{ij}$. By construction, the reciprocal lattice vector \mathbf{G} is the difference in wave vectors of the incident and diffracted waves. This difference is also called the scattering vector, $\Delta \mathbf{k}$, where $\mathbf{G} = \mathbf{k}_H - \mathbf{k}_0 = \Delta \mathbf{k}$. If the scattering vector deviates from the Laue conditions, the diffraction pattern does not produce constructive interference. That is, if the coefficients of the Laue condition, H_i , of the reciprocal lattice vector are not integers, there is no diffraction maxima. The set H_i is also known as the Miller indices hkl . The integers hkl define \mathbf{G} to a

reciprocal lattice plane such that the distance normal between two planes is parallel to the vector set \mathbf{a}_i by construction. The distance d of the interplanar spacing is given by $d = \hat{\mathbf{n}} \cdot \mathbf{a}_i / H_i = 1/|\mathbf{G}|$, where $\hat{\mathbf{n}} = \mathbf{G}/|\mathbf{G}|$. The Laue equations can then be written as

$$\mathbf{a}_1 \cdot \mathbf{G} = h, \quad \mathbf{a}_2 \cdot \mathbf{G} = k, \quad \mathbf{a}_3 \cdot \mathbf{G} = l. \quad (3.7)$$

From simple geometry (Figure 3.3), the path difference between the incident and diffracted wave vectors is $2 \sin(\theta)/\lambda$. Combining this with the definition of the scattering vector $\Delta \mathbf{k} = \mathbf{G} = 1/d$, the Bragg law is derived:

$$|\mathbf{k}_H - \mathbf{k}_0| = |\mathbf{G}| \Rightarrow 2 \sin(\theta_B)/\lambda = \frac{1}{d} \quad (3.8)$$

where the subscript B denotes a Bragg reflection.

3.2 The Structure Factor

When a plane wave is incident on a group of electrons, classical and quantum scattering theory allows for two scattering phenomena: inelastic and elastic scattering. Compton scattering is an inelastic process wherein some energy is imparted on an electron and diffracted radiation is Compton shifted to a longer wavelength. The inelastic scattering is incoherent in nature and represents the sum of intensities of scattering from individual atoms comprising the lattice. Since this scattering is both incoherent and independent of short and long-range order, it does not provide insight to diffraction at the Bragg peak and therefore to this discussion. The coherent, elastically scattered radiation, however, gives rise to interference and Bragg diffraction.

To calculate the unmodified scattering from the crystal, the charge density, ρ , in a volume dV must be assessed where the integral over the entire volume evaluates to a single electron, $\int \rho dV = 1$. The scattering amplitude from an electron is the volume integral of the charge density and the phase difference between the radiation scattered by the j th electron and the electron at the origin ($\mathbf{G} \cdot \mathbf{r}_j$),

$$f_0 = \int \rho e^{2\pi i \mathbf{G} \cdot \mathbf{r}_j} dV. \quad (3.9)$$

This phase term must be included because x-ray wavelengths are comparable to the distance between electrons. For any atom, the scattering power f_0 is a function of the radial dependence of the electrons, so that at small values of $\sin \theta / \lambda$, f_0 approaches Z , the number of electrons in the atom. The electron distribution can be calculated using the Hartree-Fock method [17].

The atomic scattering power, f_0 , correctly describes the scattering amplitude from a free electron (a Thomson scattering event). If the case of a scattering event from a group of bound electrons — such as in a crystal — is considered, the scattering amplitude from a unit cell must be evaluated. The scattering power of the unit cell, F_0 , replaces f_0 where the electron distribution function of the crystal lattice, Ω , replaces ρ , where

$$F_0 = \int \Omega e^{2\pi i \mathbf{G} \cdot \mathbf{r}_j}. \quad (3.10)$$

The function Ω can be found by superimposing the contributions from all electron

distributions throughout the crystal lattice,

$$\Omega(\mathbf{r}) = \sum_k \rho_k(\mathbf{r} - \mathbf{r}_k) \quad (3.11)$$

where \mathbf{r}_k is the direction from the origin to the k th atom. It should be noted that ρ_k is not the same electron distribution of Equation 3.9 where ρ was the distribution from an atom in free space. In this case, the atoms are bound together (binding energy is non-zero) and this assumption is no longer valid. Furthermore, Equation 3.9 uses a classical view of the electron cloud. To fully account for all quantum effects, this picture must be replaced with a continuous band of virtual classical oscillators. The result of this correctly accounts for the cases with non-negligible anomalous dispersion, for which the index of refraction decreases with increasing frequency of the incident light. It is therefore necessary to label the scattering amplitudes f_0 and F_0 for which anomalous dispersion is not taken into account and where the subscripts are dropped for the cases when the dispersion corrections are included. It should be noted that it is common to see the scattering power of the unit cell referred to as the *structure factor* in many references. A more detailed theory of dispersion corrections is given in Zachariasen and Cromer [16, 17].

Quantitatively, the geometric part of the form factor, f_0 , is calculated using the theoretical work of D. T. Cromer and J. B. Mann, to produce a set of nine coefficients (the Cromer-Mann coefficients) in a parameterization for neutral atoms given by

$$f_0 = \sum_{i=1}^4 a_i e^{-b_i(\sin \theta_B / \lambda)^2} + c \quad (3.12)$$

which is valid for values of $0 \leq (\sin \theta_B) / \lambda \leq 2.0 \text{ \AA}^{-1}$ and shown in Figure 3.4 [17].

The coefficients are listed in Table 3.1 for arsenide, gallium, indium, and antimony.

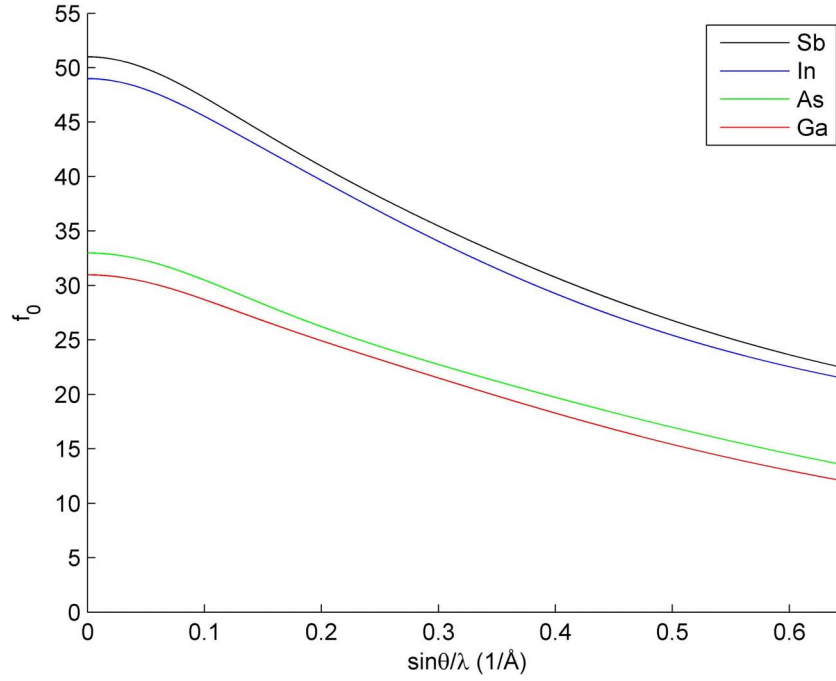


Figure 3.4: Non-Dispersive part of the atomic scattering factor for antimony, indium, arsenic, and gallium. Calculated using Cromer-Mann coefficients and Equation 3.12 [17].

The dispersion corrections, $\Delta f'$ and $\Delta f''$, are small and are expressed by

$$f = f_0 + \Delta f' + i\Delta f'' \quad (3.13)$$

where the imaginary part $\Delta f''$ represents a phase shift in the scattered radiation. This term will be important when analyzing the Bragg peak shapes. Since these corrections are a result of dispersion theory, they are dependent only on the frequency of the incident radiation and are independent of radial distribution or geometry of the given crystal.

The most drastic effects of anomalous dispersion manifest near or at an absorption edge, where the experimental uncertainty of these values are up to 15 - 20% very

Element	a_1	a_2	a_3	a_4	b_1	b_2	b_3	b_4	c
As	16.672	6.070	3.431	4.278	2.635	0.265	12.948	47.797	2.531
Ga	15.235	6.701	4.359	2.962	3.067	0.241	10.781	61.414	1.719
In	19.162	18.560	4.295	2.040	0.548	6.378	25.850	92.803	4.939
Sb	19.642	19.045	5.037	2.683	5.303	0.461	27.907	75.283	4.591

Table 3.1: Cromer-Mann coefficients for the geometric component of the atomic scattering form factor [17, 18].

near strong edges compared to $\leq 1\%$ uncertainty away from the absorption edges. Appropriate care must be taken around these absorption edges due to the discontinuities and singularities in the data (Figure 3.5). The dispersion corrections used to find the intensities of reflections are found experimentally and have been synthesized by Henke *et al.* [19]. In recent years, a database of these terms, collectively known as the *atomic form factors*, was created by the National Institute of Standards and Measures (NIST) [18]. By interpolating between data points, $\Delta f'$ and $\Delta f''$ can be estimated for any x-ray energy. The dispersion correction terms for arsenide, gallium, indium, and antimony are given in Table 3.2.

Correction	8 keV	9 keV	10 keV	11 keV	12 keV	13 keV
$\Delta f'_{As}$	-0.9136	-1.1922	-1.56186	-2.22129	-3.81902	-1.39895
$\Delta f''_{As}$	1.0169	0.82289	0.68078	0.57293	3.77479	3.21842
$\Delta f'_{Ga}$	-1.2629	-1.7348	-2.91219	-1.9114	-0.91121	-0.49946
$\Delta f''_{Ga}$	0.7857	0.63486	0.52471	3.45019	2.95286	2.61959
$\Delta f'_{In}$	0.1054	0.12455	0.07209	-0.01454	-0.11575	-0.22375
$\Delta f''_{In}$	5.0981	4.1778	3.49162	2.96388	2.54878	2.21616
$\Delta f'_{Sb}$	-0.0312	0.08996	0.09868	0.04877	-0.02907	-0.11992
$\Delta f''_{Sb}$	5.9588	4.8901	4.09321	3.47929	2.99569	2.60756

Table 3.2: Dispersion correction terms at several energies [18].

Recalling Equation 3.10 and accounting for the dispersion corrections, the struc-

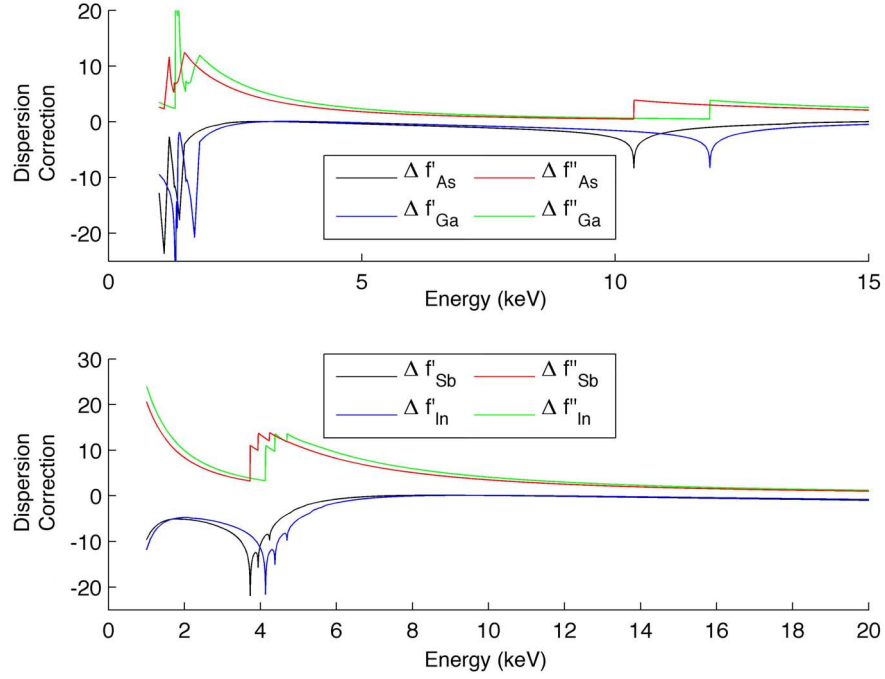


Figure 3.5: Dispersion Corrections $\Delta f'$ and $\Delta f''$ for antimony, indium, arsenic, and gallium. Data from NIST Atomic Form Factor database [18].

ture factor becomes the sum over the atoms in the unit cell,

$$F = \sum_k (f_k + \Delta f'_k + i\Delta f''_k) e^{2\pi i \mathbf{G} \cdot \mathbf{r}} \quad (3.14)$$

where F is now complex and can be written $F = F' + iF''$. The phase factor can be expanded into the unit cell and reciprocal lattice vectors, \mathbf{a}_i and \mathbf{b}_i respectively, where $\mathbf{G} \cdot \mathbf{r} = (h\mathbf{b}_1 + k\mathbf{b}_2 + l\mathbf{b}_3) \cdot (x_k\mathbf{a}_1 + y_k\mathbf{a}_2 + z_k\mathbf{a}_3)$ so that

$$F_{hkl} = \sum_k f_k e^{2\pi i (h\mathbf{b}_1 + k\mathbf{b}_2 + l\mathbf{b}_3) \cdot (x_k\mathbf{a}_1 + y_k\mathbf{a}_2 + z_k\mathbf{a}_3)} = \sum_k f_k e^{2\pi i (hx_k + ky_k + lz_k)} \quad (3.15)$$

where x_k, y_k, z_k are the fractional coordinates defined by the Bravais lattice.

For the case of a simple cubic, the lattice basis has a single atom per unit cell

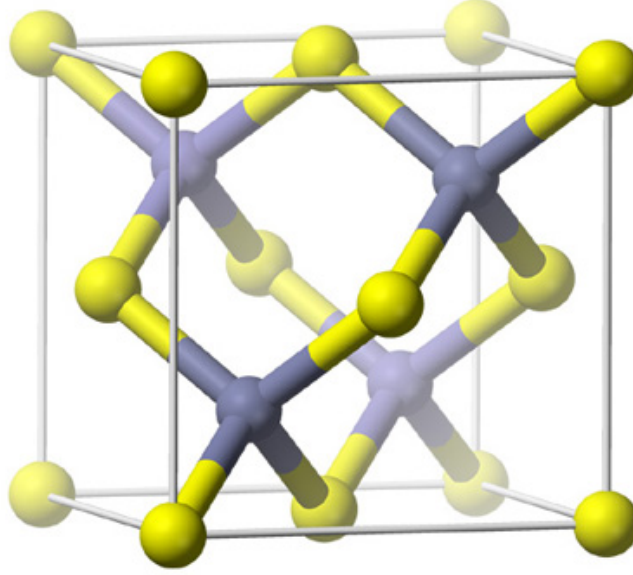


Figure 3.6: Model of the zinc blende unit cell. The diamond formation is that of the zinc blende where all atoms are identical [20].

located at the origin, or a fractional coordinates of $(0,0,0)$. Plugging this into Equation 3.15, $F_{hkl} = f$. For a body-centered cubic (BCC) of a single element, the lattice contains two atoms with fractional coordinates $(0,0,0)$ and $(\frac{1}{2}, \frac{1}{2}, \frac{1}{2})$ giving $F_{hkl} = f[1 + e^{2\pi i(h+k+l)}]$. The zinc blende structure, shown in Figure 3.6, is the Bravais lattice of GaAs and InSb and contains eight atoms per unit cell. For GaAs, the unit cell contains 4 gallium atoms and 4 arsenic atoms with fractional coordinates shown in Table 3.3.

	0	0	0		$\frac{1}{4}$	$\frac{1}{4}$	$\frac{1}{4}$
	$\frac{1}{2}$	$\frac{1}{2}$	0		$\frac{3}{4}$	$\frac{3}{4}$	$\frac{1}{4}$
Ga	$\frac{1}{2}$	0	$\frac{1}{2}$	As	$\frac{3}{4}$	$\frac{1}{4}$	$\frac{3}{4}$
	0	$\frac{1}{2}$	$\frac{1}{2}$		$\frac{1}{4}$	$\frac{3}{4}$	$\frac{3}{4}$

Table 3.3: Fractional lattice coordinates for GaAs in a zinc blende structure

The choice of atomic origin is arbitrary so that f_{Ga} and f_{As} are interchangeable.

Plugging these coordinates in for x_k, y_k, z_k in Equation 3.15, the structure factor becomes

$$F_{hkl} = f_{Ga}[e^{2\pi i(0)} + e^{\pi i(h+k)} + e^{\pi i(h+l)} + e^{\pi i(k+l)}] \\ + f_{As}[e^{\frac{1}{2}\pi i(h+k+l)} + e^{\frac{1}{2}\pi i(3h+3k+l)} + e^{\frac{1}{2}\pi i(3h+k+3l)} + e^{\frac{1}{2}\pi i(h+3k+3l)}].$$

F_{hkl} vanishes for terms where h, k, l are of differing parities. For those reflections [(100), (210), (312), etc...] the scattering power is zero and the reflections are forbidden. The allowed reflections of the zinc-blende or diamond lattice has values of h, k, l which are all even or all odd [(111), (200), (220), etc...]. The structure factor of allowed reflections reduces to

$$F_{hkl} = 4 \left[f_{Ga} + f_{As} e^{\frac{1}{2}\pi i(h+k+l)} \right]. \quad (3.16)$$

The diffracted scattering power, F_H is compared to the incident power, F_0 to find the relative refracted intensity where in the Miller formulation, $F_0 = F_{000}$, and is the structure factor for the incident wave.

Energy (keV)	$F_{000}(\text{InSb})$	$F_{400}(\text{InSb})$	$F_{000}(\text{GaAs})$	$F_{400}(\text{GaAs})$
8	400.27 - 44.23 <i>i</i>	260.35 - 41.92 <i>i</i>	247.13 - 7.21 <i>i</i>	149.14 - 6.96 <i>i</i>
9	400.83 - 36.27 <i>i</i>	260.88 - 34.38 <i>i</i>	244.12 - 5.83 <i>i</i>	146.25 - 5.63 <i>i</i>
10	400.66 - 30.34 <i>i</i>	260.72 - 28.75 <i>i</i>	237.94 - 4.82 <i>i</i>	140.28 - 4.65 <i>i</i>
11	400.11 - 25.77 <i>i</i>	260.20 - 24.43 <i>i</i>	239.30 - 16.09 <i>i</i>	141.58 - 15.50 <i>i</i>
12	399.40 - 22.18 <i>i</i>	259.52 - 21.02 <i>i</i>	236.91 - 26.91 <i>i</i>	139.25 - 25.98 <i>i</i>
13	398.60 - 19.30 <i>i</i>	258.77 - 18.29 <i>i</i>	248.24 - 23.35 <i>i</i>	150.20 - 22.54 <i>i</i>

Table 3.4: Structure factors for the (400) reflection at various energies for InSb and GaAs.

The effect of thermal vibrations in this discussion has so far been omitted. If, as a result of thermal vibrations, the lattice experiences large deviations from equilibrium

positions, atoms spend more time in the higher intensity wave field of the x-rays, leading to higher absorption. To account for this additional attenuation, the atomic scattering factor f_k is replaced by $f_k e^{-M_k}$ where M_k is the Debye-Waller factor for the k th atom. This is calculated from the average atomic displacement from equilibrium position, $\langle u_k^2 \rangle$, by

$$M_k = 8\pi^2 \langle u_k^2 \rangle \left(\frac{\sin^2 \theta}{\lambda} \right)^2. \quad (3.17)$$

The Debye-Waller factor reduces the magnitude of structure factor, attenuating the diffracted intensity, as well as reduces the width of the diffraction peak. A summary of the atomic displacements is given in Table 3.5 which shows the temperature dependence. The effect of the Debye-Waller factor is more easily seen at high temperatures and high reflection angles.

Material	Element	100 K	200 K	400 K	600 K	800 K
InSb	In	0.006102	0.011711	0.023163	0.034671	0.046194
	Sb	0.005274	0.010085	0.019926	0.029821	0.039728
GaAs	Ga	0.003397	0.006038	0.011658	0.017368	0.023101
	As	0.002949	0.005201	0.010014	0.014909	0.019827

Table 3.5: Average atomic displacements for InSb and GaAs at various temperatures. Values shown in \AA^2 . Table adapted from [21].

3.3 Kinematic Diffraction

In the above sections, the scattering amplitude from a single atom and a unit cell was derived. The results from a unit cell must be extrapolated to estimate the diffracted intensity of a small crystal. To find the scattering amplitude for the entire crystal, a first order approximation might simply be to superimpose the contributions

of each unit cell across the entire crystal, with proper handling of the phase differences. The location of any unit cell from the origin can be found by the unit vector $\mathbf{A}_L = L_1\mathbf{a}_1 + L_2\mathbf{a}_2 + L_3\mathbf{a}_3$ where L_i is the lattice parameters for the associated directions $\hat{\mathbf{a}}_i$. The total scattering amplitude from a single unit cell located at \mathbf{A}_L is $F e^{2\pi i \mathbf{G} \cdot \mathbf{A}_L}$, where the phase difference is with respect to the unit cell at the origin. The total diffracted amplitude across all unit cells becomes

$$E_H = E_0 F \sum_L e^{2\pi i \mathbf{G} \cdot \mathbf{A}_L} \quad (3.18)$$

and $E_{0,H}$ is the incident and diffracted electric field amplitude. Expanding the summation, assuming $N_1 N_2 N_3 = N$ is the total number of unit cells

$$\sum_L e^{2\pi i \mathbf{G} \cdot \mathbf{A}_L} = \sum_0^{N_1-1} e^{2\pi i L_1 \mathbf{G} \cdot \mathbf{a}_1} \sum_0^{N_2-1} e^{2\pi i L_2 \mathbf{G} \cdot \mathbf{a}_2} \sum_0^{N_3-1} e^{2\pi i L_3 \mathbf{G} \cdot \mathbf{a}_3} \quad (3.19)$$

which can be reduced to the form

$$\frac{E_H}{E_0} = F \prod_i \frac{e^{2\pi i N_i \mathbf{G} \cdot \mathbf{a}_i} - 1}{e^{2\pi i \mathbf{G} \cdot \mathbf{a}_i} - 1}. \quad (3.20)$$

Finally the fractional reflected intensity, I_H/I_0 , is found by multiplying the ratio of the amplitudes with its complex conjugate to give

$$\frac{I_H}{I_0} = |F|^2 \prod_i \frac{\sin^2(\pi N_i \mathbf{G} \cdot \mathbf{a}_i) - 1}{\sin^2(\pi \mathbf{G} \cdot \mathbf{a}_i) - 1}. \quad (3.21)$$

When the Laue condition (Equation 3.7) is satisfied, the scattering intensity reduces to

$$I_H = I_0 |F|^2 N^2 \quad (3.22)$$

This approach to solving for the scattering intensity has several assumptions that allow it to be an excellent first order approximation to perfect crystal reflections and serves as a good estimate for small, mosaic, or highly imperfect crystals. That is to say, this method is only acceptable for crystals comprised of a small number of unit cells, crystals that maintain short range order but not long range, or crystals with defects.

The obvious omission to this derivation is absorption. Two types of absorption occur in the crystal. In the first type, incident photons suffer true absorption through the photoelectric effect where electrons absorb energy and are promoted to a different band or ejected from the atom. Quantitatively, normal absorption is described through

$$\mu_n = \left(\frac{e^2}{mc^2} \right) \left(\frac{\lambda}{2\pi\epsilon_0 V} \right) F'' \quad (3.23)$$

where, again, F'' is the imaginary part of the structure factor in Equation 3.14, e and m are the charge and mass of an electron, c is the speed of light, ϵ_0 is the permittivity of free space, and V is the unit cell volume. Absorption along any other direction has a smaller coefficient since the absorption only depends on the depth from the surface where in a direction θ from the normal, $\mu_\theta = \mu_n \cos(\theta)$. The quantity μ is the fractional intensity decrease in the intensity per unit length where this absorption

obeys the Beer-Lambert Law,

$$I(z) = I_0 e^{-\mu z} \quad (3.24)$$

for any depth z . The theory presented above can be easily corrected for normal absorption by including $e^{-\mu z}$ to Equation 3.21.

In the second type of absorption, the incident beam interacts with the diffracted beam in a process known as extinction. This interference only occurs when the Laue condition is satisfied. Extinction can not be easily accounted for in the kinematical diffraction theory of Equation 3.21 and a new theory is necessary to accurately describe this physical process. This new theory is required to include the mutual dependencies of the incident and diffracted beams by creating a coupled system. This is done by modeling the interaction as coupled coherent oscillators and for this reason, is known as the dynamical theory of x-ray diffraction.

3.4 Dynamical Diffraction

The theory of kinematic diffraction makes an assumption that each unit cell of the crystal is independent of each other. To correct for this inaccuracy, the theory of dynamical diffraction was developed first by C. G. Darwin in 1914, and in a different formulation by P. P. Ewald in 1916. The theory has been updated and improved by many others, yet the greatest contribution was by M. Von Laue in which Maxwell's equations for a periodic complex dielectric constant were solved. In the Laue description, the wave field inside the crystal is considered as a single entity where the incident and diffracted beams coherently interact and energy is exchanged between the two (see Figure 3.7). It should be said that all three formulations are correct,

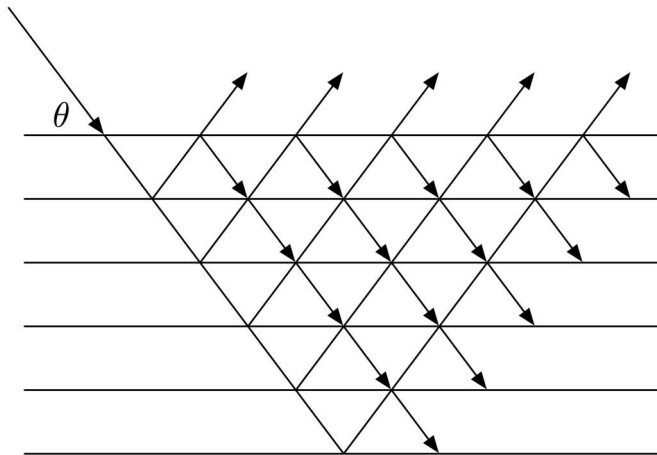


Figure 3.7: Dynamical diffraction illustration where incident and diffracted beams create a coupled system.

however the effects of absorption are implicitly included in Ewald and Laue. The discussion presented here only reviews the Bragg case of dynamical diffraction. A study of the Laue diffraction case¹ is given in Batterman and Cole [22].

According to the Darwin case — that is, no absorption ($\text{Im}(F_{hkl}) = F''_{hkl} = 0$) — the peak has a region of total reflection where $|I_H/I_0| = 1$ (blue curve in Figure 3.8). In 1930, J. A. Prins adapted this work to naturally include absorption through the structure factor. The complex structure factor works to reduce the reflection intensity across the region of total reflection, yet more importantly, includes the asymmetry of the reflection (red curve in Figure 3.8). In general, the attenuation due to extinction (negative interference) is many times greater than that produced by true absorption. To physically explain extinction, the most intuitive approach is the wave field treatment. At the surface, the wave nodes are located at the atomic plane, at the low-angle side of the reflection. As the incident angle increases, the nodes move linearly with angle until the atoms rest on the antinodal plane at the high-angle side

¹Laue diffraction uses a different geometry than Bragg diffraction and uses non-monochromatic x-rays to gain information on atomic structure.

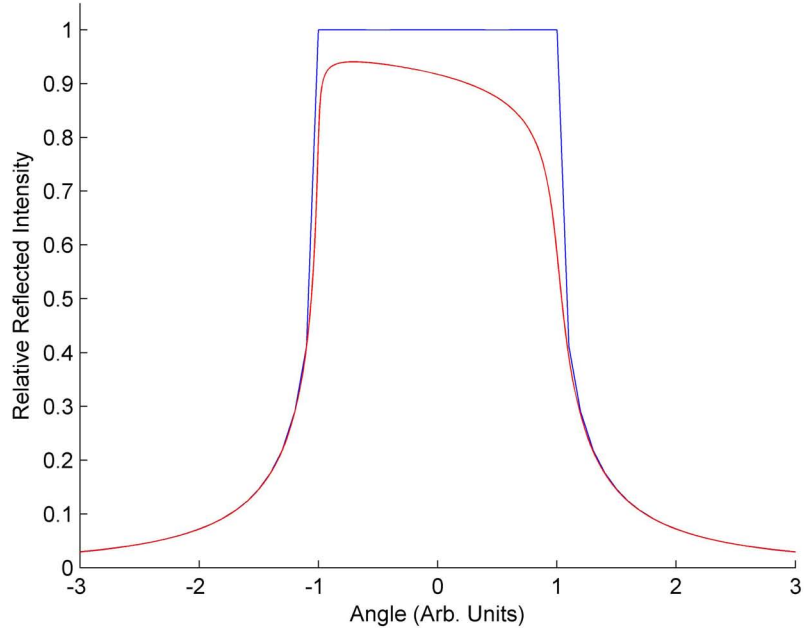


Figure 3.8: Darwin (blue) and Darwin-Prins (red) rocking curves.

of the reflection range. As the atoms move into the higher amplitude wave field, the absorption contribution increases from each particle, giving rise to an asymmetric pattern. A cartoon of this shift is presented in Figure 3.9.

Another great advance to the efforts of this field came in 1962 and 1964 respectively, when S. Takagi and D. Taupin independently developed a dynamical theory which can be applied to a distorted or strained crystal [24, 25]. This theory removed any condition on thin crystals or small Bragg angles, treating the entire bulk as does the Laue formulation for the unstrained case by directly solving Maxwell's equations. The Takagi-Taupin equation is

$$\begin{aligned} i\frac{\lambda}{\pi}\boldsymbol{\beta}_0 \cdot \nabla \mathbf{D}_0(r) &= \psi_0 \mathbf{D}_0(r) + \psi_H \mathbf{D}_H(r) \\ i\frac{\lambda}{\pi}\boldsymbol{\beta}_H \cdot \nabla \mathbf{D}_H(r) &= \psi_0 \mathbf{D}_H(r) + \psi_H \mathbf{D}_0(r) - \alpha_H \mathbf{D}_H(r) \end{aligned} \quad (3.25)$$

where the parameters are given in Table 3.6. The Takagi-Taupin equation expresses

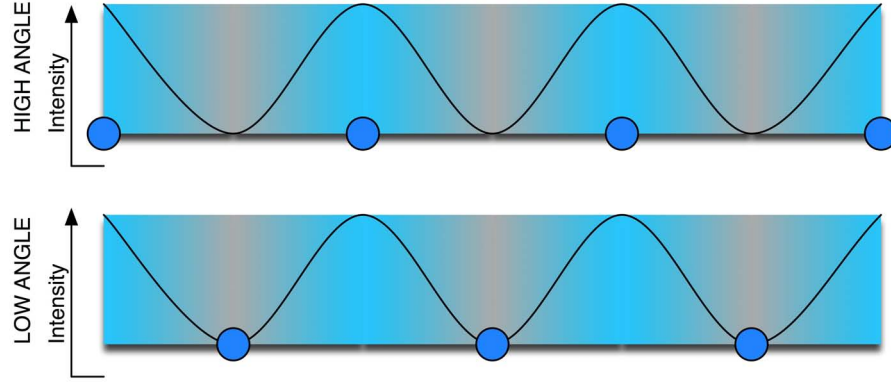


Figure 3.9: As the wave field moves from atoms residing at field nodes (lower figure) to having atoms at antinodes (upper figure), the absorption from an atom increases producing an asymmetric Bragg diffraction pattern. Figure adapted from [23].

the variation in the complex wave amplitudes in the incident and diffracted directions (\mathbf{r}). In 1986, C. R. Wie published a method to incorporate depth-dependent strain for an arbitrarily thick crystal [26]. This method builds on the Takagi-Taupin equation and has been indispensable when modeling Bragg diffraction from strained crystals [1, 4–7, 14, 27].

3.5 Numerical Modeling

The Wie method begins at the infinite atomic plane and calculates the rocking curve for the unstrained case, or the infinite crystal solution. At each depth iteration, the rocking curve is again calculated where the top layer solution is the fully strained case and comparable to diffraction data. The implementation of this method is most efficiently done by using the inner loop to iterate depth and the outer to iterate angle. The set of parameters shown in Table 3.6 are necessary for the Wie method [26, 28].

For F_H , the term in the exponential ($\exp[-(8\pi^2 \sin^2 \theta_B / \lambda^2) u^2]$) is the Debye-Waller factor from Equation 3.17 and can be taken into account when the structure

Wave Vectors:	$\beta_{0,H}$
Complex Wave Amplitudes:	$\mathbf{D}_{0,H}(r)$
Polarizability per Unit Volume:	$\psi_{0,H} = -(e^2/mc^2)(\lambda^2/\pi^2)(F_{0,H}/V)(1/4\pi\epsilon_0)$ $\psi_{0,H} = \psi'_{0,H} + i\psi''_{0,H}$
Structure Factor:	$F_0 = F_{000}$ and $F_H = F_{hkl}$
Unit Cell Volume:	V
Normalized Depth:	$A = z\pi \psi'_H /\lambda\sqrt{\gamma_0\gamma_H}$
Depth inside the crystal:	z
Direction of Cosines:	$\gamma_{0,H}, b = \gamma_0/\gamma_H = 1$ for symm. reflections
Incident Absorption Parameter:	$g = (1+b)\psi''_0$
Diffacted Absorption Parameter:	$k = \psi''_H/\psi'_H$
Deviation from Bragg Angle:	$y = [(1+b)\psi'_0 - b\alpha_H]/(2 \psi'_H \sqrt{b})$
Displaced Structure Factor:	$F_H = F_H^0 \exp[-(8\pi^2 \sin^2 \theta_B/\lambda^2)u^2]$
Average Atomic Displacement:	u
Angle of Reflection:	$\alpha_H = -2(\theta - \theta_B) \sin 2\theta_B - (c_1\epsilon_1 + c_2\epsilon_2)$
Strain Perpendicular to Surface:	ϵ_1
Strain Parallel to Surface:	ϵ_2
Strain Strength:	$c_1 = 2 \sin \theta_B [\cos^2 \phi \tan \theta_B \pm \sin \phi \cos \phi]$
($\phi = 0$ for all symmetric bragg cases)	$c_2 = 2 \sin \theta_B [\sin^2 \phi \tan \theta_B \mp \sin \phi \cos \phi]$

Table 3.6: List of parameters for the Wie method of calculating rocking curves.

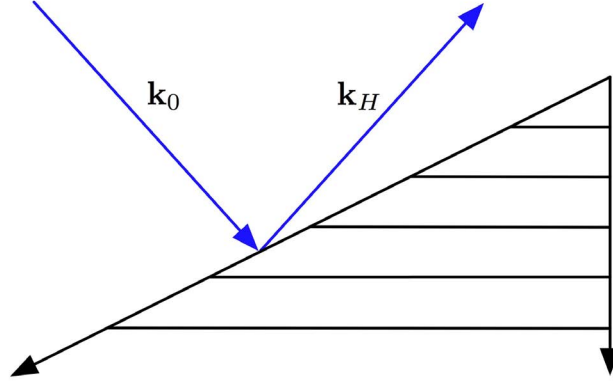


Figure 3.10: Example of an asymmetric Bragg reflection on a crystal cut such that the angle between the surface and reflecting plane is nonzero.

factor is calculated. The direction of cosines term b is to account for asymmetric Bragg reflections, where the crystal has not been oriented or cleaved along an atomic plane, in a geometry similar to Figure 3.10.

The scattering amplitude is given by the differential equation

$$i \frac{dX}{dA} = (1 + ik)X^2 - 2(y + ig)X + (1 + ik) \quad (3.26)$$

where $X = \sqrt{b} \frac{\mathbf{D}_H(r)}{\mathbf{D}_0(r)}$ is the scattering amplitude. Analytically integrating Equation 3.26 provides the iterative Wie solution,

$$X_{n+1}(A_{n,n-1}) = \frac{sX_{n-1} + i(B + CX_{n-1}) \tan[s(A_n - A_{n-1})]}{s - i(C + BX_{n-1}) \tan[s(A_n - A_{n-1})]}, \quad (3.27)$$

where A is dependent on the depth from the surface z , $B = -(1 + ik)$, $C = y + ig$, and $s = \sqrt{C^2 + B^2}$. A_0 is defined as the infinite crystal depth. The term s is not straight forward as it involves the square root of a complex number which must be carefully treated [26]. The notation of Equation 3.27 differs from that in Reference [26] where

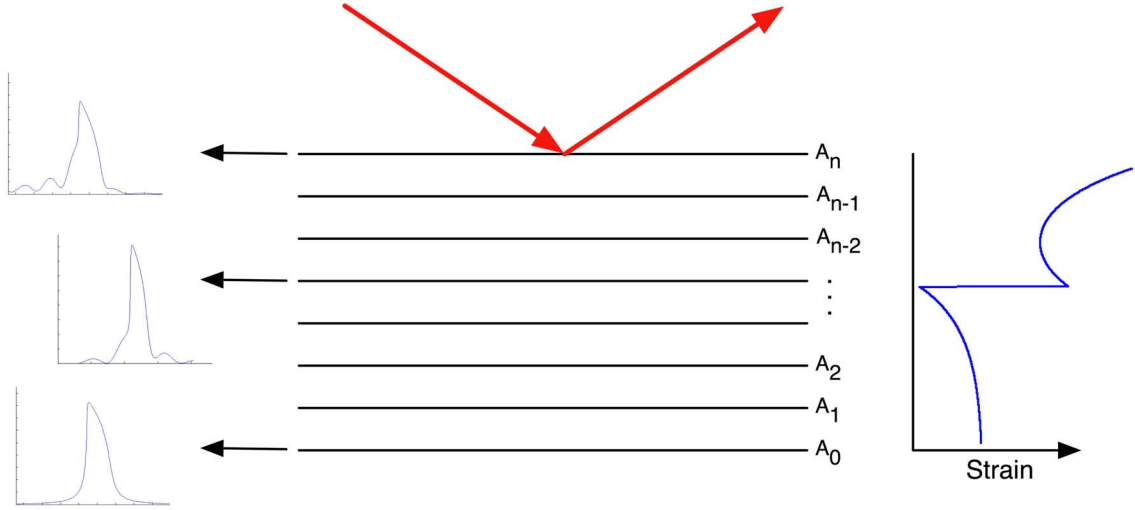


Figure 3.11: A schematic of the Wie algorithm. The solution originates at the infinite crystal solution depth (no strain) and builds a rocking curve at each layer towards the surface. The top layer solution gives the appropriate dynamical diffraction solution.

the subscript $n, n \pm 1$ are omitted. The Wie algorithm begins deep within the crystal where no strain exists, and the diffraction pattern is that of a perfect crystal. Then, it is imposed that at the maximum crystal depth (A_0), $X(A_0) = X_0$. A process schematic for the Wie method is given in Figure 3.11. This relation is easily derived from Equation 3.27, where the notation found in Reference [26] is used, setting the left hand side to X_0 ,

$$X_0 = \frac{sX_0 + i(B + CX_0) \tan(s(A - A_0))}{s - i(C + BX_0) \tan(s(A - A_0))}. \quad (3.28)$$

Collecting terms of X_0 ,

$$0 = BX_0^2 + 2CX_0 + B$$

and solving for X_0 gives

$$X_0 = \frac{-C \pm \sqrt{(C^2 - B^2)}}{B}$$

where the minus sign gives the appropriate and physically significant solution

$$X_0 = -\frac{B}{C - \sqrt{C^2 - B^2}}. \quad (3.29)$$

The infinite solution produces curves such as those shown in red in Figure 3.12. Strain in the crystal distorts the diffraction peak resulting in larger peak widths, reduced intensities and creates ripples off the Bragg peak. Experimental diffraction data usually can not resolve the sideband structures shown here as the angular divergence and energy spread of the x-ray beam are too large; however these distortions of the diffraction peak do appear as asymmetric peak shapes in strain crystal structure.

3.6 Comparison with $\chi_{0,H}$

To test the accuracy of the Wie calculation, an x-ray database that calculates crystal susceptibilities (in this formulation $\chi_{0,H} = \psi_{0,H}$) for scattering and Bragg diffraction, created by S. Stephanov, is used [29]. This database is heavily used within the x-ray community as an accepted source for accurate calculations of angles, widths, intensities and line shape of Bragg peaks. The database can produce diffraction peaks for more than 100 samples at any energy from 5 – 700 keV. The limitation of this calculator is that it is only applicable to the unstrained crystal case and is directly comparable to only the infinite solution from Wie. Unstrained InSb and GaAs crystals are compared to the solutions of $\chi_{0,H}$ in Figure 3.13 and 3.14 at room temperature.

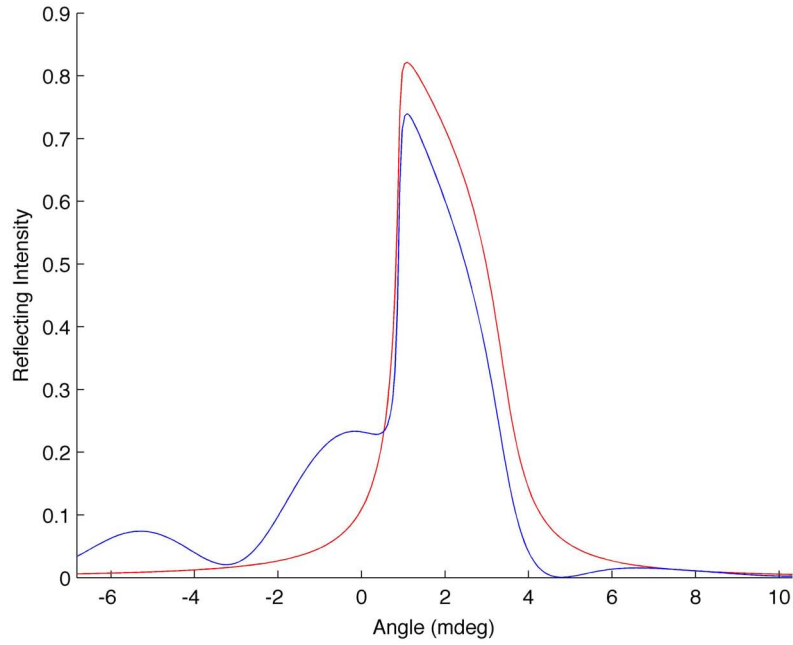


Figure 3.12: The unstrained crystal produces a smooth diffraction peak (red). After the strain has affected the crystal, the lattice deforms and produces lumps on either side of the peak (blue). Calculated using Equation 3.27 with a Thomsen model strain profile (Equation 2.2) for InSb. The wiggles on the sides of the peak are related to the phonon modes that exist in the crystal. A Fourier transform of the diffraction pattern will give the wave vectors present in the material.

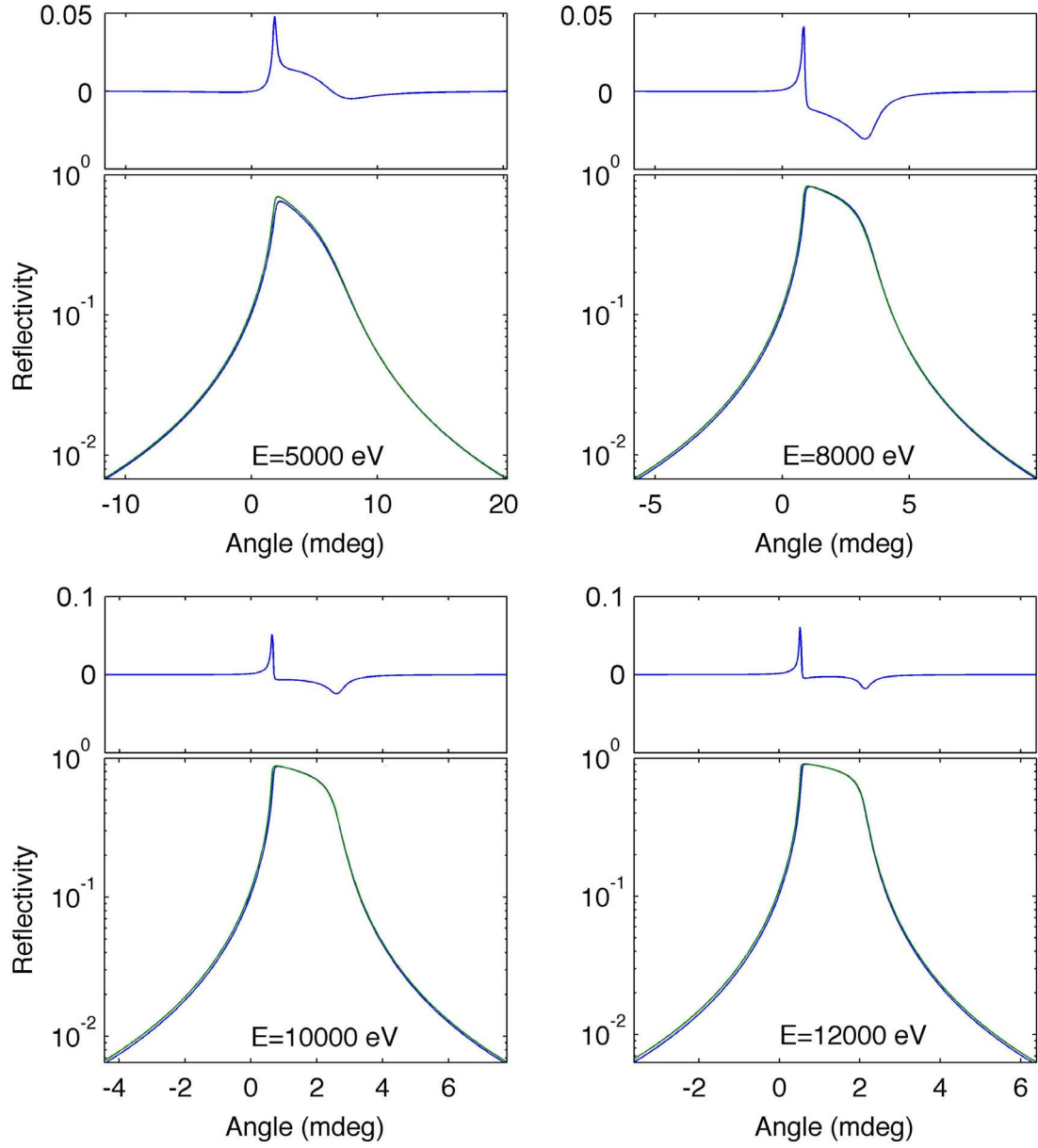


Figure 3.13: Direct comparison between the Wie ($\psi_{0,H}$) algorithm and $\chi_{0,H}$ for InSb at the (400) reflection. Wie is shown in blue, $\chi_{0,H}$ in green. A subtraction residual plot of the difference in the two algorithms ($\psi_{0,H} - \chi_{0,H}$) are shown above each plot. Sb absorption edge at 4.6984 keV.

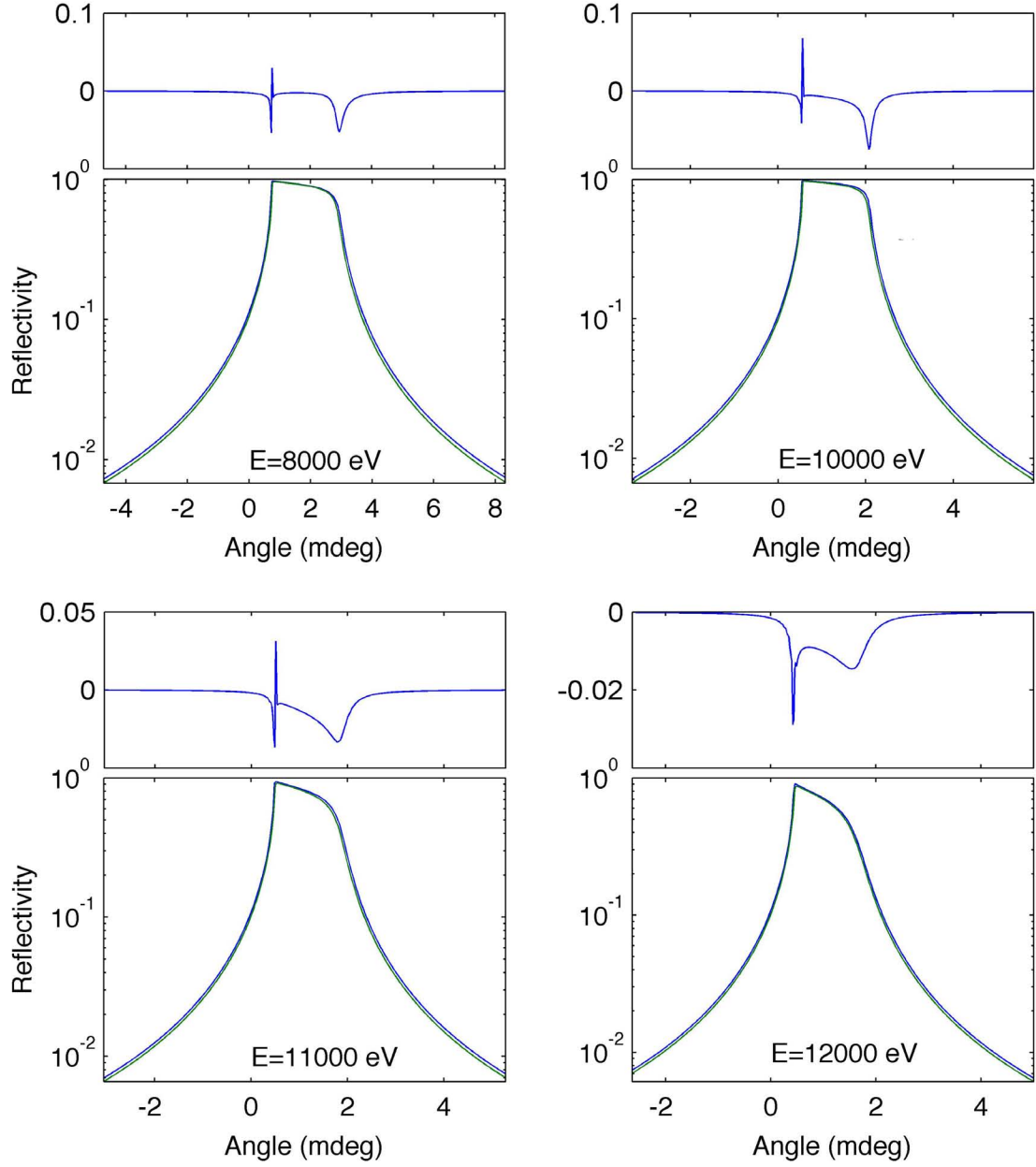


Figure 3.14: Direct comparison between the Wie ($\psi_{0,H}$) algorithm and $\chi_{0,H}$ for GaAs at the (400) reflection. Wie is shown in blue, $\chi_{0,H}$ in green. A subtraction residual plot of the difference in the two algorithms ($\psi_{0,H} - \chi_{0,H}$) are shown above each plot. Ga absorption edge at 10.3682 keV, As absorption edge at 11.865 keV.

CHAPTER IV

Experimental Setup

The experiments presented here were performed at the Advanced Photon Source (APS) at Argonne National Laboratory. The APS is a third generation synchrotron producing x-ray pulses near 1 \AA in wavelength, allowing for precise measurements on the atomic scale. To produce x-rays of high brilliance, insertion devices (ID) are used at each of the 34 beamlines that comprise the APS. In addition, each beamline is equipped with a single bend magnet able to produce x-rays and support experiments. Sector 7 (7-ID) is part of the X-ray Science Division, operated by the Time Resolved Research Group, and was used to carry out the experiments of this study. Novel detector techniques were developed to use in time-resolved studies at 7ID for this study

4.1 X-ray source

Synchrotrons produce electromagnetic radiation through the acceleration of charged particles, usually electrons. At the APS, electrons are thermally emitted from a hot cathode and accelerated by an RF electric field in a linear accelerator (LINAC), after which bunches of electrons at 450 MeV are injected into a booster synchrotron where

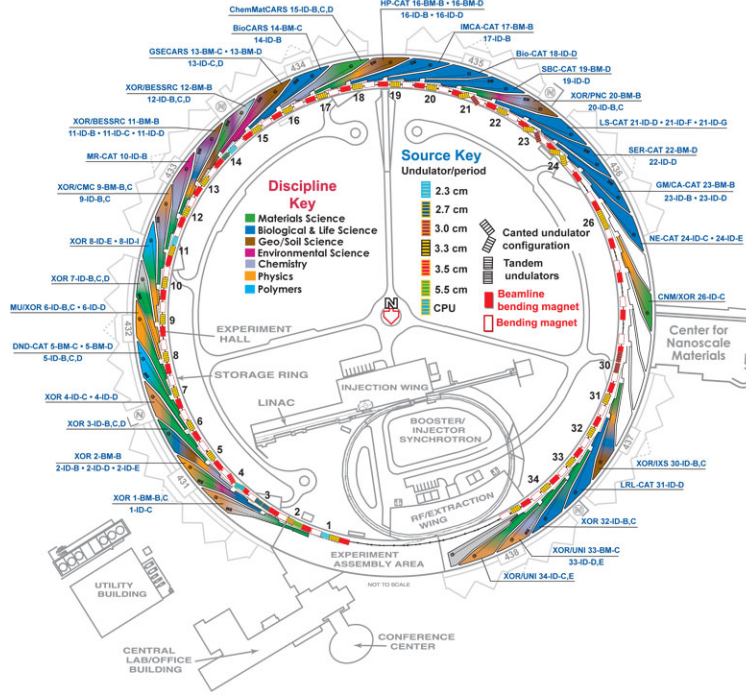


Figure 4.1: Schematic of experiment floor. Image taken from www.aps.anl.gov.

they are further accelerated (see Figure 4.1). The booster ring is synchronized to the outer storage ring with an external RF field.

The RF fields acts to compress individual bunches both spatially and temporally. The storage ring RF is set at 352 MHz where a single cycle defines a bucket, or electron bunch timing position. The APS has four operating modes with different electron distribution in the storage ring while keeping the average current constant through all modes. The standard operating mode consists of 24 bunches spaced evenly around the ring at about 153 ns apart. Other operating modes include 324 and 1296 bunch mode and a hybrid fill mode. Periodically, the extra electrons must be injected into the storage ring to keep the average current constant. In the standard operating mode, this is done by selecting a bunch and injecting additional electrons from the injector synchrotron. When this happens, the current in a single bunch will jump dramatically ($\sim 10\%$), and is referred to as a top-up occurrence.

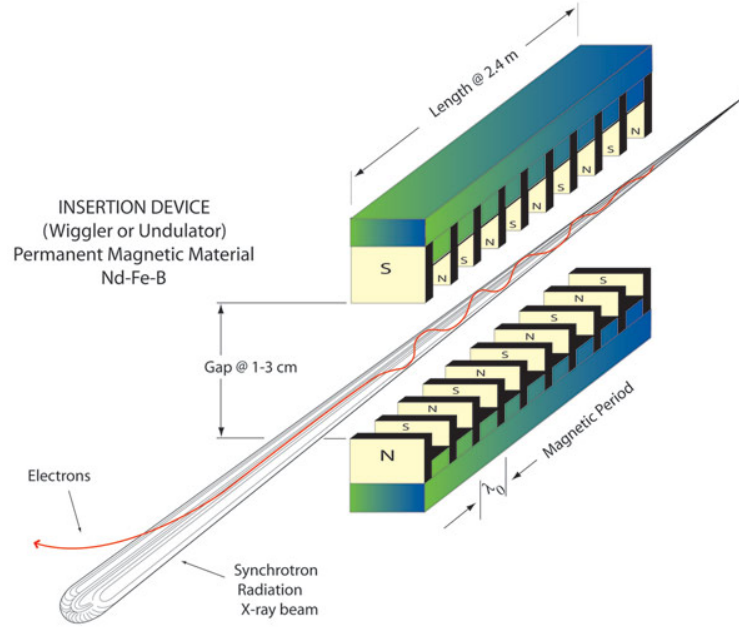


Figure 4.2: Schematic of undulator insertion device. Image taken from www.aps.anl.gov.

The APS storage ring circumference is 1104 m and contains more than 1,000 electromagnets to guide 7 GeV electrons traveling at nearly the speed of light. A third generation synchrotron like the APS is built in a geometry comprising many straight segments. At the intersection of two straight segments, a dipole magnet is placed in the electron beam to bend the electrons. The straight segments have insertion devices which produce the vast majority of the useable x-rays for each beamline. At the APS, most insertion devices are undulators, consisting of evenly spaced, alternating poled permanent magnets which vigorously accelerate electrons left and right, generating extremely bright x-ray pulses (see Figure 4.2).

When the direction of the magnetic field changes, the bunches accelerate (change directions) and emit photons. Since photons are released to conserve energy, the emitted photon wavelength is dependent on the strength of the magnetic field, B_0 , the electron velocity, v_e , and the spacing of magnets in the undulator. The fundamental

wavelength, λ_1 , of radiation from an undulator is related to the periodicity of the undulator, λ_u , by

$$\lambda_1(\theta) = \frac{\lambda_u}{2\gamma^2} \left(1 + \frac{K^2}{2} + (\gamma\theta)^2 \right) \quad (4.1)$$

where θ is the angle between the undulator axis and observation,

$$\gamma \equiv \frac{1}{\sqrt{1 - \beta^2}} = \frac{1}{\sqrt{1 - \frac{v_e^2}{c^2}}}$$

and

$$K = \frac{eB_0\lambda_u}{2\pi m_e c} = 0.934\lambda_u(\text{cm})B_0(\text{T}) \quad (4.2)$$

where e is the charge of the electron, m_e is the mass of the electron, and c is the speed of light [23]. The relative bandwidth of the n th harmonic is

$$\frac{\Delta\lambda}{\lambda} \cong \frac{\Delta\omega}{\omega} \cong \frac{1}{nN} \quad (4.3)$$

where N is the number of magnetic poles in the undulator.

At sector 7, the undulator has a total length of 2.4 m with a magnetic period of 3.3 cm and produces photon fluxes of up to 10^{15} photons per second. The fundamental harmonic tuning range is roughly 3 to 12.5 keV, with a high harmonic generation able to produce 100 keV x-rays. For 24 bunch mode, the temporal pulse width of the x-rays is dictated by the electron bunch length of ~ 70 ps at full width half maximum.

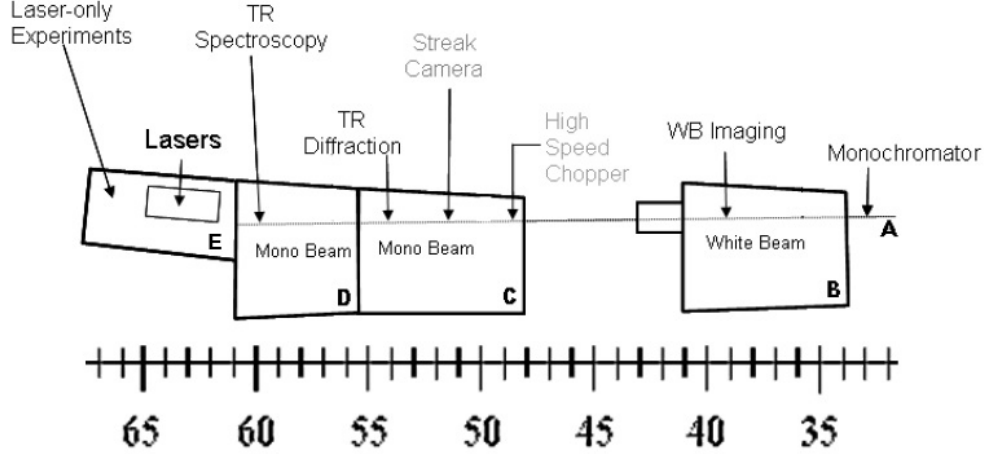


Figure 4.3: Sector 7 beamline layout. TR = time-resolved. WB = white beam. Scale in meters from storage ring. Image taken from [30].

4.2 Beamline layout

The spatial profile and spectral distribution of the x-ray beam from the undulator are much too large for accurate x-ray diffraction measurements. Using Equation 4.3, the spectral bandwidth is on the order of $\sim 1\%$. In order to measure changes in diffraction peak shifts, it is necessary to reduce the spectral bandwidth to $< 0.01\%$. This is accomplished by using Bragg diffraction from a water-cooled diamond (111) double-crystal monochromator to reduce the energy bandwidth to $\Delta E/E = \sim 5 \times 10^{-5}$. By choosing either the fundamental undulator radiation or a higher harmonic, the beamline can produce monochromatic x-ray at energies from 3 to 24 keV.

These experiments were performed in the C hutch (7-IDC) (see Figure 4.3). This hutch is dedicated to time-resolved diffraction experiments using monochromatic beam. An amplified femtosecond laser is brought in from Hutch E by evacuated beam pipe through Hutch D. As the x-rays arrive in Hutch C, they pass a set of collimating slits (JJ slits), which confine the x-rays to $\sim 1 \text{ mm} \times 0.5 \text{ mm}$, and a set

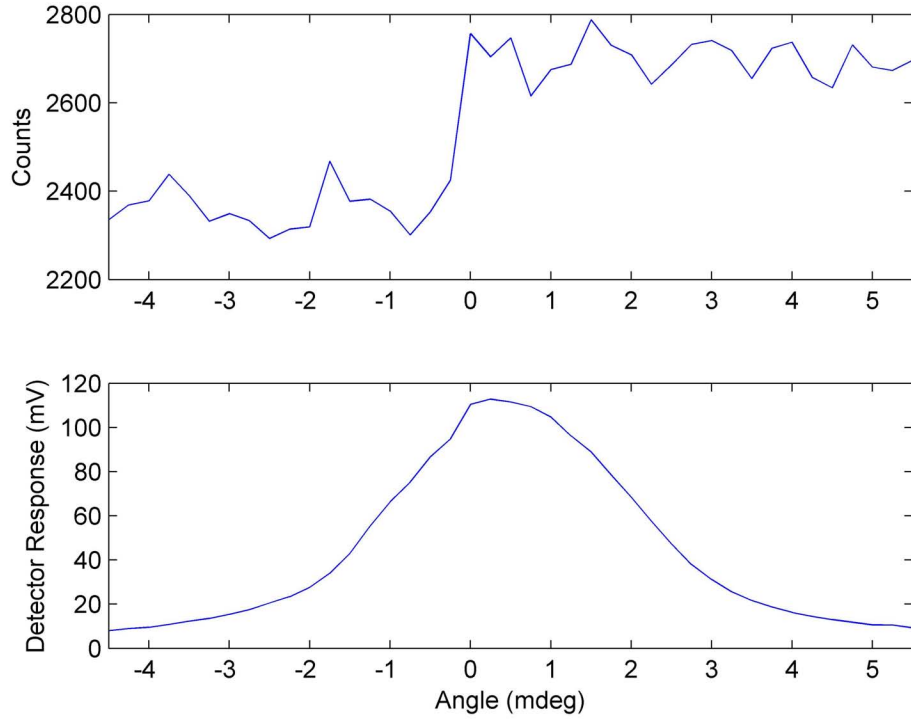


Figure 4.4: Top-up occurrence. The normalization detector (top) has a dramatic change in observed scattering events. The unexpected jump in diffracted intensity at the downstream detector (bottom) can be normalized to compensate for the jump. Data from Scan 784 on GaAs.

of attenuation filters before reaching a scattering foil. This foil has a low x-ray cross section and scatters only a small portion of the upstream x-rays where the scattered radiation is detected by a single photon counting detector. If a time resolved experiment is tracking a bunch that is topped up, the diffraction intensity will increase due to the increased photon flux. With this upstream detector, this additional intensity detected can be normalized, eliminating any discontinuous data (see Figure 4.4).

Beyond the upstream scattering detector are a pair of focusing Kirkpatrick Baez (KB) mirrors. The KB mirrors are 200 mm long, rhodium coated silicon trapezoidal mirrors in a helium-gas enclosure. The x-rays arrive at the sample, mounted on a six-circle Huber diffractometer. In the case of the experiments here, x-rays were

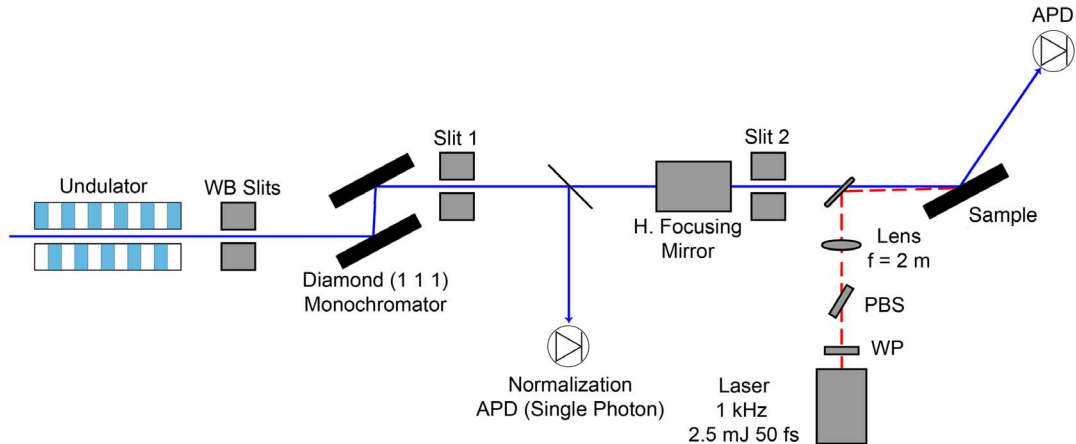


Figure 4.5: Experimental layout of a pump-probe experiment done at APS 7ID-C. WP = wave polarizer, PBS = polarizing beam splitter, WB = white beam.

focused to $20\ \mu\text{m}$ horizontally and collimated with upstream slits to $50\ \mu\text{m}$ vertically to achieve maximum x-ray intensity with minimal vertical divergence at the sample.

4.3 Pump-Probe X-ray Experiments

Ultrafast processes, which take place on the order of picoseconds or femtoseconds, are much too fast for any electronic detector system. To resolve effects with high temporal resolution, the shutter speed — or time over which the detector records information — must be on the order of the time scale of the action. It is then necessary to use ultrafast pulses of light to record ultrafast dynamics. If a long pulse, or continuous beam of radiation were used, the effects would be averaged over the length of the pulse and transient effects would be ignored. Therefore, in ultrafast experiments, very short pulses of light are needed to resolve the structural or optical properties of materials.

The experiments presented here consisted of an optical pump, x-ray probe setup. First a pump pulse being absorbed by the sample disturbing the structure of the material. At some fixed time later, a probe beam arrives. The change in system configuration can be inferred by the change in reflectivity, absorption, or diffracted intensity between the unperturbed and perturbed case. In the cases presented here, structural changes in crystal formation are examined using the change in x-ray diffraction. The pump beam is an optical-wavelength amplified femtosecond laser. An example of a pump-probe experiment layout is given in Figure 4.5.

In these x-ray experiments, samples are mounted on a six-circle Huber diffractometer. This has the capability of placing a sample at any orientation with respect to the incident beam. A crystal is rocked about a symmetric reflection on an axis perpendicular to the incident beam and parallel to the crystal planes, making an angle θ between the crystal and beam. Since the diffracted beam also makes an angle θ with the surface, the detector is positioned at an angle 2θ with respect to the beam. In the experiments presented here, the detector arm is left at a fixed 2θ position and the crystal is rocked about a Bragg angle, producing rocking curves. Additionally, the motors on the diffractometer controlling the changes in crystal orientation may be called by the orientation name (θ -motor, 2θ -motor, χ -motor, etc.).

4.4 Detectors

In order to record single diffraction events, detectors must be able to differentiate between x-ray bunches. This is essential to perform time-resolved experiments since low speed detectors average over multiple bunches losing the transient information recorded in each x-ray pulse. In normal operating mode, the bunches arrive nearly every 153 ns, therefore, it is required that the detectors completely recover from

residual changes resulting from the arrival of the previous bunch within ~ 100 ns. The high-speed detector chosen for these experiments is a silicon avalanche photodiode (APD) which can be configured to be either a single photon counting device or a fast integrated intensity detector by adjusting the high voltage bias and amplifier gain.

4.4.1 Counting Mode

In photon counting mode, the APD is biased to nearly the breakdown voltage of silicon. This extreme biasing allows the detector to measure single x-ray events through a process known as avalanching. When photons of energy greater than the silicon energy gap are absorbed, an electron-hole pair is created and violently collides with other electrons due to the large bias. After a few collisions, the charge is enough to be detected by the electronics as a current. While the charge carriers exit the bulk of the silicon, the detector experiences a deadtime — a finite time needed to reestablish the biasing voltage, during which time the detector is unable to resolve additional photons. A detector deadtime underestimates the number of actual x-ray events and a statistical model must be used to estimate the actual number of counts. If a detector is dead for a time τ after each single event, the arrival of additional x-rays in the interval $0 \leq t \leq \tau$ is not counted. Additionally, the time needed to reestablish the bias is extended by a time $\delta\tau$. This is the extended deadtime model and is generally used for slower detectors such as scintillators using a single channel analyzer.

For the cases of fast detectors used at Sector 7 and other synchrotron-based applications, the model is slightly different [31]. If the deadtime is less than the x-ray pulse separation, any photons arriving during that time will be registered as a single

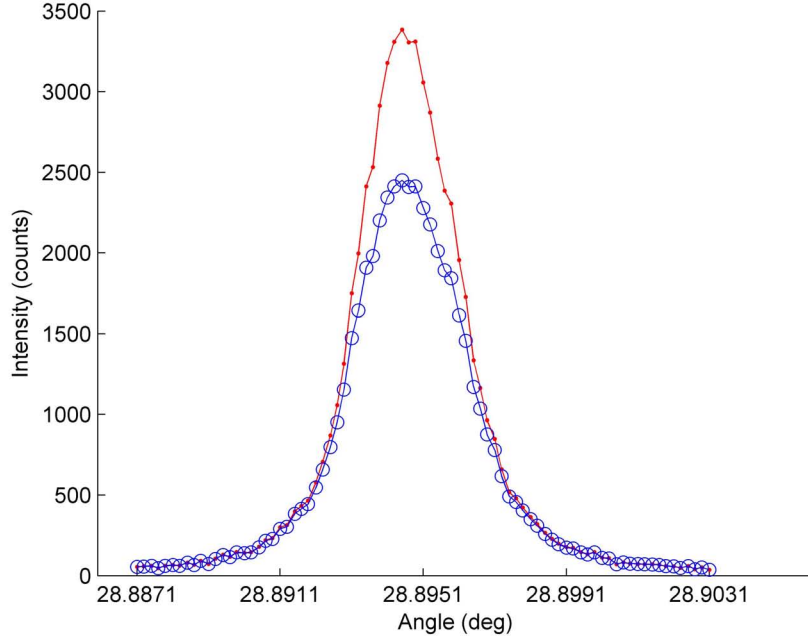


Figure 4.6: Deadtime correction for counting detectors. Observed counts shown in circles in blue, true counts in red. The number of true counts is given by Equation 4.4.

count. This is known as the isolated deadtime model and gives a true count rate of

$$N_T = -\frac{1}{\tau} \ln(1 - \tau N_O) \quad (4.4)$$

where N_T, N_O are the true and observed count rates. Figure 4.6 shows an example of the observed and true counts for an InSb reflection.

The associated uncertainty in the estimation of the true count rate is dependent on the statistical uncertainty in N_O given by the square root of the number of counts, $\sqrt{\sigma_{N_O}}$, and the uncertainty in the deadtime, σ_τ . The uncertainty in N_T , then, is found by propagating error in quadrature with respect to N_O and τ . The resulting

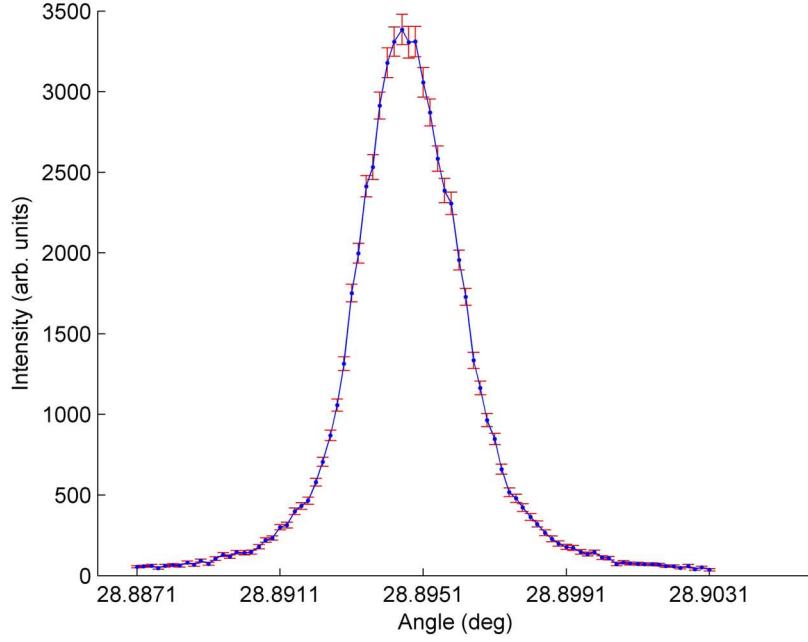


Figure 4.7: The counting statistics are slightly different for deadtime corrected measurements. Using Equation 4.5, error bars are fit to the corrected data.

relative error for the isolated deadtime model of Equation 4.4 is

$$\frac{\sigma_{N_T}}{N_T} = \frac{1}{N_T(1 - \tau N_O)} \sqrt{\frac{N_O}{t}}. \quad (4.5)$$

When used in counting mode, the APD output is sent directly to a constant fraction discriminator (CFD). The CFD compares voltage pulses from the APD to a threshold level (typically 25 – 50 mV) to separate signals originating from x-rays away from noise, which can be large at the output of a high-gain device such as an APD. The CFD outputs digital NIM signals which are then sorted into timing bins and individually counted.

4.4.2 Proportional Mode

When the APD is not critically biased, it can collect data using a proportional voltage mode. In this case, incident photons again create electron-hole pairs and an applied electric field moves them in opposite directions registering a current. The current is proportional to the number of incident photons and requires no deadtime corrections due to the ample number of valence electrons in the penetration depth of silicon and constant lower-voltage biasing. This method is very similar to that of an optical photodiode with a low bias. The output is recorded as a voltage reading with a constant error bound equal to the noise level of the APD. All efforts are taken to ensure that only diffracted x-rays arrive at the APD by shielding the detector with foil and black cloth as well as an extra set of slits on the detector arm.

There exists significant advantages to using an APD in proportional mode. Because of the high count rates associated with synchrotron radiation, counting mode often is plagued by high deadtime corrections which introduce significant uncertainty. In order to maximize the signal to deadtime error, the count rate is limited by reducing the number of x-rays in the monochromatic beam. In proportional mode, however, photon fluxes of up to 10^{13} photons per second, the maximum monochromatic flux at 7ID, are still within the linear range of the detector with proper choice of bias and gain.

4.5 Data Acquisition / Ztec Oscilloscope

For the proportional mode detectors, the x-ray pulse train is recorded through time. The analog voltage output is sent into a fast triggering oscilloscope to record the x-ray pulse shape and height. The APS systems control is an open source software

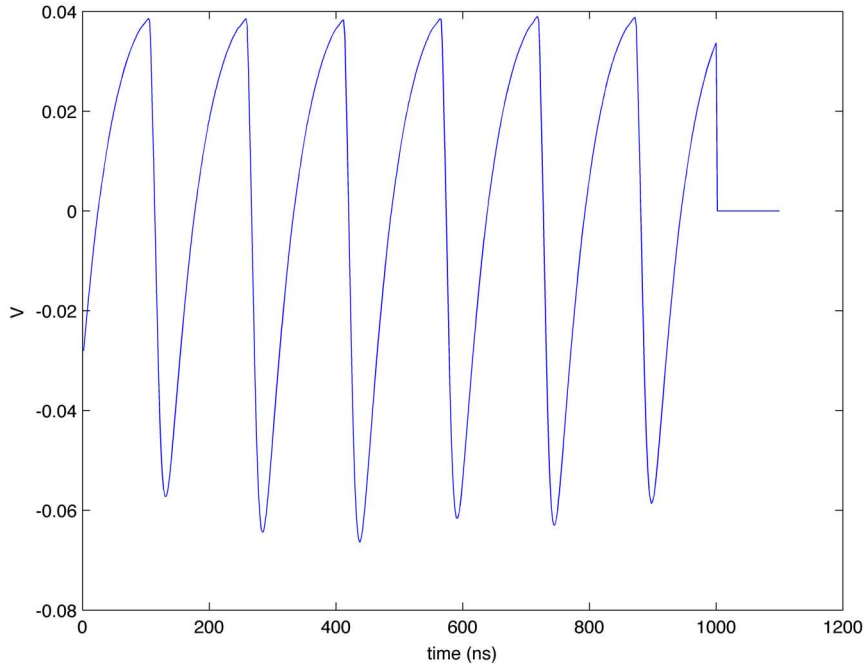


Figure 4.8: Raw data from averaged detector data in proportional mode. Figure shows negative-going spikes. The deviation in the pulse heights are due to the different current in each bunch. Data shown here has been averaged over 1024 triggers.

platform called EPICS, (Experimental Physics and Industrial Control System). In previous experiments where an oscilloscope was used, signals arriving from the detector were processed by an oscilloscope, then uploaded to a separate EPICS client, and finally uploaded to the EPICS servers. This processing and uploading has a finite time and results in the oscilloscope stalling, being unprepared for the next bunch and failing to trigger since it was still trying to offload data to the EPICS client.

The solution to this problem is a fast triggering oscilloscope that is a native EPICS client. In this situation, there is no need for an intermediate step and the oscilloscope passes data directly to the servers. Ztec Instruments provided an oscilloscope with exactly these specifications, able to sample every 2 ns, sufficiently fast for the recovery

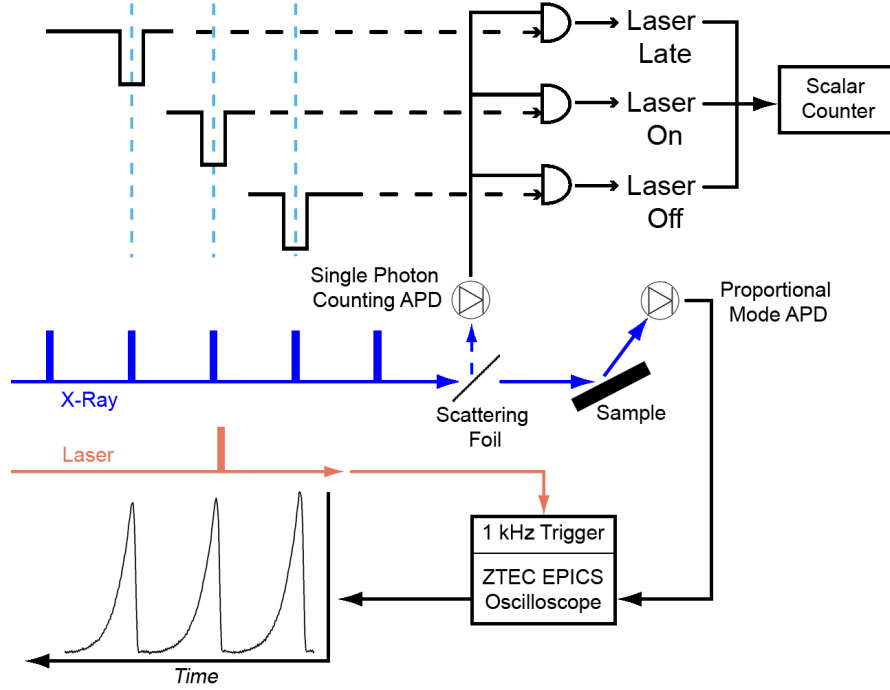


Figure 4.9: Timing diagram for a proportional mode pump-probe experiment at 7ID-C. When counting detectors are used, the detector outputs to a triggered analog to digital counter.

time of the APD (~ 75 ns). The Ztec will trigger every 1 kHz, given by the external triggering signal from the Pockels cell. The oscilloscope makes 1024 averages then offloads the data to the EPICS servers.

An example of the x-ray pulses, recorded by the Ztec oscilloscope, are shown in Figure 4.8 where the sharp negative edges are x-rays arriving at the detector and the curvature of the pulses is due to the recovery time of the APD since the x-ray pulses are only ~ 100 ps long. Each pulse is segmented and a smoothing function is fitted to determine the peak height. The maximum value for each curve is recorded, defining the diffracted intensity for the particular x-ray pulse. Since the triggering is synchronized to the storage ring, each x-ray pulse corresponds to a particular electron bunch.

Typically, there are three bunches that are followed: laser-off, laser-on, and laser-late. Laser-on and laser-off are the x-rays immediately before the laser pulse arrives at the sample and immediately after the laser arrives. Laser-late is the second bunch after laser excitation. These three bunches gives the initial condition of the sample (laser-off), the excited state (laser-on), and the long time condition 153 ns later, showing thermalization (laser-late). A schematic of the timing system used for proportional mode is given in Figure 4.9

Running an experiment with proportional mode detectors currently has one major downfall. As an EPICS platform device, the oscilloscope is controlled using process variables (PV) files to carry out particular tasks. For the Ztec, technical problems such as reading in PVs, recalling saved PVs after a restart, and saving to the EPICS servers have been an ongoing issue. This is largely avoided by a specific protocol to load PVs and increasing the time between data points when the Ztec accesses the servers to upload data. This protocol is given in Appendix B.

4.6 Laser System

A titanium sapphire Kerr-Lens modelocked 20 fs laser oscillator (manufactured by Coherent, Inc) produces a pulse train at 88 MHz which is synchronized to the electron bunches in the storage ring to within 250 fs rms. The relative timing between the laser and x-rays is adjusted using an electronic phase shifter in the synchrotron feedback loop. The laser oscillator pulses are too weak (~ 2 nJ/pulse) to excite large amplitude motions in semiconductors and too frequent at the 88 MHz repetition rate to permit sample cooling between laser pulses. Therefore, single oscillator pulses are electro-optically selected by Pockels cells and amplified at a rate of 1 or 5 kHz up to energies of 0.5 – 2.5 mJ/pulse using a regenerative chirped pulse laser amplifier (manufactured

by Coherent, Inc). The synchronization between x-rays and laser pulse is done using an antenna placed near the electron beam in the storage ring. This signal is amplified and filtered to produce an RF signal that is mixed with the output of a photodiode in the laser oscillator. The phase difference drives a piezo-mounted mirror to synchronize the laser. Delays between the x-ray and laser are generated electronically by phase shifting the electron beam RF.

CHAPTER V

Time-Resolved X-ray Diffraction

X-ray techniques may be employed to directly probe displacements at the atomic scale. In contrast, optical measurements are not directly sensitive to structural changes since the typical atomic spacing is on the order of 1 Å. An optical pump, X-ray probe technique is used to perform time resolved x-ray Bragg diffraction. At the APS, the temporal resolution is dictated by the bunch length of the electrons at ~ 100 ps, averaging out any time-dependent effects below this limit. Given this restriction, information can still be extracted on the dynamics of strain by measuring rocking curves. Here, we present time resolved studies exploring strain generation and thermalization in InSb and GaAs semiconductor crystals.

5.1 Time Resolved X-ray Rocking Curves

As a crystal is rotated with respect to an incident beam of x-rays, it will pass through a geometry in which the three Laue conditions are simultaneously met and diffracted radiation will add coherently. In the Bragg geometry, the Laue conditions are satisfied by an angle θ_B , such that $d = \lambda/2 \sin(\theta_B)$ where d is the distance between lattice planes and λ is the wavelength of the incident radiation. Due to the spatial

resolution of our experimental setup, Bragg peaks are best represented by a Gaussian distribution,

$$I(\theta) = I_0 e^{-\frac{(\theta - \theta_B)^2}{2(\delta\theta)^2}} + C \quad (5.1)$$

where I_0 and C are parameters defining the peak intensity and constant offset from zero, and $\delta\theta$ is the standard deviation which can be related to the full width at half maximum by $FWHM = 2(\delta\theta)\sqrt{2\ln 2}$. Knowing the wavelength and experimentally finding the Bragg angle, θ_B , the lattice parameter can be calculated.

There are several approaches to analyzing Bragg diffraction data. In this case, the aggregate change in lattice parameter is examined where Bragg peaks are fit to Gaussian distributions and the center position (centroid) is extracted. Using this information, these studies track structural change, Δd , in materials immediately after laser excitation. The position, however, is not the only information accessible with a rocking curve. The lineshape also contains information on the transient state of the crystal. This is summarized in Figure 5.1, where a broadened rocking curve indicates a portion of the probed crystal that has expanded or contracted in relation to the rest of the material.

As discussed in Chapter II, there are several hypotheses available to describe the dynamics of crystals under intense laser excitation. The Thomsen model states that all energy absorbed into the lattice is in the form of heat in the material. With this assumption, the temperature of a material can be measured by knowing the change in center peak position of the Bragg diffraction and linear expansion coefficient, β .

For example, if a 1.0 mdeg ($\Delta\theta/\theta = 0.0041\%$) shift in center peak position is observed for InSb at a Bragg angle of 24.5 degrees, the lattice expansion is 0.057

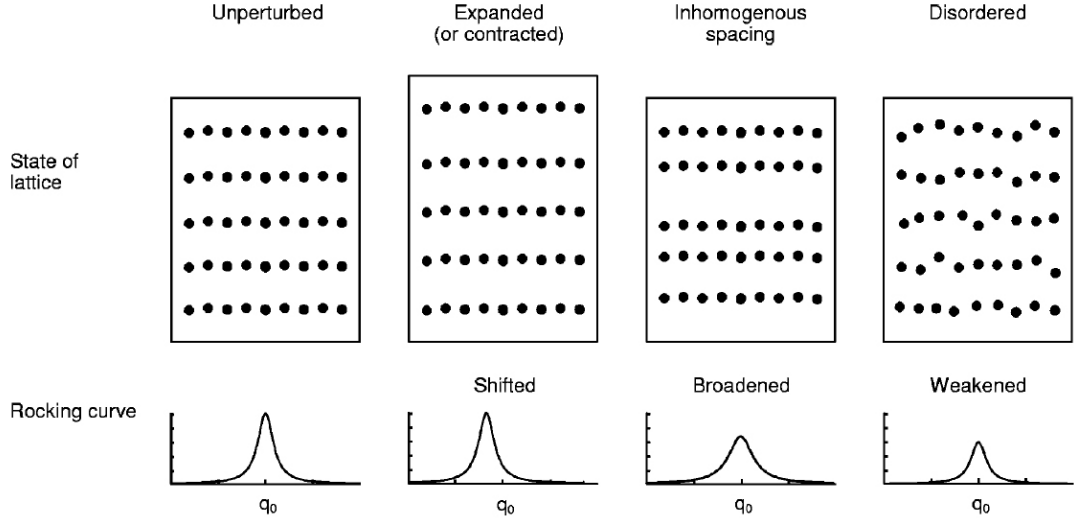


Figure 5.1: Rocking curves lineshape and position indicate the state of the lattice as transient effects pass through the penetration depth of x-rays. In these experiments, inhomogeneous spacing and lattice expansion are observed. Image taken from [32].

mÅ ($\Delta a/a = 0.0038\%$) and given a linear expansion coefficient $\beta = 5.37 \times 10^{-6} \text{ K}^{-1}$, the surface temperature rise of 7.1°C . For any angle shift, $\Delta\theta$, the temperature jump can be calculated by

$$\Delta T = \left(1 - \frac{\sin(\theta_B)}{\sin(\theta_B + \Delta\theta)} \right) \frac{1}{\beta}. \quad (5.2)$$

The non-thermal effects following laser absorption, however, have a finite lifetime in the crystal. This approximation works well for long time periods after excitation (greater than 1 ns), but for the initial non-thermal regime (up to 750 ps), this calculation is not valid and underestimates the amount of stress in the lattice. In one case, the material responds linearly to absorbed laser fluence, qualitatively similar to the characteristics of the Thomsen model. In the other material, lattice response has a nonlinear fluence relationship.

To generate transient strain in these crystals, an 800 nm, 40 fs laser pulse illuminated the crystals, each cut in the [100] orientation. The optical penetration depth for InSb and GaAs are 0.1 μm and 1 μm respectively. The x-ray absorption depth is given by the imaginary part of the x-ray scattering susceptibility for the incident beam ψ_{0i} . The absorption factor μ_0 is given by $\mu_0 = (2\pi|\psi_{0i}|)/\lambda$ where the absorption length is $a_0 = \mu_0^{-1}$. For InSb and GaAs at 10 keV, the absorption length is 12 and 47 μm respectively. This value is only valid for cases when the Laue conditions are not met and there is no diffraction taking place. That is, this is the kinematical limit where the only attenuation effect is linear absorption and extinction (interaction between incident and diffracted waves) are negligible.

In the dynamical limit, when the Laue conditions are met the extinction length for a symmetric reflection is

$$L_{\text{ext}}^{\text{Bragg}} = \frac{\lambda \sin \theta_B}{\pi \sqrt{|\psi_H \psi_{\bar{H}}|}} \quad (5.3)$$

where ψ_H is the susceptibility of the diffracted beam and $\psi_{\bar{H}} = (\psi_H)^*$. The extinction length is the depth inside the crystal at which the intensity is attenuated by a value of e^2 . The susceptibilities of these materials at arbitrary energies and reflections can be found using the computer program available in Appendix C.

The x-ray extinction depth for InSb and GaAs at 10 keV is 1.12 μm and 1.65 μm respectively, calculated using Equation 5.3. This is the depth at which x-rays probe into the sample at peak diffraction intensity, on top of the Bragg peak, when the effect is entirely in the dynamical regime. The differences between optical and x-ray extinction lengths allows for the distinction between the surface and bulk component of the impulsive strain wave. That is, the x-rays are able to probe well outside the

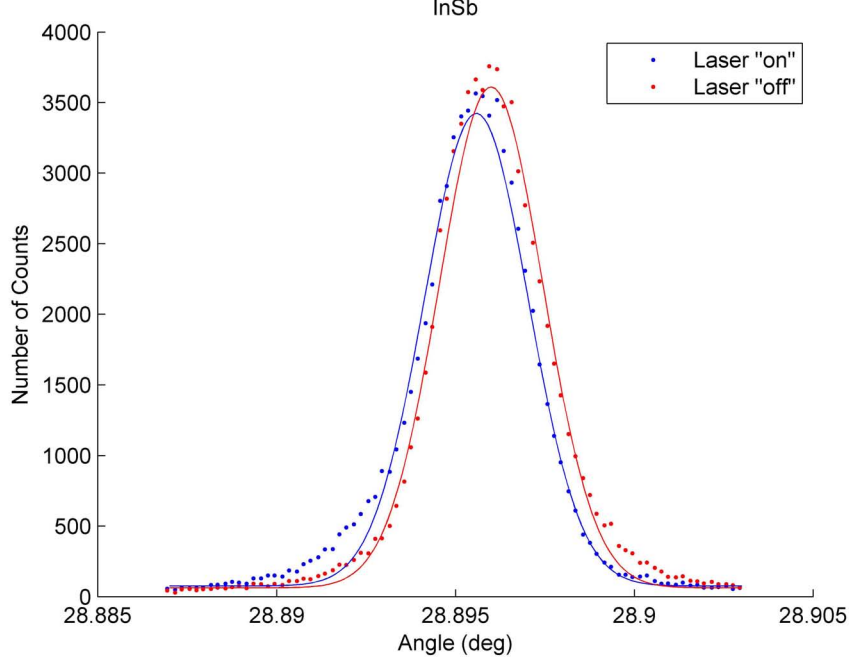


Figure 5.2: Rocking curves are fit to Gaussian distributions to extract center positions and standard deviations (FWHM) values. A disturbed (expanded) lattice is the result of ultrafast excitation (blue) compared to the equilibrium lattice (red).

penetration depth of the laser into the unperturbed crystal layers after excitation.

The symmetric (400) reflections of InSb and GaAs were observed, chosen since it is a strong reflection of zinc-blende structures. In each experiment data was collected with 10 keV x-rays and a spectral bandwidth of ~ 1 eV.

5.2 InSb Results

Rocking curves were produced with a pump-probe delay of 0 to 2.5 ns at absorbed fluences of 0.24 to 1.35 mJ/cm². At each time point, the rocking curve is fit to a Gaussian and the centroid extracted (see Figure 5.2). As the laser fluence is increased, the rocking curves are deformed with additional diffracted intensity on the low angle side of the peaks. This corresponds with an inhomogeneous lattice spac-

ing through the penetration depth of the x-rays. Extinction (destructive interference between incident and diffracted waves in the crystal) also plays a large role in the (400) reflection, further distorting the diffraction peak shape. At long time scales, the rocking curves remain significantly broadened indicating a persistent strain in the crystal. This is likely a result of thermal effects since heat takes a significant amount of time (hundreds of nanoseconds) to diffuse out of the extinction depth of the x-rays. Figure 5.3 shows rocking curves at 400 ps after laser excitation for a range of fluences. As the absorbed energy is increased, the low angle sidebands broaden and peak intensity decreases.

In order to determine whether the strain is induced thermally or electronically, the centroid and full widths at half maximum of each rocking curve at each time point and each fluence are plotted in Figure 5.4 and Figure 5.5. By taking the centroid of the gaussian fit to a rocking curve, the average strain over the extinction depth of the x-rays is calculated. For InSb, the peak strain occurs at 400 ps, where the crystal quickly recovers to an equilibrium or quasi-steady-state lattice alignment. After 1 ns the rocking curve does not significantly change centroid position, signifying that the impulsive strain wave must be completely outside the probing depth of the x-rays, leaving behind only a thermally excited lattice. The width of the rocking curve gives an estimation on all parts of the extinction depth are thermalizing.

A measure of the full width at half maximum for each rocking curve is given in Figure 5.5. The InSb rocking curve width increases by nearly a factor of two in 200 ps, indicating that the lattice at the surface has expanded tremendously while the material deeper into the crystal remains unaltered. As the wave propagates and thermal energy diffuses, the width equilibrates with a 15% increase at the highest fluence. The quick recovery is evidence of thermally driven strain. The traveling wave

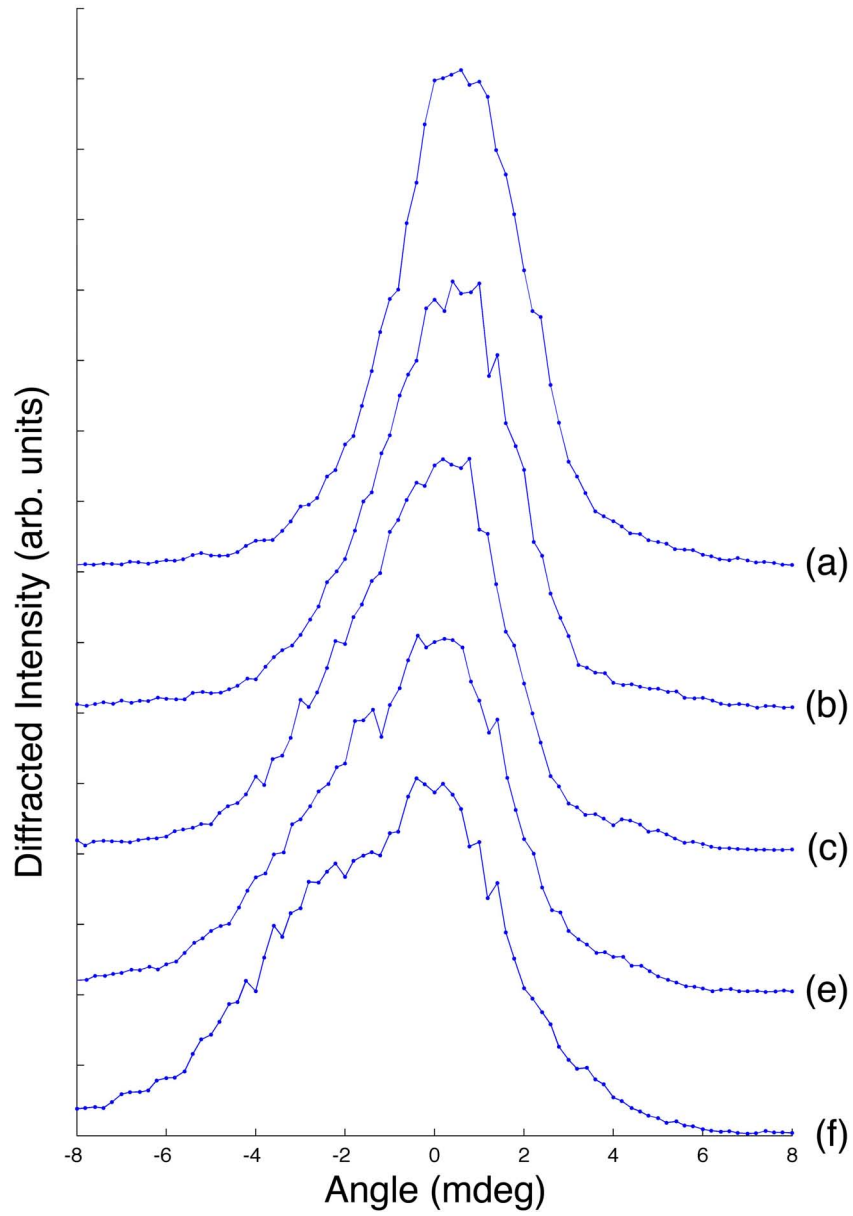


Figure 5.3: The lineshapes of InSb rocking curves significantly changes with absorbed laser fluence. The rocking curve of the lowest fluence (a) at 0.24 mJ/cm^2 begins to broaden as the fluence is incrementally increased to 0.46 (b), 0.74 (c), 1.05 (d), and 1.35 mJ/cm^2 (e). Here, the rocking curves broaden, shift, and decrease in amplitude denoting expansion and inhomogeneous spacing in the lattice. Plots are shown with a vertical displacement for clarity.

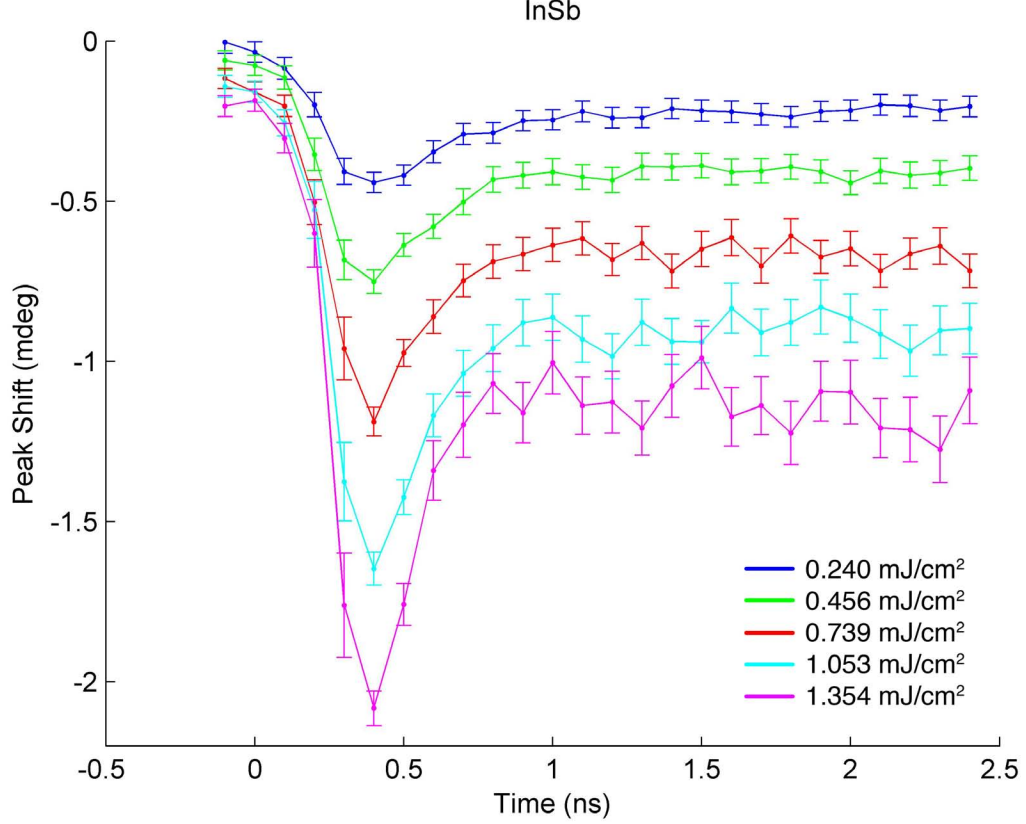


Figure 5.4: As an acoustic disturbance propagates into the crystal, the lattice responds by expanding (negative peak shift), followed by a recovery to a lattice at thermal equilibrium. Lattice expansion due to thermal contributions and transient effects are linear with fluence in InSb. Note that the lines connecting data points are there for visual aid and does not denote a model or fit.

propagates outside of the extinction depth leaving behind a temperature gradient which manifests as a slightly wider rocking curve. Here, there is no evidence that electrons play a role in the dynamic response of InSb.

Both the thermal heating and impulsive strain appear to be linear through the range of absorbed fluences. Additional data was collected suggesting that the peak strain continues to be linear up to the damage threshold of InSb. Figure 5.6 shows the peak strain (taken at 400 ps) and thermal strain (the average of centroid positions

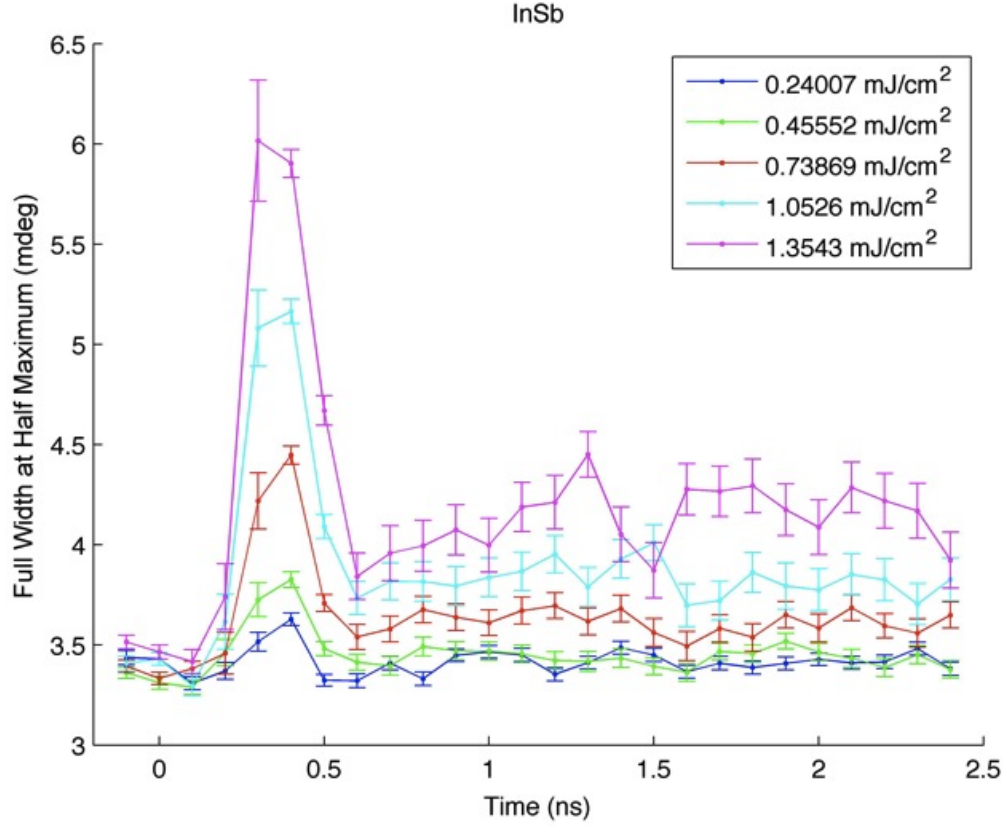


Figure 5.5: As the laser pulse is absorbed into the material and launches a bipolar strain wave, the lattice experiences inhomogeneous spacing, dramatically increasing the width of the Bragg peak.

from 1 to 2.5 ns) fitted with a linear slope versus laser fluence. The offset at time-zero is due to the inability of the crystal to cool in the 1 ms before the next laser pulse arrives. The rough curves are principally due to counting statistics and the inaccuracies in fitting gaussians to the asymmetric rocking curves (see Figure 5.3).

The counting statistics of the x-ray detectors used in this experiment (Equation 4.5) propagates into a weighted Gaussian curve fit used in determining the center of the rocking curve. The standard deviation of the fit parameter is extracted and plotted in Figure 5.4 and 5.6. The lower slope in Figure 5.6 uses an average uncertainty in the fit values between 1 – 2.5 ns while the uncertainty in the upper slope

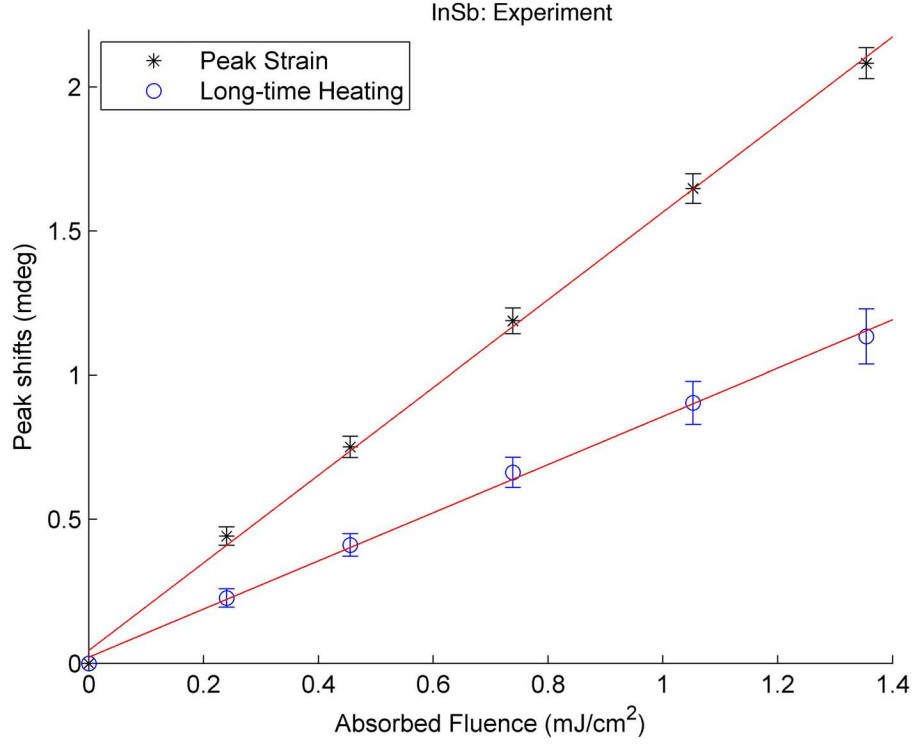


Figure 5.6: Peak (black) and thermal (blue) strain have a linear relationship with absorbed laser fluence. A linear fit was performed to each set of data, while a point at the origin was manually inserted.

are single values at 400 ps.

The linearity of InSb, with respect to both impulsive strain and thermal strain, is due to the partition of energy between thermal and electronic strains. InSb is frequently used as a near infrared detector since the band gap is only 0.17 eV, sensitive to photons of wavelength up to $\sim 7.3 \mu\text{m}$. When titanium sapphire laser light (1.55 eV) is absorbed, only a small fraction of the energy goes into promoting electrons, where almost all is deposited into the lattice as heat. It would appear that this is the physical limit of the Thomsen model with the vast majority of the energy is bundled as a thermally induced propagating wave. A discussion of the comparison and alterations to proposed models is given in Section 5.4. It is understood that the

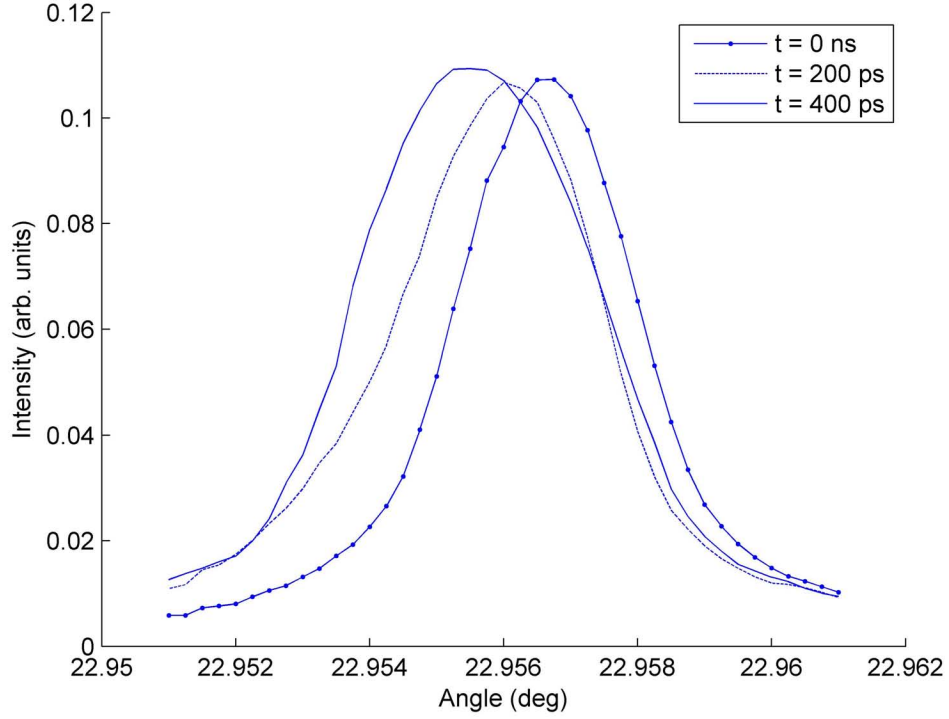


Figure 5.7: GaAs rocking curve for time-zero (solid with dot), 200 ps (dashed), and 400 ps (solid) after laser excitation. These rocking curves shift and broaden as the strain wave affects the lattice spacing.

response to heat in a crystal to be very linear, given by Equation 5.2 and shown in Figure 5.6.

5.3 GaAs Results

The sound speed, thermal expansion, and heat capacity are all very similar in magnitude between GaAs and InSb, yet the effects of laser excitation on the two materials are very different. This is at least partially due to the difference in band gap, which for GaAs is 1.424 eV. Therefore, the majority of the absorbed laser energy goes directly into producing electrons, leaving only a small remainder in the form of heat.

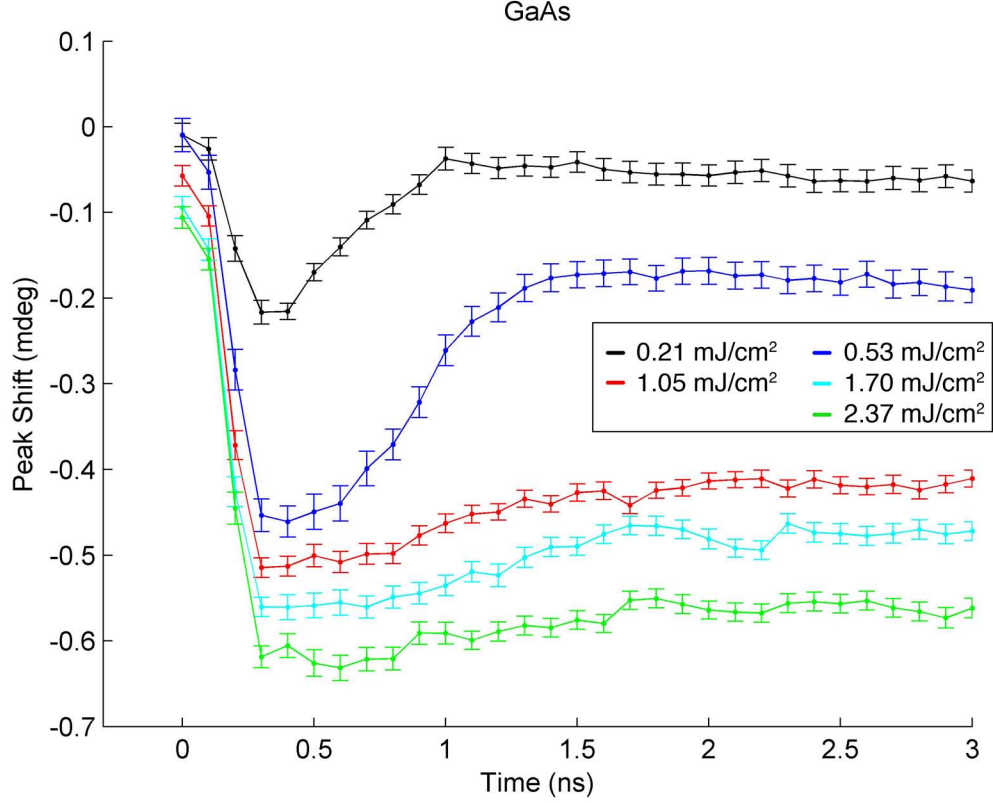


Figure 5.8: For low fluences, GaAs responses to laser-induced strain similar to InSb. As the crystal absorbs more energy, the response to the impulsive strain saturates, no longer responding in the linear manner seen in the low fluence case.

The GaAs rocking curve data again shows a centroid shift to the left indicating expansion of the lattice while also showing significant broadening of the lineshape as the impulsive strain wave moves through the crystal (see Figure 5.7). These rocking curves are exceptionally smooth due to the 1024 averages done in proportional mode, which is a great improvement over the InSb data set of highly distorted lineshapes taken with single photon counting detectors (Figure 5.3).

With this quality of data, Gaussian curve fitting produces very small confidence intervals. As well, since the measured uncertainty in the amplitude of diffracted intensity is a constant value of ~ 1 mV, further reducing the relative propagated error.

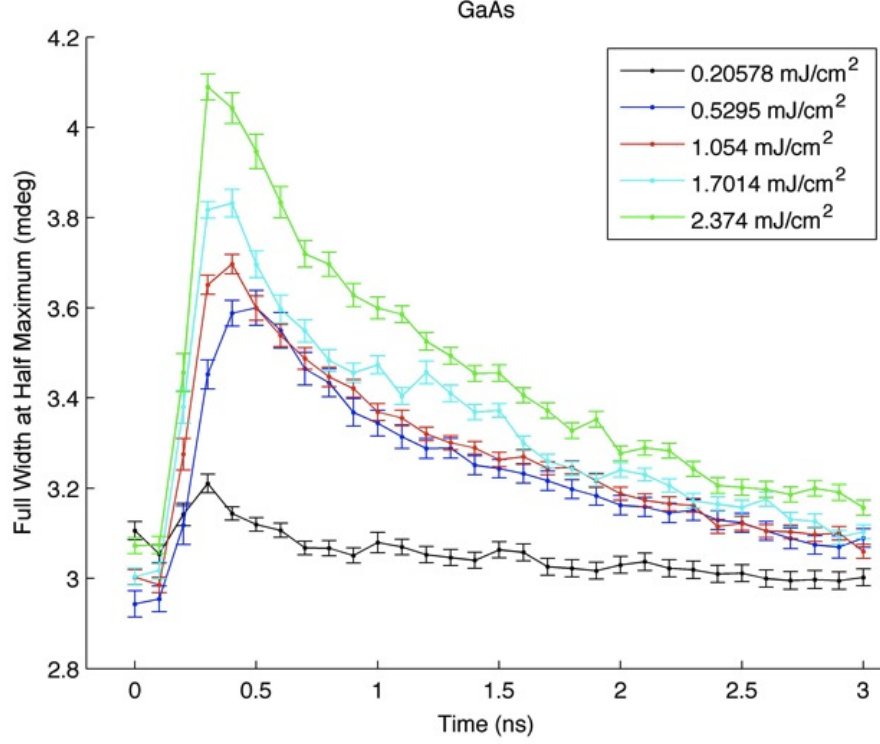


Figure 5.9: Time resolved changes in the rocking curve width of GaAs indicates a significant contribution from the energetic electrons created by the absorption of a laser pulse. The slow decay of the width shows that the lattice spacing recovers only after the electrons have recombined or diffused further than the extinction depth of the x-rays.

The reward for careful experimental setup and choice of detectors is summarized in Figure 5.8 where the centroid shift is measured with high confidence and high precision.

At low fluences (less than 0.5 mJ/cm^2), GaAs responds nearly identically to InSb. A large leftward peak shift begins the lattice reaction, cresting at 400 ps after excitation, with a quick recovery to a small, thermal offset. As the fluence is raised above 0.5 mJ/cm^2 , however, the strain due to the impulsive acoustic wave is highly attenuated. At $\sim 400 \text{ ps}$, the lattice response saturates to increasing absorbed energy in the semiconductor. In spite of the nonlinear response to impulsive strain, the thermal

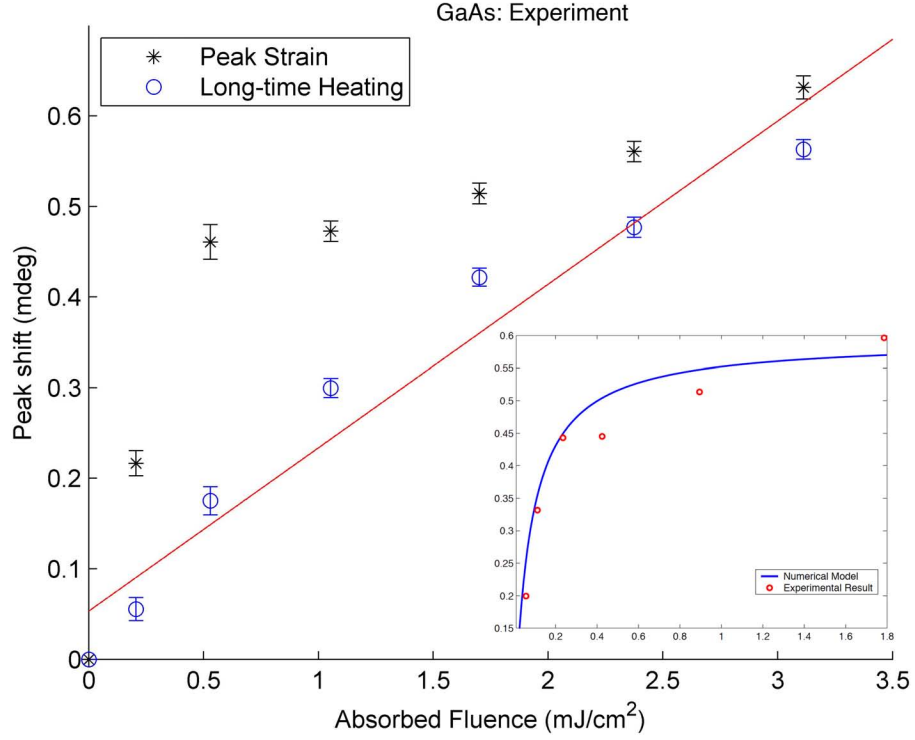


Figure 5.10: Thermal strain (blue) has a weak linear relationship with absorbed energy while the maximum peak shift (black) is nonlinear with laser fluence. A linear fit is performed on the data from the thermal regime with light agreement. Inset taken from [7] where the blue curve is a numerical model. It can be seen that the strain transition happens near the same fluence level in both cases.

regime continues to have a loosely linear response to fluence.

The rocking curve widths of GaAs in Figure 5.9 show a quick increase, qualitatively identical to that of InSb indicating that the lattice is thrown into a state of inhomogeneity. The recovery of the width, however, is quite different. Instead of recovering to within 15% of the original width, a gradient in the lattice spacing persists, taking nearly 1.5 ns to return to $\sim 15\%$ where it took InSb a mere 200 ps for the highest fluence case. The additional time necessary to bring the lattice spacing into equilibrium is driven by hot electrons interacting with and diffusing into the crystal.

In Figure 5.10, the maximum Bragg peak deflection is shown to be nonlinear with

respect to absorbed fluence. The abrupt change in the trend of peak shift (near 0.5 mJ/cm^2) has been observed in previous time-resolved strain experiments with nearly this transition threshold (see inset) [7].

GaAs is also a saturable absorber where the penetration depth is a function of the laser intensity. A possible explanation for the high fluence cases is that excited electrons are generated deeper than $1 \text{ }\mu\text{m}$ in the crystal. If carriers are located farther into the crystal, this would keep the lattice strained for a significant amount of time since the recombination rate is relatively small and the lifetime of electrons in the material is $\sim 1 \text{ ns}$.

5.4 Comparison with Models

Due to the majority of deposited energy being partitioned into thermal strain and the linear response in peak lattice distortion in InSb, the thermoelastic Thomsen model is an appropriate candidate. The Thomsen mode produces a linear peak strain (maximum distortion) and thermal strain ($> 2 \text{ ns}$ after excitation) response in diffraction simulations. Despite an underestimation in the impulsive strain response, the model shows qualitative agreement with the results obtained experimentally for InSb. In Figure 5.11, the diffraction simulation shows the equivalent plot to Figure 5.6 for InSb, highlighting the linearity of the model. The ratio between the two slopes do not correspond quantitatively with the observed lattice motions, but the general trend is consistent with data and physical intuition.

The Thomsen model roughly underestimates the strength of the acoustic pulse by a factor of 1.5. This may be attributed to the omission of electron contributions in the impulsive wave. By changing the acoustic pulse amplitude — creating a constant thermal profile at the surface with a different amplitude than the traveling pulse —

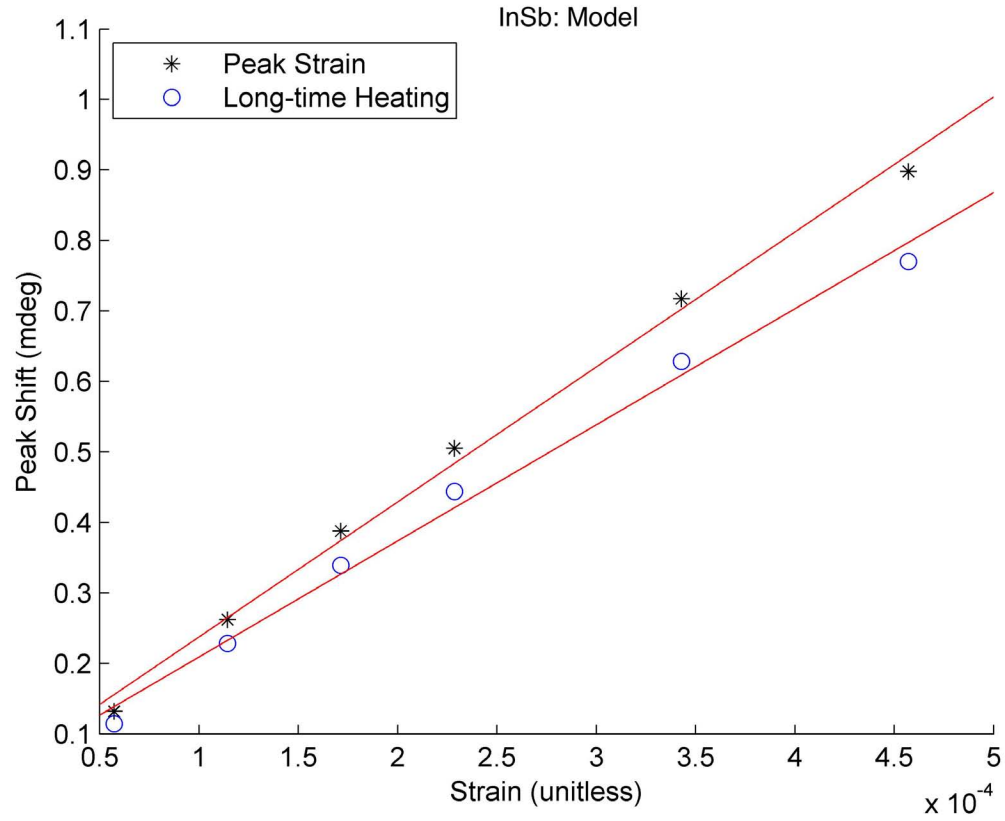


Figure 5.11: The Thomsen model shows peak strain and heating has a linear dependence with the amount of strain in the crystal. With InSb, the strain is directly related to the amount of absorbed energy. Although the ratio of the slopes contrast that of InSb data in Figure 5.6, the two are linear and represent the scalability of lattice response to absorbed energy.

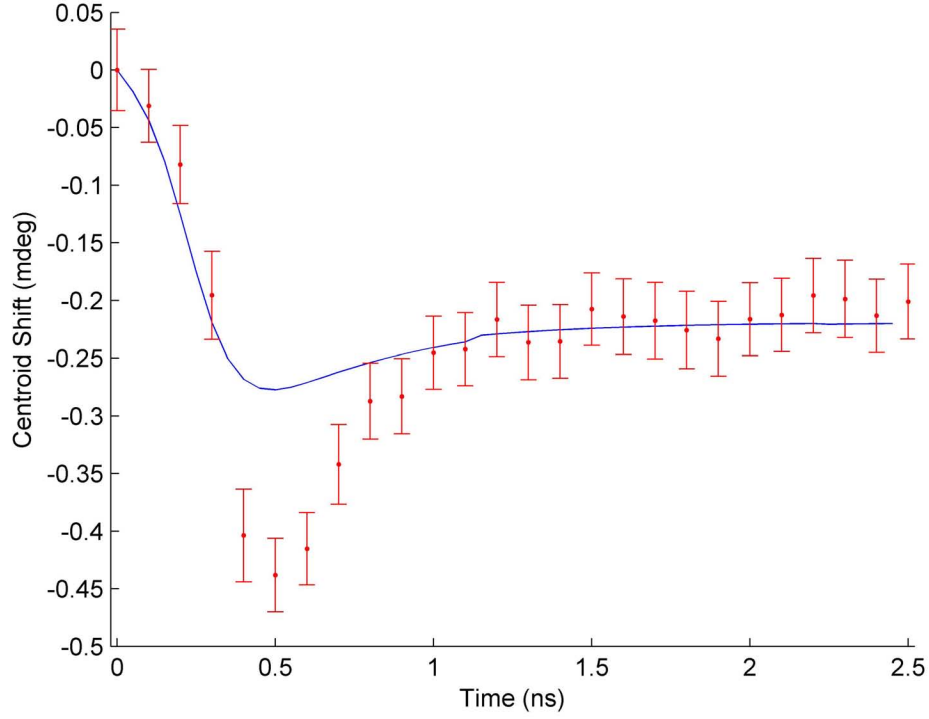


Figure 5.12: Thomsen model matched in the thermal regime to InSb data at 0.24 mJ/cm². The thermoelastic strain underestimates the contribution of non-thermal effects in the impulsive strain wave.

increases the peak strain response but fails to fully account for the magnitude of the impulsive component. Figure 5.12 shows the original, symmetric, Thomsen model with InSb data for the lowest fluence case. Since the Thomsen strain model is an analytic solution, numerical stability is not a problem. At high strain amplitudes, however, the leading edge of the bipolar strain is negative and results in a positive centroid shift. These high magnitudes of strain ($\sim 0.1\%$) lead to highly distorted and irregular diffraction patterns where a Gaussian approximation is no longer valid. For these cases, a center of mass analysis, is done to extract the center of the Bragg peak:

$$\text{Center of Mass} = \frac{\sum A_i \theta_i}{\sum A_i} \quad (5.4)$$

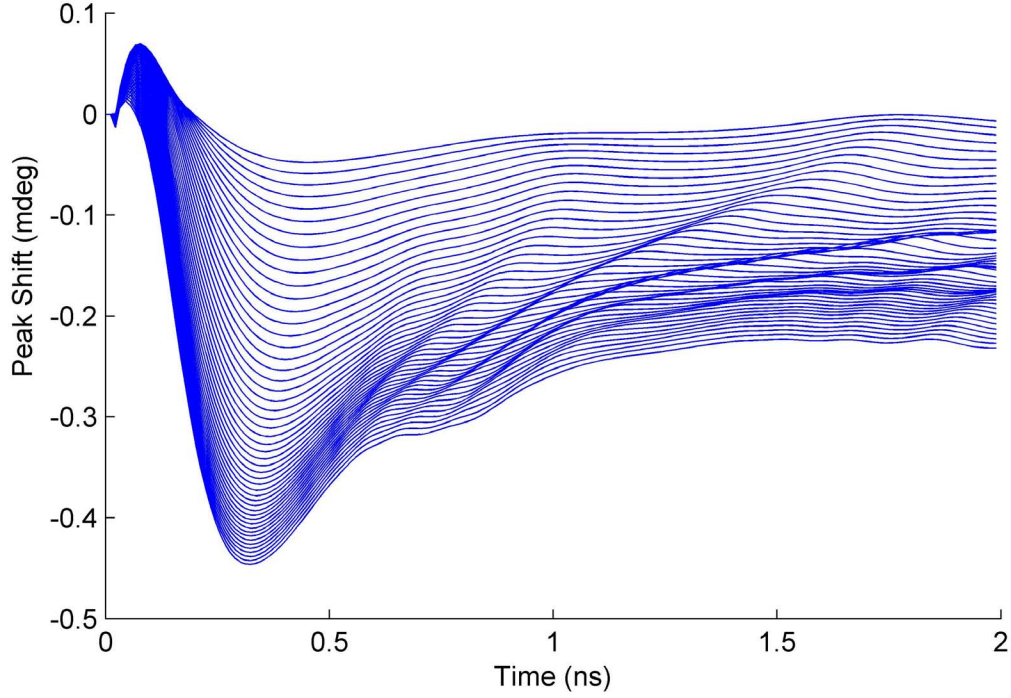


Figure 5.13: Time resolved centroid shifts calculated for GaAs with Auger recombination, electron diffusion, and thermal diffusion included shows a non-linear relation to fluence. Each plot is a even step size in fluence, and clearly shows the peak strain at a higher rate of saturation compared to the long-time condition. The ripple structure in the curves originate in the computation of the strain. To directly compare to data, the curves would be convoluted with a 100 ps gaussian, equivalent to the temporal resolution at the APS.

where A_i is the amplitude of the diffraction pattern in the i th column.

Qualitatively, the low fluence cases of GaAs are similar to that of any data set for InSb. Within the first nanosecond, the acoustic pulse disturbs the lattice producing a large shift in diffraction angle. Only thermal effects are detectable after the acoustic wave exists the x-ray extinction depth. The Thomsen model for GaAs, interestingly, appears to have similar characteristics to the high fluence data of Figure 5.8. This analysis, however, uses an inaccurate assumption that the highly energetic electrons in GaAs linearly couple with the lattice to produce strain. As shown in Equation 2.4,

the Auger recombination has a cubic dependence on the density and since the Auger recombination coefficient in GaAs is large, the resulting electron mean lifetime is ~ 1 ns.

As such, a different model is necessary to handle these nonlinear features. To accomplish this, the electron and thermal diffusion equations,

$$\frac{\partial n}{\partial t} = D_e \frac{\partial^2 n}{\partial z^2} - An^3 \quad \text{and} \quad \frac{\partial T}{\partial t} = D_t \frac{\partial^2 T}{\partial z^2} - An^3 \frac{E_g}{C}, \quad (5.5)$$

must be solved for all time and space within the confines of the simulation. Finally, the strain is propagated through the crystal depth using a one-dimensional wave equation,

$$\frac{\partial^2 u}{\partial t^2} = v^2 \frac{\partial^2 u}{\partial z^2}. \quad (5.6)$$

Since this process involves taking the derivatives of several functions, the step size and initial parameterization is important. This method produces strain profiles with similar characteristics to a driven traveling wave and produces centroid diffraction shifts better resembling data seen in InSb or the low fluence cases of GaAs. These simulations involve a nonlinear dependence on fluence where the lattice response begins to saturate at higher absorbed energies (see Figure 5.13). The nonlinearities, without the addition of a free parameter in the penetration depth, are naturally incorporated in this model. A plot of the largest lattice deflection and amount of strain, $\Delta d/d$, is given in Figure 5.14 which shows the nonlinear relation to strain and the approximately linear strain in the thermal region (> 2 ns). The transition into a nonlinear regime occurs around 0.4 mdeg, near where the GaAs data begins to behave nonlinearly. This imparts confidence into the theory behind this strain profile that

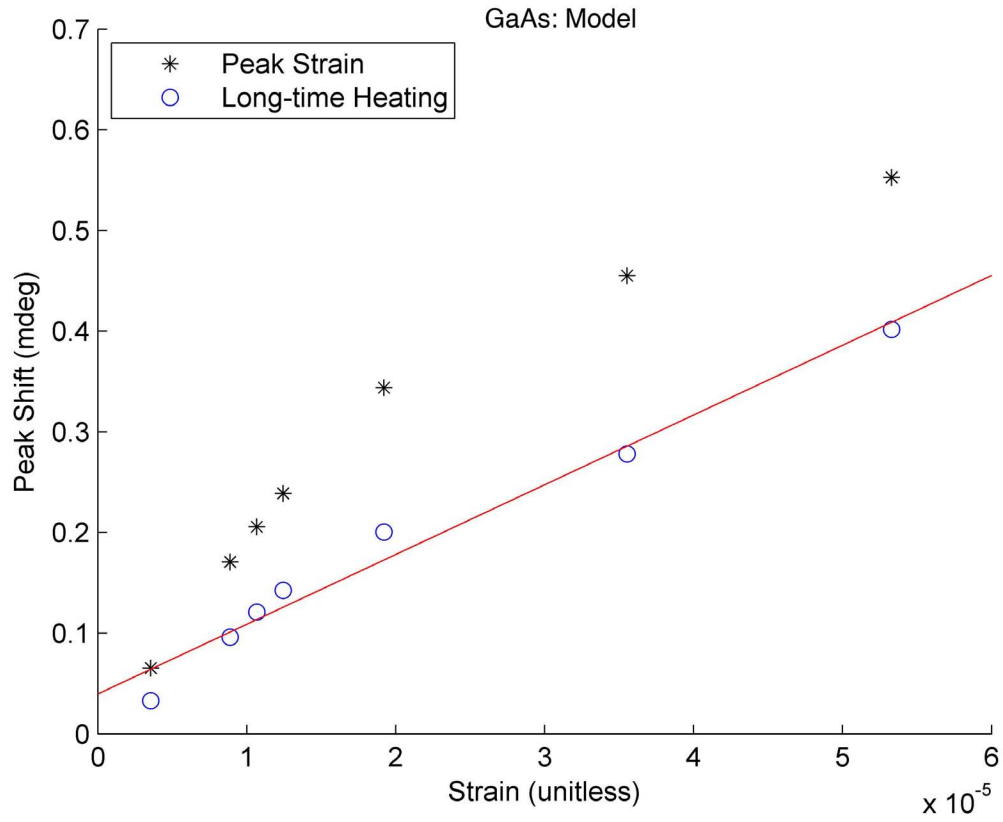


Figure 5.14: A nonlinear strain model shows that centroid shift due to heating has a rough linear dependence while the peak strain behaves nonlinear, even at low strain amplitudes. The trend of this simulation is similar to the data collected for GaAs and shown in Figure 5.10.

Auger recombination and electron diffusion must be contributing to the nonlinear response.

CHAPTER VI

Conclusions and Outlook

This thesis presents a study of strain and lattice dynamics in photo-excited InSb and GaAs. The techniques used to produce the high quality data can be extended to any time resolved diffraction experiment from any strong reflection. Additionally, a computer program was developed to calculate high resolution, benchmarked Bragg diffraction peaks for a strained crystal.

The diffraction data for InSb has a linear dependence on absorbed laser fluence. This is due to a partitioning of energy such that the majority transfers into the lattice as heat within the time resolution of these experiments. As the crystal heats, the lattice responds with linear expansion and generates a traveling acoustic impulsive wave. Future work will seek to achieve quantitative agreement between measured and modeled strain. We also anticipate that the next generation of x-ray sources with better temporal resolution may be able to capture transient nonlinearities in InSb.

For GaAs, a linear response to absorbed fluence was observed at long times following laser excitation, however, while the impulsive strain remained within the probe depth of the x-rays, the response is nonlinear. This can have several explanations. Our model shows qualitatively that strain saturation and recovery may be explained by a coupled charge and temperature distribution which is continuing to evolve at

the time and length scales accessible by this experiment. Other alternative explanations may also be tested against the high-quality time-resolved diffraction data and strain analysis code developed for this thesis. Such nonlinear strain generation processes may include free carrier absorption, carrier-carrier scattering, and saturable absorption.

In conclusion, this thesis has shown for the first time that the approach to thermal equilibrium in a laser-excited semiconductor does not necessarily follow a linear stress-strain relationship at short timescales, even far away from phase transitions. This opens up the possibility of real-time manipulations of non-equilibrium states in these systems and motivates a more nuanced understanding of this common and important process.

APPENDICES

APPENDIX A

Physical Properties of GaAs and InSb

Symbol	Parameter	GaAs	InSb	Unit
θ_B	Bragg Angle [400], 10 keV	23.18	28.89	deg
R	Reflectivity	0.039	0.144	Unitless
β	Linear Expansion	5.73×10^{-6}	5.37×10^{-6}	1/K
A	Laser Spot Size	38.30	27.82	mm ²
n	Index of Refraction	$3.644 + i0.089$	$4.4 + i0.637$	Unitless
ζ, d	Absorption Length	1	0.1	μm
C	Heat Capacity	1.096×10^7	7.203×10^6	eV/K/ μm^3
ν	Poisson's Ratio	0.31	0.35	Unitless
v	Sound Speed	4.73	3.4	$\mu\text{m}/\text{ns}$
ρ	Density	5.32×10^3	5.77×10^3	kg/m ³
B	Bulk Modulus (100)	75.3×10^9	40.9×10^9	Pa
E_g	Band Gap	1.424	0.17	eV
α_t	Thermal Expansion	5.73×10^{-6}	5.37×10^{-6}	1/K
α_e	Electronic Strain Coupling	2.019×10^{-11}	2.195×10^{-11}	μm^3
D_t	Temperature Diffusion	0.031	0.016	$\mu\text{m}^2/\text{ns}$
D_e	Electron Diffusion	10	200	$\mu\text{m}^2/\text{ns}$
A	Auger Recombination	1×10^{-15}	5×10^{-11}	$\mu\text{m}^6/\text{ns}$

Table A.1: Properties of GaAs and InSb at 300 K. Needed for calculations of Thomsen *et al.* and Decamp *et al.* strain models.

APPENDIX B

Ztec Oscilloscope Boot Protocol

Instructions for operating the Ztec Oscilloscope ZT4212 at 7IC-C.

Compiled by Eric Landahl, Dohn Arms, and Jackson Williams

For acquiring APD waveforms in proportional mode, the following should be noted:

APD output into Channel 1.

APD control voltage: 7.75 V.

APD high voltage: 210 V.

Detector is linear up to 100 mV.

Linearity can be corrected up to ~ 150 mV.

Laser trigger (Pockel's cell signal) to External Trigger.

An external delay box is helpful for moving this trigger to the correct bunch.

User Array Calcs need to be set up properly:

→ Array Variables: ztec:Inp1ScaledWave NPP NMS, Calculation: `-aa[00,500] - amin(nsmoo(-aa[95,120],5))`.

ScanH needs to be set up properly:

→ DetTriggers: ztec:OpInitiate, Detectors: ztec:Inp1ScaledWave, Settling: 1.5 s.

For the initial boot running from bantu (use current IP address):

```
export EPICS_CA_ADDR_LIST = 164.54.107.56
```


Check if oscilloscope is communicating:

```
caget ztec:UtilID
```

Operational setup for acquiring APD waveforms in proportional mode:

```
caput ztec:Inp1Wave.SCAN 7
caput ztec:Inp1ScaledWave.SCAN 7
caput ztec:Inp1ScaledTime.SCAN 7
caput ztec:setInp1Enable 1
caput ztec:setInp1Imped 50
caput ztec:setInp1Couple DC
caput ztec:setInp1Range 0.25
caput ztec:setTrigSource EXT
caput ztec:setTrigLevExt -0.5
caput ztec:setTrigSlope NEG
caput ztec:setTrigImpedExt 50
caput ztec:setTrigMode NORM
caput ztec:setTrigType EDGE
caput ztec:setAcqType AVER
caput ztec:setAcqCount 1024
caput ztec:setHorzOffset 0
caput ztec:setHorzTime 1e-6
caput ztec:setHorzPoints 512
```

APPENDIX C

Matlab Code

C.1 Strained Crystal Dynamical Diffraction Routines

C.1.1 Main Routine for Dynamical Diffraction

```
1 %% Main Routine for Dynamical Diffraction Simulation
2 % X_top.m
3 % Written by G.J. Williams
4 % Last Updated 6/7/2010
5 clear all; tic
6 %Choose initial parameters:
7 crystal = 1; % GaAs = 1, InSb = 2, Ge = 3
8 E = 10000; % Energy currently fixed at 10 keV
9 reflect = [4 0 0]; % Reflection fixed at [4 0 0]
10 T = 300; % Temperature (K)
11
12 % Find Atomic Form Factors, lattice parameters, reflection parameters:
13 [F_0,F_hkl,a,lambda,thetaB] = formf(reflect,crystal,E,T);
14 % Calculate psi_0 and psi_H (complex crystal susceptibilities):
15 [psi_0,psi_H] = X0H(F_0,F_hkl,a,lambda);
16
17 t_f = .5; % final time (must be in ns)
18 E_p = 1.55; % photon energy in eV
19 F = 4.5e-2; % Fluence in mJ/cm^2
20 fluence = F*6.242*10^7/E_p; % Fluence in photons/micron^2
21
22 [s,x,t] = FStrain(crystal,fluence,t_f); % Strain calculation
23
```

```

24 centshift = zeros(length(t),1);           % Preallocate space for centshift
25 for n = 1:length(t);                       % Time iteration loop
26
27     % Run the dynamical diffraction code for each time point
28     [cent,dtheta] = Wie(psi_0,psi_H,thetaB,lambda,s(:,n),x);
29     if(n == 1);                             % Reference point to measure change in centroid
30         cent0 = cent;                         % Initial (t = 0) centroid position
31     end
32     centshift(n) = cent - cent0;             % Calculate centroid shift
33 end
34 A1 = smooth(t,centshift);                   % Smoothing Function (running average)
35 if(crystal == 1);                           % Load Data for comparison
36     zzz = load('GaAs.all.txt');              % GaAs Data
37 elseif(crystal == 2);
38     zzz = load('InSb.all.txt');              % InSb Data
39 end
40
41 figure(6); clf; hold on
42 plot(t,A1,'b');
43 plot(t,centshift,'g');
44 errorbar(zzz(:,1),zzz(:,2),zzz(:,3),'k. ');
45 errorbar(zzz(:,1),zzz(:,4),zzz(:,5),'b. ');
46 errorbar(zzz(:,1),zzz(:,6),zzz(:,7),'r. ');
47 errorbar(zzz(:,1),zzz(:,8),zzz(:,9),'c. ');
48 errorbar(zzz(:,1),zzz(:,10),zzz(:,11),'g. ');
49 xlabel('Time (ns)');
50 ylabel('Centroid Shift (mdeg)');
51
52 t3 = toc;

```

C.1.2 Structure Factor

```

1 %% Subroutine for dynamical diffraction simulation
2 % Calculates atomic form factors
3 % Written by G.J. Williams
4 % Last Updated 6/7/2010
5 function [F_0,F_hkl,a,lambda,thetaB] = formf(reflect,crystal,E,T)
6 warning off all;
7
8 % Choose which crystal to use, load form factor data and lattice parameter
9 if(crystal == 1);
10     aa = load('Ga.txt');    bb = load('As.txt');    a = 5.65325;
11 elseif(crystal == 2);
12     aa = load('In.txt');    bb = load('Sb.txt');    a = 6.4789;
13 elseif(crystal == 3);
14     aa = load('Ge.txt. ');  bb = 0;                a = 5.64613;
15 elseif(crystal == 4);
16     aa = load('Zn.txt');    bb = load('S.txt');    a = 5.420;

```

```

17 elseif(crystal == 5);
18     aa = load('C.txt. ');      bb = 0;                a = 3.56683;
19 elseif(crystal == 6);
20     aa = load('Si.txt ');      bb = 0;                a = 5.43095;
21 else
22     fprintf('Warning: No Form Factor Could Be Calculated \n');
23 end
24
25 % Constants:
26 i = sqrt(-1);
27 planck = 4.13566733e-15;      % in ev*s
28 c = 299792458e10;            % in Angs/s
29 % Bragg's law calculations:
30 h = reflect(1); k = reflect(2); l = reflect(3);
31 d = a/sqrt(h^2 + k^2 + l^2);
32 Q = 2*pi/d;
33 lambda = planck*c/E;
34 theta2 = asin(lambda/(2*d))*2 * 180/pi;      % In degrees
35 thetaB = theta2/2 * pi/180;                  % In radians
36
37 % Load data for f' and f'' correction terms
38 fpp_data = aa(1:length(aa),3);
39 fp_data = aa(1:length(aa),2);
40 E1_data = aa(1:length(aa),1);
41 % Interpolate data at every 1 eV delineation
42 E1 = (min(E1_data):1:max(E1_data));
43 fpZ = interp1(E1_data,fp_data,E1);
44 fpp = interp1(E1_data,fpp_data,E1);
45 % Making sure the energy corresponds to the correct interpolated element
46 fp_aa = fpZ(E - min(E1) + 1);
47 fpp_aa = fpp(E - min(E1) + 1);
48
49 %% Finding f0.  Cromer-Mann coefficients taken from ruppweb, differs
50 % slightly from Cromer, DT and Mann, JB (Acta. Cryst. A., 1968)
51 % (http://www.ruppweb.org/new-comp/scattering\_factors.htm)
52 if(crystal == 1)      %Ga
53     a1 = 15.235; a2 = 6.701; a3 = 4.359; a4 = 2.962;
54     b1 = 3.067;  b2 = 0.241; b3 = 10.781; b4 = 61.414;
55     c = 1.719;
56 elseif(crystal == 2) % In
57     a1 = 19.162; a2 = 18.560; a3 = 4.295; a4 = 2.040;
58     b1 = 0.548;  b2 = 6.378; b3 = 25.850; b4 = 92.803;
59     c = 4.939;
60 elseif(crystal == 3) %Ge
61     a1 = 16.082;  a2= 6.375;  a3= 3.707;  a4 = 3.683;
62     b1 = 2.851;   b2= 0.252;  b3= 11.447; b4= 54.763;
63     c = 2.131;
64 elseif(crystal == 4) %Zn
65     a1 = 14.074;  a2= 7.032; a3= 5.165;  a4= 2.410;
66     b1 = 3.266;   b2= 0.233;  b3= 10.316; b4 = 58.710;
67     c = 1.304;
68 elseif(crystal == 5) % C
69     a1 = 2.310;   a2=1.020;  a3= 1.589;  a4 =0.865;
70     b1 = 20.844;  b2= 10.208; b3= 0.569;  b4= 51.651;

```

```

71     c    = 0.216;
72     elseif(crystal == 6)    % Si
73         a1 = 6.292; a2 = 3.035;  a3= 1.989;  a4=1.541;
74         b1 = 2.439; b2 = 32.334; b3=0.678;  b4= 81.694;
75         c = 1.141;
76     else
77         a1 = 0; a2 = 0; a3 = 0; a4 = 0;
78         b1 = 0; b2 = 0; b3 = 0; b4 = 0;
79         c = 0;
80     end
81     %Assimilate into: f0 = sum a_i*exp(b_i*(Q/4*pi)^2) + c:
82     f0_aa = c + a1*exp(-b1*(Q/(4*pi))^2) + a2*exp(-b2*(Q/(4*pi))^2)
83 + a3*exp(-b3*(Q/(4*pi))^2) + a4*exp(-b4*(Q/(4*pi))^2);
84     % Finding incident form factor:
85     f0_aa0 = c + a1 + a2 + a3 + a4;
86
87     % Data for the second atom in the crystal:
88     if(bb == 0);
89         f0_bb = f0_aa; fp_bb = fp_aa; f0_bb0 = f0_aa0; fpp_bb = fpp_aa;
90     elseif(bb ≠ 0);
91         % Load data
92         fpp_data = bb(1:length(bb),3);
93         fp_data = bb(1:length(bb),2);
94         E1_data = bb(1:length(bb),1);
95         % Interpolate data
96         E1 = (min(E1_data):1:max(E1_data));
97         fpZ = interp1(E1_data,fp_data,E1);
98         fpp = interp1(E1_data,fpp_data,E1);
99         fp_bb = fpZ(E - min(E1) + 1);
100        fpp_bb = fpp(E - min(E1) + 1);
101        if(crystal == 1)
102            a1 = 16.672; a2 = 6.070; a3 = 3.431; a4 = 4.278;
103            b1 = 2.635;  b2 = 0.265; b3 = 12.948;b4 = 47.797;
104            c = 2.531;
105        elseif(crystal == 2)
106            a1 = 19.642; a2 = 19.045; a3 = 5.037;  a4 = 2.683;
107            b1 = 5.303;  b2 = 0.461;  b3 = 27.907; b4 = 75.283;
108            c = 4.591;
109        elseif(crystal == 4)
110            a1 = 6.905; a2= 5.203;  a3= 1.438;  a4= 1.586;
111            b1 = 1.468;    b2= 22.215; b3= 0.254;  b4= 56.172;
112            c = 0.867;
113        else
114            % keep all a_i,b_i,c constants the same
115        end
116        % f0 = sum(a_i * exp(-b_i * Q^2)) + c
117        f0_bb = c + a1*exp(-b1*(Q/(4*pi))^2) + a2*exp(-b2*(Q/(4*pi))^2) ...
118 + a3*exp(-b3*(Q/(4*pi))^2) + a4*exp(-b4*(Q/(4*pi))^2);
119        % Incident scattering power
120        f0_bb0 = c + a1 + a2 + a3 + a4;
121    end
122    %% Compiling the Atomic Form Factors
123    % Debye-Waller Factor [M.in M.sb] = debye(crystal,temperature)
124    [u2_aa u2_bb] = debye(2,T);

```

```

125 M_aa = 8*pi^2/3*(sin(thetaB)/lambda)^2*(u2_aa); %
126 M_bb = 8*pi^2/3*(sin(thetaB)/lambda)^2*(u2_bb); %
127 % Atomic form factor:
128 f_aa = (f0_aa + fp_aa + i*fpp_aa)*exp(-M_aa);
129 f_bb = (f0_bb + fp_bb + i*fpp_bb)*exp(-M_bb);
130 % Atomic form factor for reflection [0 0 0], needed for F_0
131 f_aa0 = f0_aa0 + fp_aa + i*fpp_aa; % — these also seem reasonable
132 f_bb0 = f0_bb0 + fp_bb + i*fpp_bb;
133 % Full structure factor for the InSb crystal.
134 F_0 = 4*(f_aa0 + f_bb0);
135 F_hkl = f_aa*(1 + exp(pi*i*(h+k))+exp(pi*i*(h+l))+exp(pi*i*(k+l))) ...
136 +f_bb*(exp(.5*pi*i*(h+k+l))+exp(.5*pi*i*(3*h+3*k+l)) ...
137 +exp(.5*pi*i*(3*h+k+3*l))+exp(.5*pi*i*(h+3*k+3*l)));
138 end

```

C.1.3 Calculating the Debye-Waller Coefficient

```

1 %% Subroutine for dynamical diffraction simulation
2 % debye.m
3 % Calculates Debye-Waller factors
4 % Written by G.J. Williams
5 % Last Updated 6/7/2010
6
7 function [M1,M2] = debye(crystal,T)
8
9 temp = [0.001 100 200 400 600 800 1000];
10 temperature = 1:1:1000;
11
12 if(crystal == 1); %GaAs
13     e1 = [1.858e-3 3.397e-3 6.038e-3 0.011658 0.017368 0.023101 0.028844];
14     e2 = [1.632e-3 2.949e-3 5.201e-3 0.010014 0.014909 0.019827 0.024754];
15 elseif(crystal == 2); %InSb
16     e1 = [1.958e-3 6.102e-3 0.011711 0.023163 0.034671 0.046194 0.057723];
17     e2 = [1.724e-3 5.274e-3 0.010085 0.019926 0.029821 0.039728 0.049642];
18 elseif(crystal == 3); %Ge — both atoms in the structure are the same
19     e1 = [2.471e-3 3.196e-3 4.865e-3 8.772e-3 0.01287 0.017022 0.021198];
20     e2 = [2.471e-3 3.196e-3 4.865e-3 8.772e-3 0.01287 0.017022 0.021198];
21 elseif(crystal == 4); %ZnS
22     e1 = [2.229e-3 3.942e-3 7.046e-3 0.013641 0.020335 0.027053 0.033781];
23     e2 = [2.425e-3 3.504e-3 5.565e-3 0.010258 0.015132 0.020054 0.024997];
24 elseif(crystal == 5); %C
25     e1 = [1.611e-3 1.626e-3 1.690e-3 1.986e-3 2.436e-3 2.962e-3 3.529e-3];
26     e2 = [1.611e-3 1.626e-3 1.690e-3 1.986e-3 2.436e-3 2.962e-3 3.529e-3];
27 elseif(crystal == 6); %Si
28     e1 = [1.718e-3 3.191e-3 5.665e-3 0.01093 0.01628 0.021653 0.027035];
29     e2 = [1.718e-3 3.191e-3 5.665e-3 0.01093 0.01628 0.021653 0.027035];
30 else
31     fprintf('Warning: Debye Waller Factor could not be calculated \n');

```

```

32     e1 = [0 0 0 0 0 0 0];
33     e2 = [0 0 0 0 0 0 0];
34 end
35 debye1 = interp1(temp,e1,temperature);
36 debye2 = interp1(temp,e2,temperature);
37
38 M1 = debye1(T);
39 M2 = debye2(T);
40 end

```

C.1.4 Determining $\psi_{0,H}$

```

1 %% Subroutine for dynamical diffraction simulation
2 % X0H.m
3 % Calculates susceptibilities
4 % Written by G.J. Williams
5 % Last Updated 6/7/2010
6 function [psi_0,psi_H] = X0H(F_0,F_hkl,a,lambda)
7 a = a*10^-10; % in meters
8 V = a^3; % Volume in m^3
9 e = 1.60217733*10^-19; % in C
10 m = 9.1093897*10^-31; % in kg
11 c = 299792458; % in m/s
12 e0 = 8.854187817*10^-12; % F/m
13 lambda = lambda*10^-10; % in meters
14 F_0H = F_0; % Undamaged structure factor
15 F_H = F_hkl; % Debye factor already taken care of.
16 % Structure parameter of incident wave
17 psi_0 = -(e^2/(m*c^2))*(lambda^2/pi)*(F_0H/V)/(4*pi*e0);
18 % Structure parameter of diffracted wave
19 psi_H = -(e^2/(m*c^2))*(lambda^2/pi)*(F_H/V)/(4*pi*e0);
20 end

```

C.1.5 Takagi-Taupin Rocking Curves

```

1 %% Subroutine for dynamical diffraction simulation
2 % Wie.m
3 % Calcualtes strained crystal diffraction peaks
4 % Written by G.J. Williams
5 % Last Updated 6/7/2010
6 % Everything in this program should be in SI units
7 function [cent,dtheta] = Wie(psi_0,psi_H,thetaB,lambda,s,x)
8

```

```

9  strain = flipud(s);
10 lambda = lambda*10^-10;
11
12 psi_0r = real(psi_0);      psi_0i = imag(psi_0);
13 psi_Hr = real(psi_H);      psi_Hi = imag(psi_H);
14
15 angstep = 10^-6;           % Angular steps (keep fixed at 1 urad)
16 nmax = 300;                % 300 angular steps
17 A00 = max(x)*10^-6;        % Size of crystal (depth) (
18 jmax = length(x);          % 2000 depth steps
19 dstep = A00/(jmax - 1);    % step size is 2.5 nm
20
21 pXtop = zeros(1,nmax); ptheta = zeros(1,nmax);    % Preallocating Space
22
23 for n = 1:nmax              % Angluar loop
24     % Calculate angluar range
25     theta = thetaB - 0.4*nmax*angstep + n*angstep ;
26     % Ratio of the deffracted/incident cosines
27     b = 1;    % For symmetric Bragg reflections, b = 1
28     % Incident absorbtion parameter
29     g = ((1+b)*psi_0i)/(2*abs(psi_Hr)*sqrt(b));
30     % Diffracted absorption parameter
31     k = psi_Hi/psi_Hr;
32     % Difrection of cosines
33     gamma_0 = cos(pi/2 - thetaB);
34     gamma_H = cos(pi/2 - thetaB);
35
36     for j = 1:jmax          % Depth loop
37         z = (A00 - (j)*dstep);    % Iterating through the crystal depth
38
39         e1 = strain(j);          % Import strain depth position
40         % For the first step, A01 is the infinite crystal solution
41         A01 = (A00)*(pi*abs(psi_Hr))/(lambda*sqrt(gamma_H*gamma_0));
42         % Normalizing iterative crystal depth
43         A = (pi*z*abs(psi_Hr))/(lambda*sqrt(gamma_H*gamma_0));
44         % Strain coefficient
45         c1 = 2*sin(2*thetaB)*tan(thetaB);
46
47         % Angle between the surface and reflecting plane is zero, c2 = 0
48         c2 = 0;
49         e2 = 0;                  % e2 set to 0 for consistency.
50         % Angle of reflection (independent variable)
51         alpha = -2*(theta - thetaB)*sin(2*thetaB) - (c1*e1 + c2*e2);
52         % Deviation from Bragg angle
53         y = ((1+b)*psi_0r - b*alpha)/(2*abs(psi_Hr)*sqrt(b));
54
55         % Taking the square root of a complex number
56         r1 = abs(y^2 - g^2 + k^2 - 1);    % APPENDIX FROM WIE et al.
57         r2 = 2*(y*g - k);
58         r = sqrt(r1^2 + r2^2);
59         s1 = sqrt((r+r1)/2);
60         s2 = sqrt((r-r1)/2);
61         q1 = sqrt(1 - k^2 + g^2);
62         q2 = k/g;

```



```

63     i = sqrt(-1);
64     if(y ≤ - q1)
65         s = s1 + i*s2;
66     elseif(y ≤ q2) && (y ≥ -q1)
67         s = s2 + i*s1;
68     elseif(y ≤ q1) && (y ≥ q2)
69         s = -s2 + i*s1;
70     elseif(y ≥ q1);
71         s = -s1 + i*s2;
72     else
73         fprintf('Error found in taking the square root');
74     end
75     i = sqrt(-1);
76     B = -(1+i*k);
77     C = y + i*g;
78     X0 = -B/(C - s); % Zero-strain solution
79
80     if(j == 1)
81         Xj = X0; % Start with zero strain solution
82         A0 = A01; % Start with infinite depth
83     end
84
85     % Diffraction solution
86     Xj = (s*Xj + i*(B+C*Xj)*tan(s*(A - A0)))/(s - i*(C+B*Xj)*tan(s*(A - A0)));
87     A0 = A; % Update A0 as the previous A value
88 end
89
90     pXtop(n) = Xj; % Top layer soln vs theta
91     ptheta(n) = theta; % Theta for plotting
92
93 end
94 amp = conj(pXtop).*pXtop; % Total reflecting intensity
95 dtheta = (ptheta - thetaB)*180/pi*1000; % In mdeg
96
97 % Angular Convolution
98 width = 2.5; % Double Crystal curve FWHM of Diamond (111) in mdeg
99 c = width*1/(2*sqrt(2*log(2))); % Convert from FWHM to "tau"
100 a = dtheta; % Independent variable
101
102 b1 = 0;
103 G = exp(-(a-b1).^2/(2*c^2)); % Angular Gaussian to convolute
104 convamp = conv2(amp,G,'same'); % Convolution function
105 % Normalization value (same size as amp)
106 convamp = max(amp)/max(convamp)*convamp;
107
108 f = fitype('gauss1'); % Fitting a single gaussian to peak
109 ffit = fit(dtheta',convamp',f);
110 params = coeffvalues(ffit); % Extracting fit parameters
111 cent = params(2); % Extraction centroid positon
112 end

```

C.1.6 Thomsen Strain Model for GaAs

```

1 %% strain.m
2 % Written by G. Jackson Williams 6/7/2010
3 % strainInSb.m creates the Thomsen strain for GaAs
4
5 function [strain] = strainGaAs(z,t,thetaB)
6 lambda = 800*10^-9;           % Center wavelength of laser (m)
7
8 % These numbers are for GaAs ONLY
9 H = 3.1894;                   % Width of beam (mm)
10 V = 4.7264/sin(thetaB);      % Height of beam (mm) (adjusted for the angle)
11 A = H*V*10^-6;               % Area of beam spot (m^2)
12
13 RepRate = 1000;               % Repetition Rate of the Laser (Hz)
14 P = 0.39;                     % Power (Watts)
15 Q = P/RepRate;               % Energy of the pulse (J)
16
17 C = 1.739*10^6;               % Heat Capacity (J/m^3-K)
18 nu = 0.31;                    % Poisson's Ratio (unitless)
19 Y = 75.3*10^9;                % Youngs Modulus in (100) direction(Pa)
20 rho = 5.317*10^3;             % Denisity (kg/m^3)
21 beta = 5.73*10^-6;           % Coefficient of Thermal Expansion (1/K)
22
23 P = 1;                         % Light is P polarization
24 S = 0;
25
26 n1 = 1;                        % Index of refraction of air
27 n = 3.664;                     % Index of Refraction n(Real) for GaAs
28 k = 0.089;                    % n(Imag) for GaAs
29 n2 = n + i*k;                 % Complex index of refraction for GaAs
30
31 % Finding the reflectation coefficient of light for GaAs
32 theta = (pi/2 - thetaB);
33 theta2 = asin(n1*sin(theta)/n2);
34 r_p = (-n2*cos(theta) + n1*cos(theta2))/(n2*cos(theta) + n1*cos(theta2));
35 r_s = -(n1*cos(theta) - n2*cos(theta2))/(n1*cos(theta) + n2*cos(theta2));
36
37 R_p = conj(r_p)*r_p;
38 R_s = conj(r_s)*r_s;
39 R = S*R_s + P*R_p;            % Reflectivity coefficient of light
40
41 alpha = k*pi*4/lambda;        % absorbtion coefficient
42 zeta = 1/alpha;               % Penetration depth (700 nm)
43
44 v = sqrt(3*(1-nu)/(1+nu)*Y/rho); % Speed of Sound (100) (m/s)
45
46 strain = (1-R).*Q.*beta./(A.*zeta.*C).*(1+eta)./(1-eta).*(exp(-z./zeta)...
47 .* (1-0.5.*exp(-v.*t./zeta))-0.5.*exp(-abs(z-v.*t)./zeta).*(sign(z-v.*t)));
48 end

```

C.1.7 Thomsen Strain Model for InSb

```

1 %% strainInSb.m
2 % Written by G. Jackson Williams 6/7/2010
3 % strainInSb.m creates the Thomsen strain for InSb
4
5 function [strain] = strainInSb(z,t,thetaB)
6 lambda = 800*10^-9;           % Center wavelength of laser (m)
7
8 % These numbers are for InSb ONLY
9 H = 4.2105;                   % Width of beam (mm)
10 V = 3.1924/sin(thetaB);      % Height of beam (mm) (adjusted for the angle)
11 A = H*V*10^-6;               % Area of beam spot (m^2)
12
13 RepRate = 5000;               % Repetition Rate of the Laser (Hz)
14 P = 0.39;                     % Power (Watts)
15 Q = P/RepRate;                % Energy of the pulse (J)
16
17 C = 1.154*10^5;               % Specific Heat (J/m^3-K)
18 nu = 0.35;                    % Poison's Ratio (unitless)
19 Y = 40.9*10^9;                % Youngs Modulus for the (100) direction (Pa)
20 rho = 5.77*10^3;              % Denisity (kg/m^3)
21 beta = 5.37*10^-6;            % Coefficient of Thermal Expansion (1/K)
22
23 P = 1;                         % Light is P polarization
24 S = 0;
25
26 n1 = 1;                        % Index of refraction of air
27 n = 4.4;                       % Index of Refraction n(Real) for InSb
28 k = 0.63662;                  % n(Imag) for InSb
29 n2 = n + i*k;                 % Complex index of refraction for InSb
30
31 % Finding the reflectation coefficient of light for InSb
32 theta = (pi/2 - thetaB);
33 theta2 = asin(n1*sin(theta)/n2);
34 r_p = (-n2*cos(theta) + n1*cos(theta2))/(n2*cos(theta) + n1*cos(theta2));
35 r_s = -(n1*cos(theta) - n2*cos(theta2))/(n1*cos(theta) + n2*cos(theta2));
36
37 R_p = conj(r_p)*r_p;
38 R_s = conj(r_s)*r_s;
39 R = S*R_s + P*R_p;             % Reflectivity coefficient of light
40
41 alpha = k*pi*4/lambda;         % absorbtion coefficient
42 zeta = 1/alpha;                % Penetration depth (100 nm)
43
44 v = sqrt(3*(1-nu)/(1+nu)*Y/rho); % speed of sound in the (100) direction
45
46 strain = (1-R).*Q.*beta./(A.*zeta.*C).*(1+eta)./(1-eta).*(exp(-z./zeta)...
47 .* (1-0.5.*exp(-v.*t./zeta))-0.5.*exp(-abs(z-v.*t)./zeta).*(sign(z-v.*t)));
48 end

```

C.1.8 Asymmetric Thermoelastic Model for InSb

```
1 %% strainInSb1.m
2 % Written by G. Jackson Williams 6/7/2010
3 % Asymmetric Thomsen model strain using Auger and deformation potential
4
5 function [strain] = strainInSb1(z,t)
6 % z has units of meters, t has units of s, v has units of m/s
7 % Everything else is um, ns, eV, K
8 % Returns a matrix of strain elements for a particular time point.
9
10 fluence = 9e6;           % Fluence           (photons/um^2)
11
12 E_p = 1.55;              % Photon energy      (eV)
13 E_g = 0.17;              % Bandgap          (eV)
14 C = 7.203*10^6;          % Specific Heat     (ev/K/um^3)
15 d = 0.1;                 % Penetration Depth (um)
16 d1 = d*10^-6;            % Penetration Depth (m)
17 v = 3.4*10^3;            % Speed of Sound    (m/s)
18 alpha_e = 2.195*10^-11; % electronic coupling (um^3)
19 alpha_t = 5.37*10^-6;    % Thermal expansion (1/K)
20
21 strain = alpha_t.*(E_p-E_g).*fluence./C./d.*exp(-z./d1) - ...
22 alpha_e.*fluence./d.*(1/2.*exp((-z-v.*t)./d1) + ...
23 1/2.*exp(-abs(z-v.*t)/d1).*sign(z-v.*t));
24 end
```

C.2 Data Reduction and Analysis

C.2.1 Main Routine for GaAs Data Extraction

```
1 %% Angshift_GaAs.m
2 % Written by G. Jackson Williams 9/1/2009
3 % Top routine to analyze a 2-D diffraction scan.
4
5 clear all;
6 format short g;
7 hmax = 6;           % Number of waveplate points in the scan
8 tic                % Start the timer for the program
9
10 for h = 1:hmax      % For each waveplate scan, do a centroid analysis
11
12     [Dth,time,Etot,n,m] = chomplite_GaAs(h);
13     if(h == 1);      % 0.211 W
14         Dth1(1:n) = Dth;
15         E1(1:n) = Etot/2;
16         time1(1:n) = time;
17     elseif(h == 2);  % 1.24 W
18         Dth2(1:n) = Dth;
19         E2(1:n) = Etot/2;
20     elseif(h == 3);  % 0.678 W
21         Dth3(1:n) = Dth;
22         E3(1:n) = Etot/2;
23     elseif(h == 4);  % 0.964 W
24         Dth4(1:n) = Dth;
25         E4(1:n) = Etot/2;
26     elseif(h == 5);  % 0.082 W
27         Dth5(1:n) = Dth;
28         E5(1:n) = Etot/2;
29     else              % 0.420 W
30 %——Experimental Problems occurred on this run. Do not use in Analysis——
31         Dth6(1:n) = Dth;
32         E6(1:n) = Etot/2;
33     end
34 end
35
36 % Calculating the peak shift and residual heating of the crystal
37 % power    = laser power meter readings (in W)
38 % strain    = maximum centroid shift (in mdeg)
39 % heat      = averaged data from 1.5 ns to the end of the data run
40 % Estrain   = error associated with the strain measurment at particular time
41 % Eheat     = error associated with heat measurement
42 power = [0;0.082;0.211;0.42;0.678;0.946;1.24];
43 strain = -1*[0;min(Dth5);min(Dth1);min(Dth6);min(Dth3);min(Dth4);min(Dth2)];
44 heat = -1*[0;mean(Dth5(15:n));mean(Dth1(15:n));mean(Dth6(15:n)); ...
45     mean(Dth3(15:n));mean(Dth4(15:n));mean(Dth2(15:n))];
46 Estrain = [0;E5(4);E1(4);E6(4);E3(4);E4(4);E2(4)];
```

```

47 Eheat = [0;mean(E5(15:n));mean(E1(15:n));mean(E6(15:n));mean(E3(15:n)); ...
48         mean(E4(15:n));mean(E2(15:n))];
49
50 H = 3.1894*10^-3; % Horizontal laser spot on sample
51 V = 4.7264*10^-3/sin(23.178*pi/180); % Vertical laser spot on sample
52 Area = V*H; % Total beam spot
53 reptime = 1000; % Laser repetition rate
54 E = power./reptime; % Energy deposited on sample
55 R = .03887; % Reflectivity of S polarized light
56 Aflue = E./Area.*(1 - R)./10; % Absorbed laser fluence on sample
57
58 f = fittype('poly1'); % Fit heat strain to linear slope
59 ffit = fit(Aflue,heat,f);
60
61 f1 = strcat(num2str(Aflue(2)), ' mJ/cm^2'); % Create strings for legend
62 f2 = strcat(num2str(Aflue(3)), ' mJ/cm^2');
63 f3 = strcat(num2str(Aflue(4)), ' mJ/cm^2');
64 f4 = strcat(num2str(Aflue(5)), ' mJ/cm^2');
65 f5 = strcat(num2str(Aflue(6)), ' mJ/cm^2');
66
67 % Plot centroid shift as a function of time for 5 fluences with error bars
68 figure(15); clf; hold on
69 errorbar(time2,Dth5,E5, '.k-'); % 0.082 W
70 errorbar(time1,Dth1,E1, '.b-'); % 0.211 W
71 % errorbar(time,Dth6,E6, '.m-'); % 0.420 W **** DO NOT USE ****
72 errorbar(time1,Dth3,E3, '.r-'); % 0.678 W
73 errorbar(time1,Dth4,E4, '.c-'); % 0.964 W
74 errorbar(time1,Dth2,E2, '.g-'); % 1.24 W
75 xlabel('Time (ns)');
76 ylabel('Peak Shift (mdeg)');
77 title('GaAs');
78 legend({f1;f2;f3;f4;f5}, 'Location', 'SouthEast');
79 xlim([-0.3 3]);
80
81 % Plot peak strain and residual heat with error bars
82 figure(13); clf; hold on;
83 errorbar(Aflue, strain, Estrain, 'k*');
84 errorbar(Aflue, heat, Eheat, 'bo');
85 plot(ffit);
86 xlim([0 3.5]);
87 ylim([0 0.7]);
88 xlabel('Absorbed Fluence (mJ/cm^2)');
89 ylabel('Peak shift (mdeg)');
90 title('GaAs');
91 legend('Peak Strain', 'Long-time Heating', 'Location', 'NorthWest')
92
93 t = toc; % Stop the clock

```

C.2.2 Extract Centroid Shifts for Each Fluence for GaAs

```
1 %% chomplite.m
2 % Written by G. Jackson Williams 9/1/2009
3
4 % This is a subroutine to a program takes a modified .mda file from any
5 % time resolved diffraction data and outputs peak shift vs time.
6 % This one is for GaAs data.
7
8 function [Dth,time,Etot,n,m] = chomplite_GaAs(h)
9 % Load scans. These were done as individual rocking curve scans thru time
10 if(h == 1)
11     a = load('-ascii','7idc_0789.txt'); % n time points
12     m = 21; n = 31; % m angular points
13 elseif(h == 2)
14     a = load('-ascii','7idc_0794.txt');
15     m = 41; n = 31;
16 elseif(h == 3)
17     a = load('-ascii','7idc_0792.txt');
18     m = 41; n = 31;
19 elseif(h == 4)
20     a = load('-ascii','7idc_0784.txt');
21     m = 41; n = 31;
22 elseif(h == 5)
23     a = load('-ascii','7idc_0787.txt');
24     m = 41; n = 31;
25 else
26     a = load('-ascii','7idc_0778_0780_0781.txt');
27     m = 41; n = 29;
28 end
29
30
31 for i = 1:n; % For a total of "n" time steps
32
33     if(i == 1) % "m" angular points. p is carried through
34         A = p + 1:p + m; % to index the entire scan file.
35     else
36         A = max(A)+1:max(A)+m;
37     end
38
39     lsroff = a(A,19); % APD data for Laser Off bucket
40     lsron = a(A,20); % APD data for Laser on bucket
41     angle = a(A,2); % Theta positioner
42 % ** lsroff, lsron data normalized by hand for top-up occurrences. No need
43 % to normalize to upstream counting APD as it introduces more uncertainty
44     Eon = .001*max(lsron).*ones(1,length(angle));
45     Eoff = .001*max(lsroff).*ones(1,length(angle));
46
47     [outon] = gaussfit(angle,lsron,Eon);
48     [outoff] = gaussfit(angle,lsroff,Eoff);
49
```

```

50     centeroff(:,i) = outoff(1); % Store centroid positions, error
51     Ecentoff(:,i) = outoff(2); % Can not easily preallocate —> n changes
52
53     centeron(:,i) = outon(1);
54     Ecenton(:,i) = outon(2);
55
56 end
57 dtime = .1; % Each time step is 100 ps
58 time = dtime*(0:i-1); % Start time at t = 0
59
60 Dth = (centeron - centeroff)*1000; % Taking the peak shift, in mdeg
61 Etot = (Ecentoff + Ecenton)*1000; % Error in the peak shift, in mdeg
62 end

```

C.2.3 Main Routine for InSb Data Extraction

```

1 %% Angshift_InSb.m
2 % Written by G. Jackson Williams 9/1/2009
3 % Top routine to analyze a 3-D diffraction scan.
4 %Runs through the 3-D scan of 7idc-0040.txt for InSb at different fluences
5 clear all;
6 format short g;
7
8 p = 0; % Initiating angular indexing
9 m = 81; % Number of angular points in scan
10 n = 26; % Number of time points in scan
11 hmax = 5; % Number of waveplate points in the scan
12 shift = zeros(hmax,n); % Preallocate space for shift matrix
13 tic % Start the timer for the program
14
15 % Calculating the peak shift and residual heating of the crystal
16 power = [0;0.39;0.74;1.20;1.71;2.20]; % Power meter reading (in W)
17 H = 4.2105*10^-3; % Horizontal beam spot on sample (m)
18 thetaB = 28.89*pi/180; % Bragg angle (in radians)
19 V = 3.1924*10^-3/sin(thetaB); % Vertiacal beam spot on sample (m)
20 Area = V*H; % Beam spot area
21 replate = 5000; % Repetition rate of Laser (Hz) (approx)
22 E = power./replate; % Energy delivered on the sample
23 R = .14368; % Reflectivity (S-polarized) of InSb
24 Aflue = E./Area.*(1 - R)./10; % Absorbed laser fluence on the sample
25
26 for h = 1:hmax % For each waveplate scan, do a centroid analysis
27     [Dth,time,p,Etot] = chomplite_InSb(p,m,n);
28     shift(h,1:n) = Dth; % Store the centroid analysis array
29     E(h,1:n) = Etot/2; % Store error in centroid fit
30 end
31
32 % Split up shift matrix for ease of understanding

```



```

33 % All arrays are in increasing order of absorbed fluence
34 % Dth(X) = centroid shift for fluence index
35 % E(X) = error in centroid shift for fluence index
36 Dth1 = shift(1,1:n);    Dth2 = shift(2,1:n);
37 Dth3 = shift(3,1:n);    Dth4 = shift(4,1:n);    Dth5 = shift(5,1:n);
38 E1 = E(1,1:n); E2 = E(2,1:n); E3 = E(3,1:n); E4 = E(4,1:n); E5 = E(5,1:n);
39
40 f1 = strcat(num2str(Aflue(2)), ' mJ/cm^2');
41 f2 = strcat(num2str(Aflue(3)), ' mJ/cm^2');
42 f3 = strcat(num2str(Aflue(4)), ' mJ/cm^2');
43 f4 = strcat(num2str(Aflue(5)), ' mJ/cm^2');
44 f5 = strcat(num2str(Aflue(6)), ' mJ/cm^2');
45
46 % Plot of the centroid shifts
47 figure(10); clf; hold on
48 errorbar(time,Dth1,E1, '.b-');
49 errorbar(time,Dth2,E2, '.g-');
50 errorbar(time,Dth3,E3, '.r-');
51 errorbar(time,Dth4,E4, '.c-');
52 errorbar(time,Dth5,E5, '.m-');
53 ylim([-2.2 0]);
54 xlabel('Time (ns)');
55 ylabel('Peak Shift (mdeg)');
56 title('InSb');
57 %legend(f1,f2,f3,f4,f5,'Location','SouthEast');
58
59 % Calculating the peak shift and residual heating of the crystal
60 % strain = maximum centroid shift (in mdeg)
61 % heat = averaged data from 1.5 ns to the end of the data run
62 % Estrain = error associated with the strain measurment at particular time
63 % Eheat = error associated with heat measurement
64 strain = -1*[0;min(Dth1);min(Dth2);min(Dth3);min(Dth4);min(Dth5)];
65 Estrain = [0;E1(6);E2(6);E3(6);E4(6);E5(6)];
66 heat = -1*[0;mean(Dth1(10:n));mean(Dth2(10:n));mean(Dth3(10:n)); ...
67 mean(Dth4(10:n));mean(Dth5(10:n))];
68 Eheat = [0;mean(E1(10:n));mean(E2(10:n));mean(E3(10:n));mean(E4(10:n)); ...
69 mean(E5(10:n))];
70
71 f = fittype('poly1'); % Fitting both heat and strain to linear slopes
72 ffit = fit(Aflue,heat,f);
73 ffit2 = fit(Aflue,strain,f);
74
75 % Plot peak, heat strain
76 figure(12); clf; hold on;
77 errorbar(Aflue,strain,Estrain, 'k*');
78 errorbar(Aflue,heat,Eheat, 'bo');
79 plot(ffit);
80 plot(ffit2);
81 xlabel('Absorbed Fluence (mJ/cm^2)');
82 ylabel('Peak shifts (mdeg)');
83 title('InSb');
84 legend('Peak Strain','Long-time Heating','Location','NorthWest')
85 ylim([0 2.2]); hold off
86 xlim([0 1.4]);

```

```

87
88 t = toc;      % Stop the clock

```

C.2.4 Extract Centroid Shifts for Each Fluence for InSb

```

1 %% chomplite_InSb.m
2 % Written by G. Jackson Williams 9/1/2009
3 % This is a subroutine to a program takes a modified .mda file from any
4 % time resolved diffraction data and outputs peak shift vs time.
5
6 function [Dth,time,p,Etot] = chomplite_InSb(p,m,n)
7
8 a = load('-ascii','7idc_0040.txt');      % Load InSb data
9 A = p + 1:p + m;                        % Initialize indexing parameter
10
11 [lsroff1,lsron1,Eoff1,Eon1] = deadtime(a);
12
13 centeroff = zeros(1,n);      % Preallocate space for these arrays
14 Ecentoff = zeros(1,n);
15 centeron = zeros(1,n);
16 Ecenton = zeros(1,n);
17
18 for i = 1:n;                  % For a total of "n" time steps
19     if(i == 1)                % For each time step, the angle index is updated
20         A = p + 1:p + m;
21     else
22         A = max(A)+1:max(A)+m;
23     end
24     % Detector data for each rocking curve scan:
25     lsroff = lsroff1(A);      % APD Data from Laser Off bucket
26     lsron = lsron1(A);        % APD Data from Laser On bucket
27     Eoff = Eoff1(A);          % Counting statistics for off bucket
28     Eon = Eon1(A);            % Counting statistics for off bucket
29
30     apdon = a(A,15);          % Normalization APD Data for Laser On bucket
31     apdtot = a(A,14);         % Normalization APD Data for Laser Off bucket
32     angle = a(A,2);           % Angle Positioner
33
34     normon = lsroff.*apdtot./(48*apdon);      % Normalize to upstream APD
35     normoff = lsron.*apdtot./(48*apdon);      % To remove top-ups
36
37     [outon] = gaussfit(angle,normon,Eon);     % Fit rocking curves to gaussian
38     [outoff] = gaussfit(angle,normoff,Eoff);
39
40     centeroff(:,i) = outoff(1);               % Extract Centroid
41     Ecentoff(:,i) = outoff(2);               % and error in fit due to counting
42                                           % statistics and fit residuals
43     centeron(:,i) = outon(1);                % for both lsr on and lsr off

```

```

44     Ecenton(:,i) = outon(2);
45
46 end
47
48 Dth = (centeroff - centeron)*1000; % Taking the peak shift, in mdeg
49
50 dtime = .1; % Each time step is 100 ps
51 time = dtime*(0:i-1); % Start at t = 0
52 p = max(A); % keep file index to start at next 2-D scan
53 Etot = (Ecentoff+Ecenton)*1000; % Error in the peak shift, in mdeg
54 end
55
56 % Detector Definitions
57 % Column 8 Det 6 Lsr Rep Rate
58 % Column 9 Det 7 APD_B.tot NO
59 % Column 10 Det 8 APD_B.off YES lsroff
60 % Column 11 Det 9 APD_B.on YES lsron
61 % Column 12 Det 10 APD_B.off.late NO
62 % Column 13 Det 11 APD_B.on.late YES lsrlate
63 % Column 14 Det 12 APD_A.tot (normalization)
64 % Column 15 Det 13 APD_A.on (gated every bunch with P0 at 271 kHz)
65 % Column 16 Det 14 APD_A.late (gated every bunch with P0 at 271 kHz)

```

C.2.5 Deadtime Correction Subroutine

```

1 %% Program to correct for the deadtime of photon counting APDs
2 % Written by G. Jackson Williams
3 % circa 9/1/2009
4
5 function [lsroff1,lsron1,Eoff,Eon] = deadtime(a)
6     t = 1; % Counting time
7     T = 1./a(:,8); % Repitition Rate of the laser
8     lsroff = a(:,10); % N_O (observed count rate)
9     lsron = a(:,11); % N_O (observed count rate)
10    tau = 1./a(:,8); % Repetition rate of the laser
11 % Return corrected (true) count rate for entire data set-(fluence and angle)
12    lsroff1 = -(1./tau).*log(1 - lsroff.*tau);
13    lsron1 = -(1./tau).*log(1 - lsron.*tau);
14 % Return deadtime correction counting statistics
15    Eoff = 1./((1-T.*lsroff)).*sqrt(lsroff./t);
16    Eon = 1./((1-T.*lsron)).*sqrt(lsron./t);
17 end

```

C.3 Dispersion Correction Terms $\Delta f'$ and $\Delta f''$

Data taken from [19] or available on the web at
http://henke.lbl.gov/optical_constants/asf.html

C.3.1 Indium

1	%	Energy (eV)	f'	f''
2		1000.000	-9.620117	20.60602
3		1100.000	-8.054237	18.47271
4		1200.000	-7.008023	16.63640
5		1300.000	-6.270947	15.05404
6		1400.000	-5.770803	13.68025
7		1500.000	-5.439097	12.48567
8		1600.000	-5.212864	11.43919
9		1700.000	-5.076109	10.51707
10		1800.000	-5.081061	9.703634
11		1900.000	-5.118416	8.995317
12		2000.000	-5.143920	8.362679
13		2100.000	-5.204079	7.794830
14		2200.000	-5.294268	7.282991
15		2300.000	-5.415628	6.819891
16		2400.000	-5.558311	6.399615
17		2500.000	-5.725870	6.016752
18		2600.000	-5.918964	5.666907
19		2700.000	-6.180744	5.348144
20		2800.000	-6.431940	5.057722
21		2900.000	-6.747009	4.792847
22		3000.000	-7.077412	4.548751
23		3100.000	-7.458972	4.326771
24		3200.000	-7.910831	4.121375
25		3300.000	-8.461382	3.930896
26		3400.000	-9.162023	3.753936
27		3500.000	-10.11621	3.589182
28		3600.000	-11.60928	3.435501
29		3633.000	-12.36531	3.387042
30		3638.000	-12.50117	3.379793
31		3643.000	-12.64437	3.372568
32		3648.000	-12.79578	3.365368
33		3653.000	-12.95641	3.358191
34		3658.000	-13.12748	3.351039
35		3663.000	-13.31050	3.343911
36		3668.000	-13.50729	3.336806
37		3673.000	-13.72018	3.329725
38		3678.000	-13.95207	3.322668
39		3683.000	-14.20684	3.315634
40		3688.000	-14.48958	3.308623
41		3693.000	-14.80739	3.301635

42	3698.000	-15.17043	3.294671
43	3700.000	-15.33152	3.291891
44	3703.000	-15.59412	3.287729
45	3708.000	-16.10328	3.280810
46	3713.000	-16.74225	3.273914
47	3718.000	-17.60205	3.267041
48	3723.000	-18.92500	3.260190
49	3728.000	-21.94412	3.253362
50	3733.000	-21.15192	11.04794
51	3738.000	-18.65468	11.01754
52	3743.000	-17.43659	10.98730
53	3748.000	-16.62749	10.95725
54	3753.000	-16.02358	10.92737
55	3758.000	-15.54389	10.89766
56	3763.000	-15.14781	10.86812
57	3768.000	-14.81213	10.83876
58	3773.000	-14.52228	10.80956
59	3778.000	-14.26855	10.78053
60	3783.000	-14.04416	10.75166
61	3788.000	-13.84414	10.72296
62	3793.000	-13.66484	10.69443
63	3798.000	-13.50342	10.66606
64	3800.000	-13.44335	10.65475
65	3803.000	-13.35770	10.63785
66	3808.000	-13.22596	10.60979
67	3813.000	-13.10684	10.58190
68	3818.000	-12.99924	10.55417
69	3823.000	-12.90230	10.52659
70	3828.000	-12.81532	10.49917
71	3841.000	-12.63241	10.42859
72	3846.000	-12.57788	10.40172
73	3851.000	-12.53192	10.37499
74	3856.000	-12.49459	10.34842
75	3861.000	-12.46603	10.32199
76	3866.000	-12.44654	10.29572
77	3871.000	-12.43659	10.26958
78	3876.000	-12.43685	10.24360
79	3881.000	-12.44824	10.21775
80	3886.000	-12.47201	10.19205
81	3891.000	-12.50989	10.16649
82	3896.000	-12.56427	10.14108
83	3900.000	-12.62188	10.12084
84	3901.000	-12.63853	10.11580
85	3906.000	-12.73760	10.09066
86	3911.000	-12.86905	10.06565
87	3916.000	-13.04523	10.04079
88	3921.000	-13.28822	10.01606
89	3926.000	-13.64383	9.991458
90	3931.000	-14.23485	9.966997
91	3936.000	-15.70340	9.942667
92	3941.000	-15.14090	13.78414
93	3946.000	-13.86299	13.74954
94	3951.000	-13.19963	13.71513
95	3956.000	-12.73658	13.68091

96	3961.000	-12.37510	13.64688
97	3966.000	-12.07558	13.61304
98	3971.000	-11.81815	13.57939
99	3976.000	-11.59133	13.54593
100	3981.000	-11.38792	13.51265
101	3986.000	-11.20307	13.47956
102	3991.000	-11.03338	13.44664
103	3996.000	-10.87636	13.41391
104	4000.000	-10.75858	13.38786
105	4001.000	-10.73012	13.38136
106	4006.000	-10.59320	13.34899
107	4011.000	-10.46446	13.31679
108	4016.000	-10.34299	13.28478
109	4021.000	-10.22800	13.25293
110	4026.000	-10.11888	13.22126
111	4031.000	-10.01512	13.18976
112	4036.000	-9.916277	13.15844
113	4100.000	-8.972916	12.77208
114	4140.000	-8.616801	12.54372
115	4145.000	-8.584288	12.51585
116	4150.000	-8.554716	12.48812
117	4155.000	-8.528238	12.46054
118	4160.000	-8.505053	12.43311
119	4165.000	-8.485400	12.40582
120	4170.000	-8.469594	12.37867
121	4175.000	-8.458027	12.35166
122	4180.000	-8.451204	12.32480
123	4185.000	-8.449775	12.29807
124	4190.000	-8.454600	12.27148
125	4195.000	-8.466843	12.24503
126	4200.000	-8.488109	12.21872
127	4205.000	-8.520723	12.19254
128	4210.000	-8.568189	12.16650
129	4215.000	-8.636155	12.14060
130	4220.000	-8.734588	12.11483
131	4225.000	-8.883768	12.08919
132	4230.000	-9.136117	12.06368
133	4235.000	-9.734893	12.03830
134	4240.000	-9.689471	13.86571
135	4245.000	-8.994583	13.83905
136	4250.000	-8.647552	13.81252
137	4255.000	-8.404243	13.78612
138	4260.000	-8.211948	13.75986
139	4265.000	-8.050273	13.73372
140	4270.000	-7.909103	13.70771
141	4275.000	-7.782726	13.68183
142	4280.000	-7.667568	13.65607
143	4285.000	-7.561257	13.63045
144	4290.000	-7.462104	13.60494
145	4295.000	-7.368905	13.57957
146	4300.000	-7.280745	13.55431
147	4305.000	-7.196927	13.52918
148	4310.000	-7.116878	13.50417
149	4315.000	-7.040160	13.47928

150	4320.000	−6.966408	13.45452
151	4325.000	−6.895326	13.42987
152	4330.000	−6.826648	13.40534
153	4335.000	−6.760167	13.38093
154	4400.000	−6.036684	13.07408
155	4500.000	−5.216025	12.63747
156	4600.000	−4.586904	12.23960
157	4700.000	−4.076517	11.87628
158	4800.000	−3.648225	11.54393
159	4900.000	−3.051923	11.21557
160	5000.000	−2.716684	10.88601
161	5100.000	−2.423279	10.57544
162	5200.000	−2.053329	10.26510
163	5300.000	−1.817399	9.965174
164	5400.000	−1.608070	9.678737
165	5500.000	−1.421609	9.404993
166	5600.000	−1.242030	9.141077
167	5700.000	−1.091969	8.887983
168	5800.000	−0.9573733	8.645290
169	5900.000	−0.8364584	8.412432
170	6000.000	−0.7276968	8.188873
171	6100.000	−0.6297747	7.974123
172	6200.000	−0.5415545	7.767715
173	6300.000	−0.4620449	7.569220
174	6400.000	−0.3903795	7.378234
175	6500.000	−0.3257951	7.194379
176	6600.000	−0.2676182	7.017301
177	6700.000	−0.2152517	6.846665
178	6800.000	−0.1681646	6.682161
179	6900.000	−0.1258835	6.523497
180	7000.000	−8.7984264E−02	6.370395
181	7100.000	−5.4086655E−02	6.222597
182	7200.000	−2.3848634E−02	6.079858
183	7300.000	3.0379370E−03	5.941947
184	7400.000	2.5742525E−02	5.808653
185	7500.000	3.9831575E−02	5.679974
186	7600.000	5.8204472E−02	5.555813
187	7700.000	7.4223846E−02	5.435678
188	7800.000	8.8077143E−02	5.319394
189	7900.000	9.5412686E−02	5.206873
190	8000.000	0.1053914	5.098123
191	8100.000	0.1136909	4.992754
192	8200.000	0.1204404	4.890626
193	8300.000	0.1257550	4.791605
194	8400.000	0.1289506	4.695578
195	8500.000	0.1261521	4.602493
196	8600.000	0.1277380	4.512395
197	8700.000	0.1282909	4.424940
198	8800.000	0.1278871	4.340022
199	8900.000	0.1265974	4.257545
200	9000.000	0.1245486	4.177756
201	9100.000	0.1217746	4.100235
202	9200.000	0.1183310	4.024898
203	9300.000	0.1142692	3.951659

204	9400.000	0.1096367	3.880442
205	9500.000	0.1044773	3.811170
206	9600.000	9.8831564E-02	3.743773
207	9700.000	9.2737019E-02	3.678183
208	9800.000	8.6228229E-02	3.614334
209	9900.000	7.9337433E-02	3.552165
210	10000.00	7.2094239E-02	3.491616
211	10100.00	6.4526290E-02	3.432629
212	10200.00	5.6659203E-02	3.375152
213	10300.00	4.8516531E-02	3.319132
214	10400.00	4.0120408E-02	3.264520
215	10500.00	3.1491078E-02	3.211268
216	10600.00	2.2647552E-02	3.159331
217	10700.00	1.3607492E-02	3.108665
218	10800.00	4.3870425E-03	3.059227
219	10900.00	-4.9984660E-03	3.010980
220	11000.00	-1.4535142E-02	2.963883
221	11100.00	-2.4209827E-02	2.917900
222	11200.00	-3.4010295E-02	2.872996
223	11300.00	-4.3925460E-02	2.829136
224	11400.00	-5.3944673E-02	2.786288
225	11500.00	-6.4058408E-02	2.744421
226	11600.00	-7.4257568E-02	2.703504
227	11700.00	-8.4533669E-02	2.663510
228	11800.00	-9.4879173E-02	2.624408
229	11900.00	-0.1052867	2.586174
230	12000.00	-0.1157497	2.548781
231	12100.00	-0.1262621	2.512203
232	12200.00	-0.1368179	2.476419
233	12300.00	-0.1474122	2.441403
234	12400.00	-0.1580406	2.407135
235	12500.00	-0.1701095	2.373597
236	12600.00	-0.1808073	2.340777
237	12700.00	-0.1915212	2.308642
238	12800.00	-0.2022513	2.277173
239	12900.00	-0.2129946	2.246352
240	13000.00	-0.2237483	2.216160
241	13100.00	-0.2345093	2.186581
242	13200.00	-0.2463433	2.157599
243	13300.00	-0.2571144	2.129208
244	13400.00	-0.2678905	2.101380
245	13500.00	-0.2786658	2.074101
246	13600.00	-0.2894384	2.047357
247	13700.00	-0.3002066	2.021133
248	13800.00	-0.3109696	1.995416
249	13900.00	-0.3217258	1.970193
250	14000.00	-0.3324746	1.945451
251	14100.00	-0.3432152	1.921177
252	14200.00	-0.3539466	1.897360
253	14300.00	-0.3646685	1.873988
254	14400.00	-0.3753802	1.851050
255	14500.00	-0.3860818	1.828535
256	14600.00	-0.3967727	1.806433
257	14700.00	-0.4074528	1.784734

258	14800.00	−0.4181222	1.763427
259	14900.00	−0.4287809	1.742503
260	15000.00	−0.4394290	1.721953
261	15100.00	−0.4500668	1.701768
262	15200.00	−0.4606945	1.681939
263	15300.00	−0.4713125	1.662459
264	15400.00	−0.4819210	1.643317
265	15500.00	−0.4925076	1.624508
266	15600.00	−0.5033034	1.606024
267	15700.00	−0.5138884	1.587856
268	15800.00	−0.5244666	1.569998
269	15900.00	−0.5350385	1.552442
270	16000.00	−0.5456047	1.535181
271	16100.00	−0.5561627	1.518209
272	16200.00	−0.5685115	1.501531
273	16300.00	−0.5790550	1.485150
274	16400.00	−0.5896059	1.469038
275	16500.00	−0.6001569	1.453189
276	16600.00	−0.6107085	1.437597
277	16700.00	−0.6212618	1.422258
278	16800.00	−0.6318178	1.407165
279	16900.00	−0.6423778	1.392314
280	17000.00	−0.6529418	1.377698
281	17100.00	−0.6650278	1.363322
282	17200.00	−0.6756017	1.349190
283	17300.00	−0.6861889	1.335278
284	17400.00	−0.6967878	1.321583
285	17500.00	−0.7073996	1.308100
286	17600.00	−0.7180257	1.294823
287	17700.00	−0.7286680	1.281750
288	17800.00	−0.7393280	1.268876
289	17900.00	−0.7500080	1.256197
290	18000.00	−0.7607096	1.243708
291	18100.00	−0.7714351	1.231406
292	18200.00	−0.7821867	1.219288
293	18300.00	−0.7929702	1.207349
294	18400.00	−0.8060690	1.195600
295	18500.00	−0.8169246	1.184048
296	18600.00	−0.8278037	1.172664
297	18700.00	−0.8387176	1.161446
298	18800.00	−0.8496690	1.150391
299	18900.00	−0.8606611	1.139494
300	19000.00	−0.8716962	1.128754
301	19100.00	−0.8827770	1.118167
302	19200.00	−0.8939061	1.107730
303	19300.00	−0.9050862	1.097440
304	19400.00	−0.9163203	1.087294
305	19500.00	−0.9276114	1.077291
306	19600.00	−0.9389625	1.067426
307	19700.00	−0.9503766	1.057698
308	19800.00	−0.9618567	1.048104
309	19900.00	−0.9734068	1.038642
310	20000.00	−0.9850299	1.029308
311	20100.00	−0.9967297	1.020101

312	20200.00	-1.008510	1.011019
313	20300.00	-1.020374	1.002059
314	20400.00	-1.032327	0.9932181
315	20500.00	-1.044371	0.9844953
316	20600.00	-1.056513	0.9758883
317	20700.00	-1.068755	0.9673947
318	20800.00	-1.081103	0.9590129
319	20900.00	-1.093562	0.9507405
320	21000.00	-1.106136	0.9425758
321	21100.00	-1.118830	0.9345169
322	21200.00	-1.131651	0.9265619
323	21300.00	-1.144603	0.9187092
324	21400.00	-1.157693	0.9109567
325	21500.00	-1.170927	0.9033028
326	21600.00	-1.184310	0.8957459
327	21700.00	-1.197851	0.8882844
328	21800.00	-1.211556	0.8809167
329	21900.00	-1.225432	0.8736409
330	22000.00	-1.239488	0.8664557
331	22100.00	-1.253731	0.8593596
332	22200.00	-1.268169	0.8523510
333	22300.00	-1.282812	0.8454286
334	22400.00	-1.297670	0.8385908
335	22500.00	-1.312753	0.8318363
336	22600.00	-1.328070	0.8251638
337	22700.00	-1.343634	0.8185719
338	22800.00	-1.359455	0.8120593
339	22900.00	-1.375547	0.8056247
340	23000.00	-1.391922	0.7992668
341	23100.00	-1.408595	0.7929844
342	23200.00	-1.425581	0.7867764
343	23300.00	-1.442896	0.7806416
344	23400.00	-1.460556	0.7745786
345	23500.00	-1.478580	0.7685865
346	23600.00	-1.496987	0.7626642
347	23700.00	-1.515797	0.7568104
348	23800.00	-1.535034	0.7510244
349	23900.00	-1.554720	0.7453048
350	24000.00	-1.574883	0.7396507
351	24100.00	-1.595548	0.7340611
352	24200.00	-1.616747	0.7285349
353	24300.00	-1.638511	0.7230715
354	24400.00	-1.660876	0.7176694
355	24500.00	-1.683881	0.7123281
356	24600.00	-1.707566	0.7070464
357	24700.00	-1.731978	0.7018237
358	24800.00	-1.757165	0.6966589
359	24900.00	-1.783184	0.6915511

C.3.2 Antimony

1	%	Energy (eV)	f'	f''
2		1000.000	-11.80711	24.04015
3		1100.000	-9.505189	21.63727
4		1200.000	-7.983030	19.55356
5		1300.000	-6.937045	17.73706
6		1400.000	-6.199494	16.15649
7		1500.000	-5.661477	14.77380
8		1600.000	-5.315005	13.55524
9		1700.000	-5.055348	12.48680
10		1800.000	-4.883482	11.53821
11		1900.000	-4.797727	10.69303
12		2000.000	-4.748501	9.936948
13		2100.000	-4.742525	9.257375
14		2200.000	-4.890482	8.655450
15		2300.000	-4.945248	8.113972
16		2400.000	-5.024939	7.621761
17		2500.000	-5.127174	7.172884
18		2600.000	-5.250607	6.762289
19		2700.000	-5.394918	6.385658
20		2800.000	-5.561098	6.039280
21		2900.000	-5.757222	5.720049
22		3000.000	-5.994437	5.425198
23		3100.000	-6.222447	5.161564
24		3200.000	-6.477096	4.917472
25		3300.000	-6.765496	4.691054
26		3400.000	-7.091969	4.480657
27		3500.000	-7.468798	4.284714
28		3600.000	-7.912734	4.101889
29		3700.000	-8.450916	3.930999
30		3800.000	-9.132996	3.771023
31		3900.000	-10.05588	3.621086
32		4000.000	-11.49109	3.480281
33		4035.000	-12.26530	3.433017
34		4040.000	-12.39764	3.426346
35		4045.000	-12.53718	3.419696
36		4050.000	-12.68478	3.413067
37		4055.000	-12.84142	3.406457
38		4060.000	-13.00835	3.399868
39		4065.000	-13.18703	3.393298
40		4070.000	-13.37927	3.386748
41		4075.000	-13.58734	3.380218
42		4080.000	-13.81419	3.373708
43		4085.000	-14.06357	3.367217
44		4090.000	-14.34055	3.360745
45		4095.000	-14.65212	3.354294
46		4100.000	-15.00836	3.347861
47		4105.000	-15.42443	3.341448
48		4110.000	-15.92482	3.335053
49		4115.000	-16.55297	3.328679

50	4120.000	-17.39820	3.322323
51	4125.000	-18.69591	3.315986
52	4130.000	-21.61562	3.309667
53	4135.000	-21.02710	11.06989
54	4140.000	-18.47883	11.03836
55	4145.000	-17.24737	11.00703
56	4150.000	-16.42999	10.97591
57	4155.000	-15.81923	10.94498
58	4160.000	-15.33313	10.91426
59	4165.000	-14.93064	10.88373
60	4170.000	-14.58841	10.85339
61	4175.000	-14.29177	10.82325
62	4180.000	-14.03097	10.79331
63	4185.000	-13.79909	10.76355
64	4190.000	-13.59117	10.73398
65	4195.000	-13.40348	10.70459
66	4200.000	-13.23316	10.67540
67	4205.000	-13.07793	10.64639
68	4210.000	-12.93603	10.61755
69	4215.000	-12.80599	10.58891
70	4220.000	-12.68668	10.56044
71	4225.000	-12.57708	10.53215
72	4230.000	-12.47643	10.50404
73	4283.000	-11.84502	10.21658
74	4288.000	-11.82186	10.19042
75	4293.000	-11.80506	10.16443
76	4298.000	-11.79486	10.13859
77	4300.000	-11.79271	10.12830
78	4303.000	-11.79162	10.11291
79	4308.000	-11.79578	10.08739
80	4313.000	-11.80796	10.06202
81	4318.000	-11.82891	10.03681
82	4323.000	-11.85965	10.01175
83	4328.000	-11.90151	9.986842
84	4333.000	-11.95625	9.962086
85	4338.000	-12.02622	9.937481
86	4343.000	-12.11484	9.913022
87	4348.000	-12.22689	9.888711
88	4353.000	-12.36969	9.864546
89	4358.000	-12.55505	9.840529
90	4363.000	-12.80395	9.816654
91	4368.000	-13.15910	9.792922
92	4373.000	-13.73182	9.769332
93	4378.000	-15.04990	9.745885
94	4383.000	-14.90222	13.57064
95	4388.000	-13.52772	13.53626
96	4393.000	-12.85290	13.50208
97	4398.000	-12.39108	13.46813
98	4400.000	-12.23893	13.45460
99	4403.000	-12.03474	13.43438
100	4408.000	-11.74198	13.40083
101	4413.000	-11.49199	13.36750
102	4418.000	-11.27291	13.33437
103	4423.000	-11.07733	13.30145

104	4428.000	-10.90027	13.26872
105	4433.000	-10.73827	13.23620
106	4438.000	-10.58879	13.20388
107	4443.000	-10.44995	13.17176
108	4448.000	-10.32025	13.13983
109	4453.000	-10.19854	13.10810
110	4458.000	-10.08389	13.07656
111	4463.000	-9.975549	13.04522
112	4468.000	-9.872877	13.01406
113	4473.000	-9.775362	12.98309
114	4478.000	-9.682563	12.95232
115	4500.000	-9.321861	12.81909
116	4600.000	-8.350879	12.25607
117	4601.000	-8.345910	12.25077
118	4606.000	-8.322629	12.22437
119	4611.000	-8.302059	12.19813
120	4616.000	-8.284369	12.17204
121	4621.000	-8.269765	12.14611
122	4626.000	-8.258502	12.12033
123	4631.000	-8.250902	12.09470
124	4636.000	-8.247368	12.06922
125	4641.000	-8.248412	12.04389
126	4646.000	-8.254697	12.01871
127	4651.000	-8.267096	11.99367
128	4656.000	-8.286781	11.96878
129	4661.000	-8.315382	11.94404
130	4666.000	-8.355250	11.91944
131	4671.000	-8.409937	11.89498
132	4676.000	-8.485182	11.87067
133	4681.000	-8.591166	11.84650
134	4686.000	-8.748684	11.82247
135	4691.000	-9.012354	11.79857
136	4696.000	-9.646976	11.77482
137	4700.000	-9.793721	13.59795
138	4701.000	-9.514109	13.59295
139	4706.000	-8.859342	13.56806
140	4711.000	-8.526525	13.54332
141	4716.000	-8.293218	13.51871
142	4721.000	-8.109350	13.49423
143	4726.000	-7.955288	13.46990
144	4731.000	-7.821229	13.44569
145	4736.000	-7.701613	13.42163
146	4741.000	-7.592951	13.39769
147	4746.000	-7.492924	13.37389
148	4751.000	-7.399879	13.35022
149	4756.000	-7.312633	13.32668
150	4761.000	-7.230290	13.30327
151	4766.000	-7.152167	13.27999
152	4771.000	-7.077701	13.25684
153	4776.000	-7.006462	13.23381
154	4781.000	-6.938091	13.21092
155	4786.000	-6.872299	13.18815
156	4791.000	-6.808825	13.16550
157	4796.000	-6.747465	13.14297

158	4800.000	-6.699776	13.12504
159	4900.000	-5.765469	12.70139
160	5000.000	-5.102882	12.32126
161	5100.000	-4.583796	11.97982
162	5200.000	-4.157225	11.67296
163	5300.000	-3.795290	11.39715
164	5400.000	-3.122936	11.13059
165	5500.000	-2.821460	10.83750
166	5600.000	-2.555288	10.56187
167	5700.000	-2.147382	10.30077
168	5800.000	-1.922743	10.02468
169	5900.000	-1.721841	9.759982
170	6000.000	-1.541518	9.506063
171	6100.000	-1.379160	9.262341
172	6200.000	-1.220096	9.026402
173	6300.000	-1.086831	8.799265
174	6400.000	-0.9661846	8.580628
175	6500.000	-0.8568169	8.370067
176	6600.000	-0.7575686	8.167182
177	6700.000	-0.6674300	7.971601
178	6800.000	-0.5855171	7.782971
179	6900.000	-0.5110527	7.600965
180	7000.000	-0.4433494	7.425272
181	7100.000	-0.3817973	7.255600
182	7200.000	-0.3258536	7.091674
183	7300.000	-0.2750331	6.933233
184	7400.000	-0.2289017	6.780035
185	7500.000	-0.1870687	6.631847
186	7600.000	-0.1491827	6.488451
187	7700.000	-0.1149265	6.349641
188	7800.000	-8.4013142E-02	6.215221
189	7900.000	-5.6183465E-02	6.085007
190	8000.000	-3.1202115E-02	5.958823
191	8100.000	-8.8558793E-03	5.836503
192	8200.000	1.1047892E-02	5.717890
193	8300.000	2.2593230E-02	5.602978
194	8400.000	3.8073659E-02	5.491742
195	8500.000	5.1603872E-02	5.383783
196	8600.000	6.3303068E-02	5.278973
197	8700.000	7.3269002E-02	5.177189
198	8800.000	7.7152573E-02	5.078423
199	8900.000	8.3780266E-02	4.982624
200	9000.000	8.9963034E-02	4.890071
201	9100.000	9.4975851E-02	4.800124
202	9200.000	9.8902687E-02	4.712685
203	9300.000	0.1018212	4.627656
204	9400.000	0.1034972	4.544953
205	9500.000	0.1045515	4.464508
206	9600.000	0.1047990	4.386224
207	9700.000	0.1042965	4.310025
208	9800.000	0.1030971	4.235836
209	9900.000	0.1012531	4.163585
210	10000.00	9.8678328E-02	4.093205
211	10100.00	9.5506266E-02	4.024632

212	10200.00	9.1962896E-02	3.957804
213	10300.00	8.7934487E-02	3.892659
214	10400.00	8.3456486E-02	3.829142
215	10500.00	7.8560412E-02	3.767197
216	10600.00	7.3275670E-02	3.706771
217	10700.00	6.7629695E-02	3.647815
218	10800.00	6.1647858E-02	3.590281
219	10900.00	5.5354048E-02	3.534122
220	11000.00	4.8770312E-02	3.479294
221	11100.00	4.1917399E-02	3.425756
222	11200.00	3.4814678E-02	3.373466
223	11300.00	2.7480043E-02	3.322384
224	11400.00	1.9930463E-02	3.272475
225	11500.00	1.2181519E-02	3.223700
226	11600.00	4.2479681E-03	3.176027
227	11700.00	-3.8563842E-03	3.129421
228	11800.00	-1.2118864E-02	3.083849
229	11900.00	-2.0527324E-02	3.039283
230	12000.00	-2.9070716E-02	2.995691
231	12100.00	-3.7738487E-02	2.953044
232	12200.00	-4.6520751E-02	2.911317
233	12300.00	-5.5408530E-02	2.870480
234	12400.00	-6.4393088E-02	2.830511
235	12500.00	-7.3466599E-02	2.791382
236	12600.00	-8.2621500E-02	2.753071
237	12700.00	-9.1850720E-02	2.715556
238	12800.00	-0.1011479	2.678812
239	12900.00	-0.1105068	2.642820
240	13000.00	-0.1199219	2.607559
241	13100.00	-0.1293878	2.573008
242	13200.00	-0.1388994	2.539149
243	13300.00	-0.1484523	2.505962
244	13400.00	-0.1580421	2.473431
245	13500.00	-0.1676648	2.441537
246	13600.00	-0.1773168	2.410263
247	13700.00	-0.1869944	2.379595
248	13800.00	-0.1966945	2.349515
249	13900.00	-0.2064141	2.320009
250	14000.00	-0.2161506	2.291061
251	14100.00	-0.2259012	2.262659
252	14200.00	-0.2356635	2.234788
253	14300.00	-0.2456708	2.207434
254	14400.00	-0.2572366	2.180591
255	14500.00	-0.2670264	2.154254
256	14600.00	-0.2768171	2.128397
257	14700.00	-0.2866097	2.103008
258	14800.00	-0.2964028	2.078076
259	14900.00	-0.3061953	2.053590
260	15000.00	-0.3159861	2.029539
261	15100.00	-0.3257742	2.005913
262	15200.00	-0.3355593	1.982702
263	15300.00	-0.3466452	1.959902
264	15400.00	-0.3564211	1.937504
265	15500.00	-0.3661904	1.915492

266	15600.00	-0.3759529	1.893857
267	15700.00	-0.3857084	1.872590
268	15800.00	-0.3954565	1.851684
269	15900.00	-0.4051970	1.831129
270	16000.00	-0.4149298	1.810918
271	16100.00	-0.4246547	1.791044
272	16200.00	-0.4343716	1.771498
273	16300.00	-0.4440804	1.752273
274	16400.00	-0.4537815	1.733363
275	16500.00	-0.4634750	1.714760
276	16600.00	-0.4731609	1.696458
277	16700.00	-0.4828395	1.678449
278	16800.00	-0.4925109	1.660729
279	16900.00	-0.5021759	1.643290
280	17000.00	-0.5118346	1.626127
281	17100.00	-0.5214876	1.609234
282	17200.00	-0.5311353	1.592604
283	17300.00	-0.5407780	1.576234
284	17400.00	-0.5504167	1.560116
285	17500.00	-0.5600520	1.544246
286	17600.00	-0.5696844	1.528619
287	17700.00	-0.5793166	1.513229
288	17800.00	-0.5891474	1.498075
289	17900.00	-0.5988278	1.483148
290	18000.00	-0.6104063	1.468477
291	18100.00	-0.6200312	1.454026
292	18200.00	-0.6296562	1.439790
293	18300.00	-0.6392828	1.425764
294	18400.00	-0.6489127	1.411943
295	18500.00	-0.6585468	1.398324
296	18600.00	-0.6681861	1.384903
297	18700.00	-0.6778318	1.371676
298	18800.00	-0.6874846	1.358639
299	18900.00	-0.6971462	1.345788
300	19000.00	-0.7083941	1.333125
301	19100.00	-0.7180721	1.320661
302	19200.00	-0.7277620	1.308373
303	19300.00	-0.7374650	1.296258
304	19400.00	-0.7471827	1.284311
305	19500.00	-0.7569164	1.272531
306	19600.00	-0.7666674	1.260913
307	19700.00	-0.7764372	1.249454
308	19800.00	-0.7862270	1.238153
309	19900.00	-0.7960388	1.227006
310	20000.00	-0.8058740	1.216009
311	20100.00	-0.8157342	1.205161
312	20200.00	-0.8256211	1.194458
313	20300.00	-0.8355370	1.183899
314	20400.00	-0.8478423	1.173494
315	20500.00	-0.8578241	1.163248
316	20600.00	-0.8678378	1.153137
317	20700.00	-0.8778864	1.143159
318	20800.00	-0.8879718	1.133312
319	20900.00	-0.8980965	1.123593

320	21000.00	-0.9082623	1.114000
321	21100.00	-0.9184713	1.104530
322	21200.00	-0.9287258	1.095182
323	21300.00	-0.9390277	1.085954
324	21400.00	-0.9493799	1.076844
325	21500.00	-0.9597845	1.067848
326	21600.00	-0.9702440	1.058967
327	21700.00	-0.9807608	1.050196
328	21800.00	-0.9913374	1.041536
329	21900.00	-1.001977	1.032983
330	22000.00	-1.012682	1.024537
331	22100.00	-1.023455	1.016194
332	22200.00	-1.034300	1.007954
333	22300.00	-1.045219	0.9998155
334	22400.00	-1.056216	0.9917758
335	22500.00	-1.067293	0.9838335
336	22600.00	-1.078455	0.9759872
337	22700.00	-1.089705	0.9682353
338	22800.00	-1.101046	0.9605765
339	22900.00	-1.112482	0.9530089
340	23000.00	-1.124018	0.9455312
341	23100.00	-1.135657	0.9381419
342	23200.00	-1.147403	0.9308398
343	23300.00	-1.159261	0.9236235
344	23400.00	-1.171236	0.9164914
345	23500.00	-1.183332	0.9094423
346	23600.00	-1.195555	0.9024749
347	23700.00	-1.207909	0.8955880
348	23800.00	-1.220399	0.8887804
349	23900.00	-1.233033	0.8820506
350	24000.00	-1.245815	0.8753976
351	24100.00	-1.258751	0.8688202
352	24200.00	-1.271849	0.8623172
353	24300.00	-1.285115	0.8558877
354	24400.00	-1.298555	0.8495302
355	24500.00	-1.312179	0.8432438
356	24600.00	-1.325992	0.8370275
357	24700.00	-1.340004	0.8308802
358	24800.00	-1.354224	0.8248008
359	24900.00	-1.368660	0.8187884

C.3.3 Gallium

1	%	Energy (eV)	f'	f''
2		1000.000	-12.78024	2.622440
3		1100.000	-23.67351	2.312109
4		1200.000	-2.682566	11.65662
5		1205.000	-3.065672	10.81520
6		1210.000	-3.465937	10.08000
7		1215.000	-3.875939	9.435927
8		1220.000	-4.290639	8.870313
9		1225.000	-4.706735	8.372511
10		1230.000	-5.122201	7.933538
11		1235.000	-5.535975	7.545800
12		1240.000	-5.947742	7.202854
13		1245.000	-6.357804	6.899230
14		1250.000	-6.766998	6.630270
15		1255.000	-7.176702	6.392002
16		1260.000	-7.588907	6.181035
17		1265.000	-8.006413	5.994472
18		1270.000	-8.433251	5.829834
19		1275.000	-8.875569	5.685009
20		1280.000	-9.343676	5.558189
21		1285.000	-9.857612	5.447840
22		1290.000	-10.46733	5.352658
23		1295.000	-11.39250	5.271546
24		1300.000	-11.80414	7.023297
25		1305.000	-11.45599	6.967597
26		1310.000	-11.47662	6.923607
27		1315.000	-11.60475	6.890850
28		1320.000	-11.78719	6.868974
29		1325.000	-12.00424	6.857738
30		1330.000	-12.24675	6.857008
31		1335.000	-12.51003	6.866754
32		1340.000	-12.79155	6.887047
33		1345.000	-13.09006	6.918058
34		1350.000	-13.40507	6.960057
35		1355.000	-13.73658	7.013420
36		1360.000	-14.08498	7.078628
37		1365.000	-14.45092	7.156275
38		1370.000	-14.83532	7.247075
39		1375.000	-15.23928	7.351871
40		1380.000	-15.66408	7.471646
41		1385.000	-16.11121	7.607537
42		1390.000	-16.58234	7.760849
43		1395.000	-17.07932	7.933075
44		1400.000	-17.60420	8.125916
45		1500.000	-4.018536	12.44893
46		1600.000	-2.885425	11.31038
47		1700.000	-2.145375	10.32254
48		1800.000	-1.592947	9.482872
49		1900.000	-1.184808	8.750233

50	2000.000	-0.8953396	8.107148
51	2100.000	-0.6709451	7.539242
52	2200.000	-0.4910424	7.033835
53	2300.000	-0.2669138	6.570822
54	2400.000	-0.1589576	6.143772
55	2500.000	-7.8631461E-02	5.756646
56	2600.000	-2.8784975E-02	5.404647
57	2700.000	1.1684831E-02	5.085346
58	2800.000	3.8398005E-02	4.793488
59	2900.000	5.4030951E-02	4.525991
60	3000.000	5.7593603E-02	4.280249
61	3100.000	5.6503318E-02	4.055951
62	3200.000	4.9936719E-02	3.849130
63	3300.000	3.8955834E-02	3.657989
64	3400.000	2.4415979E-02	3.480960
65	3500.000	7.0093237E-03	3.316668
66	3600.000	-1.2702152E-02	3.163903
67	3700.000	-3.4260809E-02	3.021596
68	3800.000	-5.7292998E-02	2.888803
69	3900.000	-8.1493519E-02	2.764682
70	4000.000	-0.1066125	2.648485
71	4100.000	-0.1324460	2.539543
72	4200.000	-0.1588271	2.437257
73	4300.000	-0.1856200	2.341089
74	4400.000	-0.2127144	2.250556
75	4500.000	-0.2400214	2.165220
76	4600.000	-0.2674696	2.084686
77	4700.000	-0.2950028	2.008598
78	4800.000	-0.3225760	1.936629
79	4900.000	-0.3527754	1.868593
80	5000.000	-0.3820444	1.804215
81	5100.000	-0.4095708	1.743193
82	5200.000	-0.4370374	1.685247
83	5300.000	-0.4644422	1.630172
84	5400.000	-0.4917867	1.577779
85	5500.000	-0.5190772	1.527894
86	5600.000	-0.5463270	1.480357
87	5700.000	-0.5766885	1.435150
88	5800.000	-0.6039156	1.392048
89	5900.000	-0.6311359	1.350885
90	6000.000	-0.6583713	1.311545
91	6100.000	-0.6856458	1.273920
92	6200.000	-0.7129853	1.237912
93	6300.000	-0.7404187	1.203427
94	6400.000	-0.7679761	1.170380
95	6500.000	-0.7956909	1.138691
96	6600.000	-0.8235986	1.108286
97	6700.000	-0.8517374	1.079096
98	6800.000	-0.8801485	1.051055
99	6900.000	-0.9088759	1.024103
100	7000.000	-0.9379674	0.9981853
101	7100.000	-0.9674743	0.9732476
102	7200.000	-0.9974524	0.9492409
103	7300.000	-1.027962	0.9261189

104	7400.000	-1.059070	0.9038382
105	7500.000	-1.090847	0.8823581
106	7600.000	-1.123374	0.8616402
107	7700.000	-1.156737	0.8416483
108	7800.000	-1.191034	0.8223487
109	7900.000	-1.226374	0.8037095
110	8000.000	-1.262904	0.7857007
111	8100.000	-1.300705	0.7682937
112	8200.000	-1.339959	0.7514619
113	8300.000	-1.380844	0.7351796
114	8400.000	-1.423561	0.7194232
115	8500.000	-1.468345	0.7041699
116	8600.000	-1.515470	0.6893983
117	8700.000	-1.565254	0.6750884
118	8800.000	-1.618083	0.6612206
119	8900.000	-1.674413	0.6477770
120	9000.000	-1.734817	0.6348592
121	9100.000	-1.799964	0.6223299
122	9200.000	-1.870713	0.6101736
123	9300.000	-1.948166	0.5983752
124	9400.000	-2.033750	0.5869208
125	9500.000	-2.129380	0.5757968
126	9600.000	-2.237686	0.5649906
127	9700.000	-2.362435	0.5544900
128	9800.000	-2.509282	0.5442833
129	9900.000	-2.687268	0.5343597
130	10000.00	-2.912190	0.5247084
131	10100.00	-3.215471	0.5153197
132	10200.00	-3.674937	0.5061839
133	10270.00	-4.222119	0.4999343
134	10275.00	-4.276143	0.4994925
135	10280.00	-4.333321	0.4990512
136	10285.00	-4.394018	0.4986105
137	10290.00	-4.458680	0.4981703
138	10295.00	-4.527843	0.4977308
139	10300.00	-4.602160	0.4972918
140	10305.00	-4.682434	0.4968535
141	10310.00	-4.769671	0.4964157
142	10315.00	-4.865138	0.4959786
143	10320.00	-4.970545	0.4955420
144	10325.00	-5.088117	0.4951059
145	10330.00	-5.220948	0.4946705
146	10335.00	-5.373483	0.4942356
147	10340.00	-5.552439	0.4938013
148	10345.00	-5.768679	0.4933676
149	10350.00	-6.041520	0.4929345
150	10355.00	-6.410619	0.4925020
151	10360.00	-6.981718	0.4920700
152	10365.00	-8.292125	0.4916386
153	10370.00	-7.948841	3.892291
154	10375.00	-6.856984	3.888264
155	10380.00	-6.320314	3.884248
156	10385.00	-5.960458	3.880240
157	10390.00	-5.688938	3.876241

158	10395.00	-5.470593	3.872252
159	10400.00	-5.287859	3.868273
160	10405.00	-5.130586	3.864302
161	10410.00	-4.992494	3.860340
162	10415.00	-4.869360	3.856387
163	10420.00	-4.758223	3.852444
164	10425.00	-4.656924	3.848509
165	10430.00	-4.563839	3.844584
166	10435.00	-4.477720	3.840667
167	10440.00	-4.397598	3.836760
168	10445.00	-4.322653	3.832861
169	10450.00	-4.252260	3.828971
170	10455.00	-4.185891	3.825090
171	10460.00	-4.123104	3.821218
172	10465.00	-4.063528	3.817355
173	10500.00	-3.714567	3.790558
174	10600.00	-3.067343	3.716298
175	10700.00	-2.652269	3.645302
176	10800.00	-2.347398	3.577394
177	10900.00	-2.107723	3.512410
178	11000.00	-1.911404	3.450194
179	11100.00	-1.746119	3.390604
180	11200.00	-1.604182	3.333506
181	11300.00	-1.480459	3.278773
182	11400.00	-1.371341	3.226288
183	11500.00	-1.274183	3.175941
184	11600.00	-1.186988	3.127628
185	11700.00	-1.108208	3.081252
186	11800.00	-1.036615	3.036722
187	11900.00	-0.9712204	2.993952
188	12000.00	-0.9112132	2.952861
189	12100.00	-0.8559216	2.913374
190	12200.00	-0.8047814	2.875419
191	12300.00	-0.7573131	2.838929
192	12400.00	-0.7131080	2.803839
193	12500.00	-0.6718121	2.770091
194	12600.00	-0.6331190	2.737627
195	12700.00	-0.5967606	2.706394
196	12800.00	-0.5624999	2.676341
197	12900.00	-0.5301288	2.647420
198	13000.00	-0.4994608	2.619587
199	13100.00	-0.4703301	2.592797
200	13200.00	-0.4425876	2.567012
201	13300.00	-0.4160981	2.542190
202	13400.00	-0.3907388	2.518298
203	13500.00	-0.2629591	2.493533
204	13600.00	-0.2365060	2.463472
205	13700.00	-0.2113342	2.433945
206	13800.00	-0.1873535	2.404938
207	13900.00	-0.1644931	2.376440
208	14000.00	-0.1426874	2.348438
209	14100.00	-0.1218766	2.320921
210	14200.00	-0.1020055	2.293878
211	14300.00	-8.3022378E-02	2.267297

212	14400.00	-6.4879976E-02	2.241168
213	14500.00	-4.7533680E-02	2.215482
214	14600.00	-3.0942462E-02	2.190227
215	14700.00	-1.5068039E-02	2.165395
216	14800.00	1.2577558E-04	2.140975
217	14900.00	1.4672253E-02	2.116958
218	15000.00	2.8603101E-02	2.093337
219	15100.00	4.1947644E-02	2.070101
220	15200.00	5.4733433E-02	2.047243
221	15300.00	6.6986710E-02	2.024754
222	15400.00	7.8731716E-02	2.002627
223	15500.00	8.9991711E-02	1.980853
224	15600.00	0.1007883	1.959426
225	15700.00	0.1111419	1.938337
226	15800.00	0.1210721	1.917580
227	15900.00	0.1305971	1.897147
228	16000.00	0.1397342	1.877033
229	16100.00	0.1484999	1.857229
230	16200.00	0.1569097	1.837731
231	16300.00	0.1649782	1.818532
232	16400.00	0.1727197	1.799624
233	16500.00	0.1801474	1.781004
234	16600.00	0.1872739	1.762664
235	16700.00	0.1941113	1.744599
236	16800.00	0.2006708	1.726804
237	16900.00	0.2069636	1.709274
238	17000.00	0.2130000	1.692002
239	17100.00	0.2187899	1.674985
240	17200.00	0.2243427	1.658216
241	17300.00	0.2296673	1.641692
242	17400.00	0.2347725	1.625407
243	17500.00	0.2396665	1.609357
244	17600.00	0.2443571	1.593537
245	17700.00	0.2488518	1.577943
246	17800.00	0.2531577	1.562572
247	17900.00	0.2572820	1.547417
248	18000.00	0.2612309	1.532475
249	18100.00	0.2650110	1.517744
250	18200.00	0.2686282	1.503217
251	18300.00	0.2720882	1.488893
252	18400.00	0.2753968	1.474766
253	18500.00	0.2785591	1.460833
254	18600.00	0.2815804	1.447092
255	18700.00	0.2844656	1.433537
256	18800.00	0.2872191	1.420167
257	18900.00	0.2898459	1.406977
258	19000.00	0.2923500	1.393965
259	19100.00	0.2947358	1.381127
260	19200.00	0.2970072	1.368460
261	19300.00	0.2991680	1.355961
262	19400.00	0.3012221	1.343627
263	19500.00	0.3031730	1.331455
264	19600.00	0.3050241	1.319443
265	19700.00	0.3067788	1.307588

266	19800.00	0.3084402	1.295886
267	19900.00	0.3100115	1.284336
268	20000.00	0.3114955	1.272934
269	20100.00	0.3128952	1.261679
270	20200.00	0.3142134	1.250567
271	20300.00	0.3154525	1.239597
272	20400.00	0.3166154	1.228765
273	20500.00	0.3177043	1.218071
274	20600.00	0.3187217	1.207510
275	20700.00	0.3196698	1.197081
276	20800.00	0.3165946	1.186852
277	20900.00	0.3173937	1.176786
278	21000.00	0.3181323	1.166845
279	21100.00	0.3188125	1.157028
280	21200.00	0.3194361	1.147333
281	21300.00	0.3200049	1.137757
282	21400.00	0.3205208	1.128299
283	21500.00	0.3209854	1.118956
284	21600.00	0.3214004	1.109727
285	21700.00	0.3217674	1.100609
286	21800.00	0.3220879	1.091602
287	21900.00	0.3223633	1.082703
288	22000.00	0.3225952	1.073911
289	22100.00	0.3227850	1.065223
290	22200.00	0.3229339	1.056639
291	22300.00	0.3230432	1.048156
292	22400.00	0.3231143	1.039773
293	22500.00	0.3231483	1.031489
294	22600.00	0.3231463	1.023301
295	22700.00	0.3231097	1.015209
296	22800.00	0.3230393	1.007210
297	22900.00	0.3229364	0.9993043
298	23000.00	0.3228019	0.9914892
299	23100.00	0.3226368	0.9837637
300	23200.00	0.3224420	0.9761264
301	23300.00	0.3222186	0.9685761
302	23400.00	0.3219673	0.9611112
303	23500.00	0.3216892	0.9537306
304	23600.00	0.3213849	0.9464331
305	23700.00	0.3210554	0.9392173
306	23800.00	0.3203978	0.9320825
307	23900.00	0.3200224	0.9250281
308	24000.00	0.3196232	0.9180520
309	24100.00	0.3192016	0.9111528
310	24200.00	0.3187584	0.9043294
311	24300.00	0.3182942	0.8975810
312	24400.00	0.3175611	0.8909068
313	24500.00	0.3170580	0.8843057
314	24600.00	0.3165355	0.8777761
315	24700.00	0.3159943	0.8713171
316	24800.00	0.3154348	0.8649277
317	24900.00	0.3148576	0.8586066

C.3.4 Arsenide

1	%	Energy (eV)	f'	f''
2		1000.000	-9.429335	3.484835
3		1100.000	-10.50740	3.068583
4		1200.000	-12.45976	2.726221
5		1226.000	-13.32295	2.647042
6		1231.000	-13.52381	2.632231
7		1236.000	-13.73969	2.617549
8		1241.000	-13.97290	2.602995
9		1246.000	-14.22623	2.588568
10		1251.000	-14.50320	2.574266
11		1256.000	-14.80822	2.560088
12		1261.000	-15.14697	2.546031
13		1266.000	-15.52682	2.532096
14		1271.000	-15.95758	2.518280
15		1276.000	-16.45258	2.504581
16		1281.000	-17.03035	2.490999
17		1286.000	-17.71758	2.477531
18		1291.000	-18.55410	2.464178
19		1296.000	-19.60247	2.450936
20		1300.000	-20.66173	2.440423
21		1301.000	-20.96742	2.437805
22		1306.000	-22.84129	2.424784
23		1311.000	-25.63062	2.411871
24		1316.000	-30.43916	2.399066
25		1321.000	-42.96489	2.386366
26		1326.000	-36.88134	37.12148
27		1331.000	-23.81698	32.86283
28		1336.000	-18.21088	29.21878
29		1341.000	-15.38761	26.09086
30		1346.000	-14.29931	23.39770
31		1351.000	-14.89571	21.07187
32		1356.000	-19.10551	19.05730
33		1361.000	-17.71439	34.55799
34		1366.000	-9.902804	30.98588
35		1371.000	-6.451541	27.89469
36		1376.000	-4.473392	25.21188
37		1381.000	-3.272238	22.87692
38		1386.000	-2.547956	20.83909
39		1391.000	-2.139610	19.05578
40		1396.000	-1.947594	17.49110
41		1400.000	-1.906566	16.37623
42		1401.000	-1.908722	16.11472
43		1406.000	-1.979324	14.90097
44		1411.000	-2.128795	13.82806
45		1416.000	-2.335210	12.87744
46		1421.000	-2.582657	12.03327
47		1429.000	-3.035664	10.87096
48		1431.000	-3.156718	10.61208
49		1434.000	-3.342456	10.24493

50	1436.000	-3.468604	10.01348
51	1439.000	-3.660655	9.684943
52	1441.000	-3.790241	9.477643
53	1444.000	-3.986477	9.183137
54	1446.000	-4.118299	8.997155
55	1449.000	-4.317206	8.732725
56	1451.000	-4.450428	8.565610
57	1454.000	-4.650976	8.327834
58	1456.000	-4.785047	8.177460
59	1459.000	-4.986594	7.963365
60	1464.000	-5.323416	7.634889
61	1469.000	-5.661268	7.338550
62	1474.000	-6.000402	7.070988
63	1479.000	-6.341493	6.829267
64	1484.000	-6.685682	6.610822
65	1489.000	-7.034696	6.413407
66	1494.000	-7.391076	6.235057
67	1499.000	-7.758647	6.074046
68	1500.000	-7.833984	6.043787
69	1504.000	-8.143474	5.928864
70	1509.000	-8.556079	5.798186
71	1514.000	-9.017524	5.680850
72	1519.000	-9.581702	5.575845
73	1524.000	-10.49753	5.482283
74	1529.000	-10.74992	7.293207
75	1534.000	-10.33972	7.215660
76	1539.000	-10.28549	7.147589
77	1544.000	-10.33768	7.088501
78	1549.000	-10.44271	7.037976
79	1554.000	-10.58016	6.995667
80	1559.000	-10.74015	6.961286
81	1564.000	-10.91732	6.934611
82	1569.000	-11.10853	6.915473
83	1574.000	-11.31185	6.903756
84	1579.000	-11.52614	6.899396
85	1584.000	-11.75070	6.902381
86	1589.000	-11.98520	6.912745
87	1594.000	-12.22952	6.930571
88	1599.000	-12.48373	6.955991
89	1600.000	-12.53578	6.962002
90	1604.000	-12.74801	6.989188
91	1609.000	-13.02272	7.030393
92	1614.000	-13.30825	7.079892
93	1619.000	-13.60511	7.138022
94	1624.000	-13.91390	7.205182
95	1700.000	-20.74950	9.869416
96	1800.000	-3.552651	11.95705
97	1900.000	-2.690663	11.04163
98	2000.000	-2.021769	10.23876
99	2100.000	-1.535833	9.514412
100	2200.000	-1.162870	8.867381
101	2300.000	-0.8732193	8.286686
102	2400.000	-0.6465170	7.763263
103	2500.000	-0.4682811	7.289583

104	2600.000	−0.3279317	6.859340
105	2700.000	−0.2076773	6.464999
106	2800.000	−0.1174221	6.100526
107	2900.000	−5.1044028E−02	5.765710
108	3000.000	−3.8216980E−03	5.457530
109	3100.000	3.1523775E−02	5.175311
110	3200.000	5.6195986E−02	4.914834
111	3300.000	7.2109155E−02	4.673888
112	3400.000	8.0811761E−02	4.450536
113	3500.000	8.3562613E−02	4.243082
114	3600.000	8.1391051E−02	4.050028
115	3700.000	7.5142905E−02	3.870053
116	3800.000	6.5516859E−02	3.701986
117	3900.000	5.2611321E−02	3.544797
118	4000.000	3.7832122E−02	3.397550
119	4100.000	2.1137524E−02	3.259409
120	4200.000	2.8622695E−03	3.129628
121	4300.000	−1.6713578E−02	3.007537
122	4400.000	−3.7355002E−02	2.892534
123	4500.000	−5.8865067E−02	2.784072
124	4600.000	−8.1078410E−02	2.681660
125	4700.000	−0.1038563	2.584851
126	4800.000	−0.1270824	2.493236
127	4900.000	−0.1506592	2.406449
128	5000.000	−0.1745056	2.324152
129	5100.000	−0.1985538	2.246036
130	5200.000	−0.2227479	2.171820
131	5300.000	−0.2470421	2.101246
132	5400.000	−0.2713985	2.034077
133	5500.000	−0.2957873	1.970095
134	5600.000	−0.3201844	1.909100
135	5700.000	−0.3445683	1.850907
136	5800.000	−0.3722760	1.795460
137	5900.000	−0.3987048	1.742554
138	6000.000	−0.4229532	1.692062
139	6100.000	−0.4471485	1.643750
140	6200.000	−0.4712933	1.597494
141	6300.000	−0.4953918	1.553177
142	6400.000	−0.5194498	1.510691
143	6500.000	−0.5434756	1.469935
144	6600.000	−0.5674836	1.430815
145	6700.000	−0.5951601	1.393386
146	6800.000	−0.6191666	1.357447
147	6900.000	−0.6431822	1.322897
148	7000.000	−0.6672234	1.289664
149	7100.000	−0.6913077	1.257681
150	7200.000	−0.7154541	1.226885
151	7300.000	−0.7396829	1.197217
152	7400.000	−0.7640153	1.168624
153	7500.000	−0.7884746	1.141051
154	7600.000	−0.8130853	1.114452
155	7700.000	−0.8378736	1.088781
156	7800.000	−0.8628673	1.063993
157	7900.000	−0.8880959	1.040049

158	8000.000	−0.9135913	1.016910
159	8100.000	−0.9393874	0.9945406
160	8200.000	−0.9655202	0.9729064
161	8300.000	−0.9920292	0.9519748
162	8400.000	−1.018956	0.9317159
163	8500.000	−1.046346	0.9121004
164	8600.000	−1.074249	0.8931014
165	8700.000	−1.102717	0.8746931
166	8800.000	−1.131810	0.8568507
167	8900.000	−1.161590	0.8395514
168	9000.000	−1.192185	0.8228930
169	9100.000	−1.223608	0.8067341
170	9200.000	−1.255944	0.7910547
171	9300.000	−1.289289	0.7758356
172	9400.000	−1.323748	0.7610589
173	9500.000	−1.359442	0.7467071
174	9600.000	−1.396506	0.7327641
175	9700.000	−1.435091	0.7192142
176	9800.000	−1.475373	0.7060425
177	9900.000	−1.517552	0.6932349
178	10000.00	−1.561863	0.6807779
179	10100.00	−1.608575	0.6686586
180	10200.00	−1.658008	0.6568649
181	10300.00	−1.710545	0.6453850
182	10400.00	−1.766640	0.6342077
183	10500.00	−1.826852	0.6233222
184	10600.00	−1.891866	0.6127184
185	10700.00	−1.962539	0.6023866
186	10800.00	−2.039969	0.5923173
187	10900.00	−2.125583	0.5825018
188	11000.00	−2.221288	0.5729312
189	11100.00	−2.329711	0.5635975
190	11200.00	−2.454608	0.5544930
191	11300.00	−2.601625	0.5456098
192	11400.00	−2.779780	0.5369410
193	11500.00	−3.004832	0.5284795
194	11600.00	−3.308127	0.5202186
195	11700.00	−3.767294	0.5121522
196	11769.00	−4.303414	0.5066964
197	11774.00	−4.356803	0.5063044
198	11779.00	−4.413270	0.5059130
199	11784.00	−4.473176	0.5055220
200	11789.00	−4.536944	0.5051315
201	11794.00	−4.605115	0.5047414
202	11799.00	−4.678308	0.5043518
203	11800.00	−4.693621	0.5042739
204	11804.00	−4.757299	0.5039626
205	11809.00	−4.843057	0.5035739
206	11814.00	−4.936817	0.5031856
207	11819.00	−5.040181	0.5027978
208	11824.00	−5.155290	0.5024104
209	11829.00	−5.285084	0.5020235
210	11834.00	−5.433736	0.5016371
211	11839.00	−5.607609	0.5012511

212	11844.00	-5.816780	0.5008656
213	11849.00	-6.078978	0.5004805
214	11854.00	-6.429896	0.5000958
215	11859.00	-6.960586	0.4997116
216	11864.00	-8.076112	0.4993278
217	11869.00	-8.254848	3.865319
218	11874.00	-7.011160	3.861774
219	11879.00	-6.446832	3.858236
220	11884.00	-6.076585	3.854706
221	11889.00	-5.800160	3.851182
222	11894.00	-5.579269	3.847666
223	11899.00	-5.395152	3.844157
224	11900.00	-5.361740	3.843457
225	11904.00	-5.237200	3.840655
226	11909.00	-5.098830	3.837161
227	11914.00	-4.975692	3.833674
228	11919.00	-4.864691	3.830194
229	11924.00	-4.763636	3.826720
230	11929.00	-4.670869	3.823254
231	11934.00	-4.585117	3.819795
232	11939.00	-4.505380	3.816343
233	11944.00	-4.430857	3.812897
234	11949.00	-4.360900	3.809459
235	11954.00	-4.294974	3.806028
236	11959.00	-4.232644	3.802605
237	11964.00	-4.173512	3.799188
238	12000.00	-3.819016	3.774788
239	12100.00	-3.181885	3.708845
240	12200.00	-2.772388	3.645494
241	12300.00	-2.470868	3.584609
242	12400.00	-2.233180	3.526073
243	12500.00	-2.037926	3.469776
244	12600.00	-1.873044	3.415612
245	12700.00	-1.731026	3.363485
246	12800.00	-1.606859	3.313302
247	12900.00	-1.497025	3.264975
248	13000.00	-1.398948	3.218422
249	13100.00	-1.310685	3.173567
250	13200.00	-1.230730	3.130335
251	13300.00	-1.157891	3.088657
252	13400.00	-1.091206	3.048468
253	13500.00	-1.029888	3.009706
254	13600.00	-0.9732839	2.972312
255	13700.00	-0.9208464	2.936231
256	13800.00	-0.8721094	2.901409
257	13900.00	-0.8266758	2.867798
258	14000.00	-0.7842017	2.835349
259	14100.00	-0.7443893	2.804018
260	14200.00	-0.7069778	2.773762
261	14300.00	-0.6717373	2.744539
262	14400.00	-0.6384651	2.716313
263	14500.00	-0.6069801	2.689046
264	14600.00	-0.5771215	2.662703
265	14700.00	-0.5487446	2.637251

266	14800.00	-0.5217186	2.612658
267	14900.00	-0.4959261	2.588894
268	15000.00	-0.4712596	2.565931
269	15100.00	-0.4476219	2.543740
270	15200.00	-0.4249241	2.522297
271	15300.00	-0.4030842	2.501575
272	15400.00	-0.3820317	2.481552
273	15500.00	-0.2537031	2.457054
274	15600.00	-0.2314214	2.431130
275	15700.00	-0.2100757	2.405610
276	15800.00	-0.1896170	2.380485
277	15900.00	-0.1699997	2.355747
278	16000.00	-0.1511804	2.331387
279	16100.00	-0.1331194	2.307398
280	16200.00	-0.1157795	2.283772
281	16300.00	-9.9125974E-02	2.260503
282	16400.00	-8.3125629E-02	2.237581
283	16500.00	-6.7748182E-02	2.215002
284	16600.00	-5.2964929E-02	2.192758
285	16700.00	-3.8748894E-02	2.170842
286	16800.00	-2.5074953E-02	2.149248
287	16900.00	-1.1918684E-02	2.127970
288	17000.00	7.4218388E-04	2.107000
289	17100.00	1.2928919E-02	2.086334
290	17200.00	2.4661615E-02	2.065966
291	17300.00	3.5959065E-02	2.045889
292	17400.00	4.6839688E-02	2.026098
293	17500.00	5.7320297E-02	2.006588
294	17600.00	6.7417055E-02	1.987354
295	17700.00	7.7145278E-02	1.968389
296	17800.00	8.6519368E-02	1.949690
297	17900.00	9.5553502E-02	1.931251
298	18000.00	0.1042607	1.913067
299	18100.00	0.1126534	1.895134
300	18200.00	0.1207435	1.877446
301	18300.00	0.1285424	1.860001
302	18400.00	0.1360610	1.842792
303	18500.00	0.1433097	1.825816
304	18600.00	0.1502983	1.809069
305	18700.00	0.1570361	1.792546
306	18800.00	0.1635175	1.776244
307	18900.00	0.1697807	1.760158
308	19000.00	0.1758191	1.744285
309	19100.00	0.1816405	1.728621
310	19200.00	0.1872524	1.713162
311	19300.00	0.1926621	1.697905
312	19400.00	0.1978766	1.682846
313	19500.00	0.2029025	1.667982
314	19600.00	0.2077461	1.653309
315	19700.00	0.2124137	1.638824
316	19800.00	0.2169109	1.624525
317	19900.00	0.2212437	1.610407
318	20000.00	0.2254172	1.596468
319	20100.00	0.2294368	1.582704

320	20200.00	0.2333074	1.569113
321	20300.00	0.2370338	1.555692
322	20400.00	0.2406207	1.542439
323	20500.00	0.2440726	1.529349
324	20600.00	0.2473937	1.516421
325	20700.00	0.2505882	1.503651
326	20800.00	0.2536599	1.491039
327	20900.00	0.2566130	1.478580
328	21000.00	0.2594509	1.466272
329	21100.00	0.2621772	1.454113
330	21200.00	0.2647954	1.442100
331	21300.00	0.2673087	1.430232
332	21400.00	0.2697205	1.418505
333	21500.00	0.2720338	1.406918
334	21600.00	0.2742515	1.395469
335	21700.00	0.2763766	1.384154
336	21800.00	0.2784117	1.372973
337	21900.00	0.2803596	1.361922
338	22000.00	0.2822230	1.351001
339	22100.00	0.2840042	1.340206
340	22200.00	0.2857057	1.329536
341	22300.00	0.2873298	1.318990
342	22400.00	0.2888789	1.308565
343	22500.00	0.2903550	1.298259
344	22600.00	0.2917604	1.288070
345	22700.00	0.2930970	1.277997
346	22800.00	0.2943668	1.268039
347	22900.00	0.2955718	1.258192
348	23000.00	0.2967138	1.248456
349	23100.00	0.2977946	1.238830
350	23200.00	0.2988158	1.229310
351	23300.00	0.2997794	1.219897
352	23400.00	0.3006867	1.210587
353	23500.00	0.3015394	1.201380
354	23600.00	0.3023391	1.192275
355	23700.00	0.3030872	1.183269
356	23800.00	0.3003767	1.174414
357	23900.00	0.3010126	1.165682
358	24000.00	0.3016027	1.157046
359	24100.00	0.3021481	1.148504
360	24200.00	0.3026502	1.140054
361	24300.00	0.3031102	1.131696
362	24400.00	0.3035291	1.123428
363	24500.00	0.3039081	1.115249
364	24600.00	0.3042483	1.107157
365	24700.00	0.3045507	1.099151
366	24800.00	0.3048164	1.091230
367	24900.00	0.3050463	1.083393

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